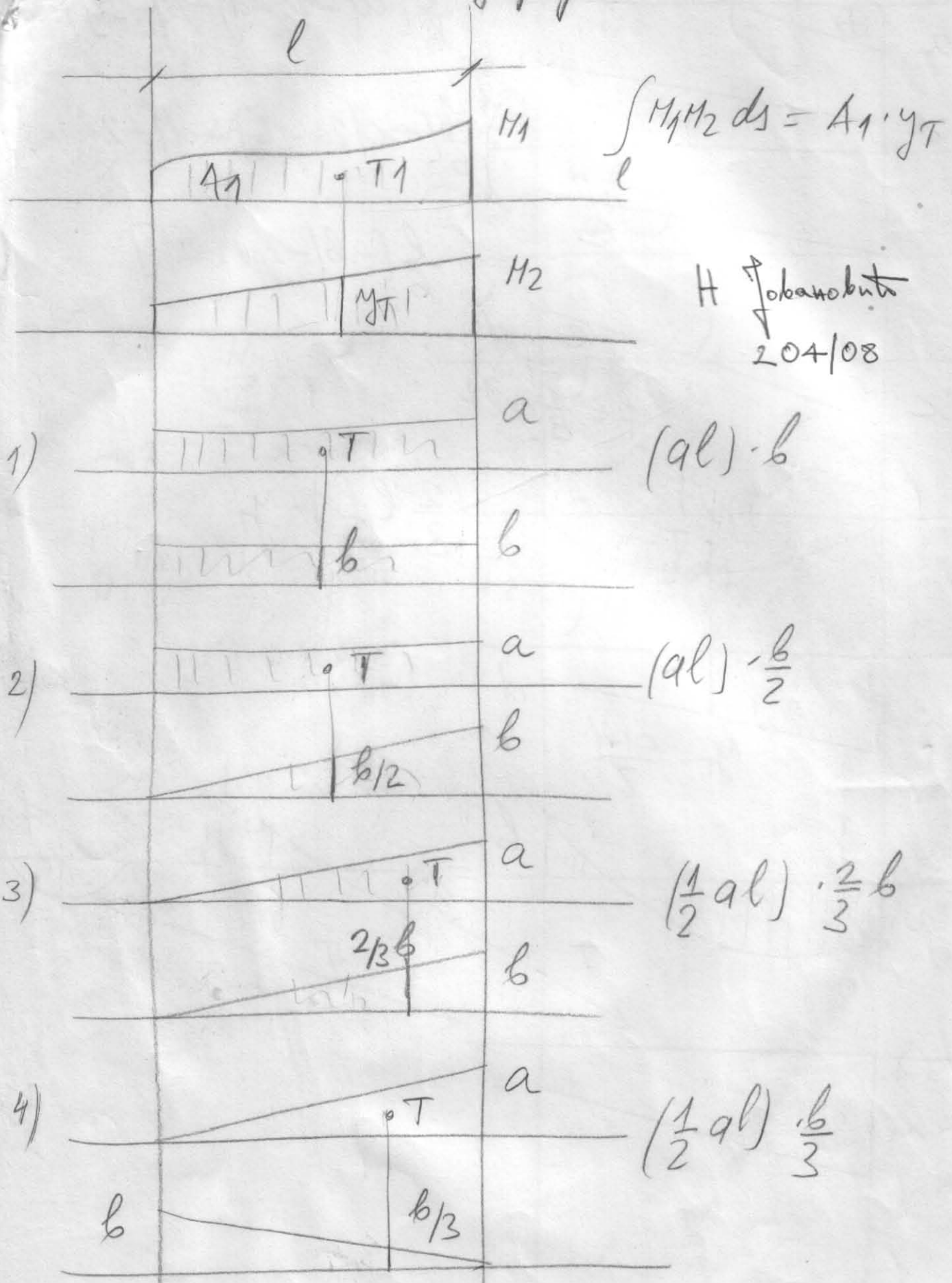


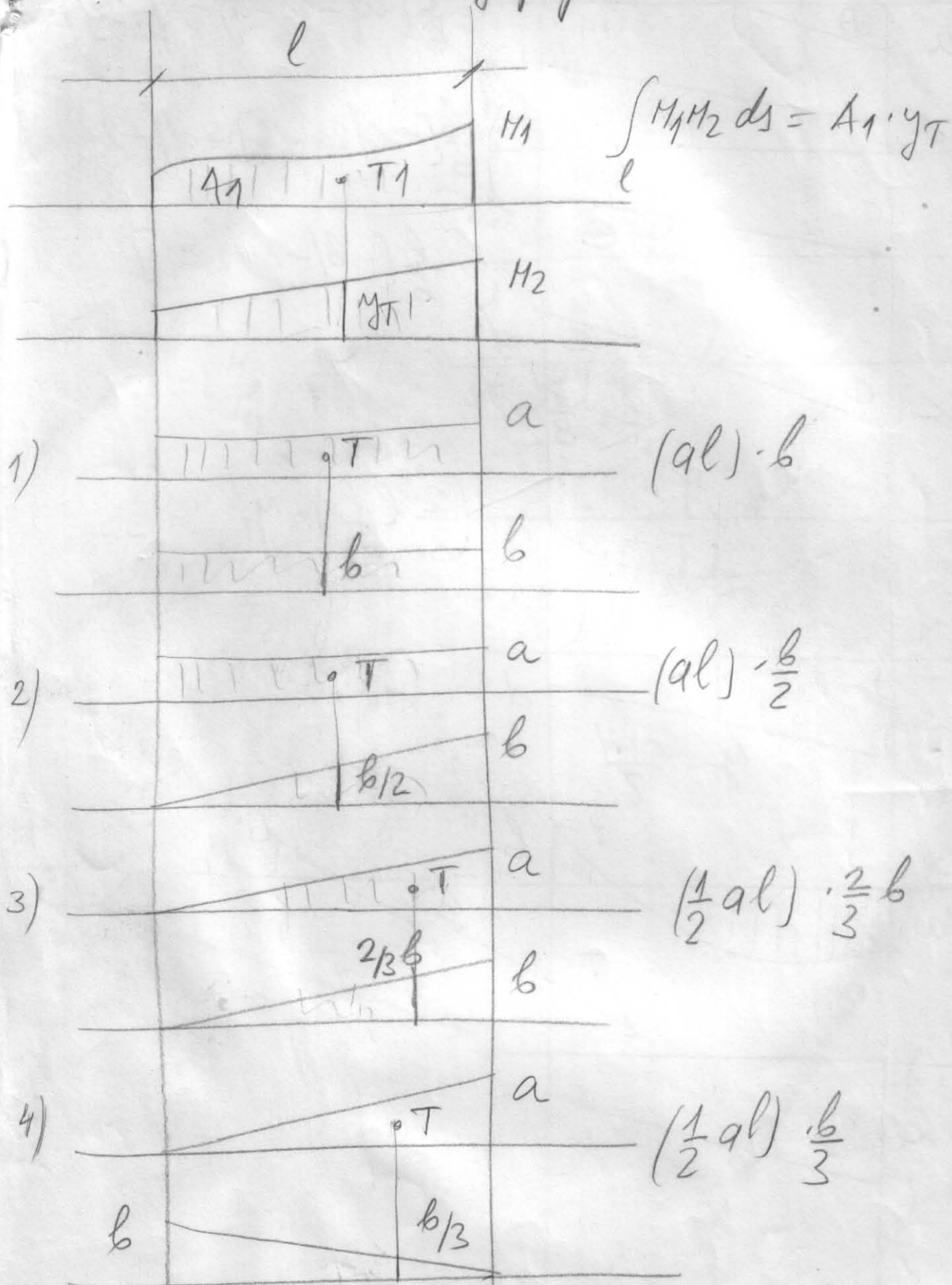
Muskruse gijafans



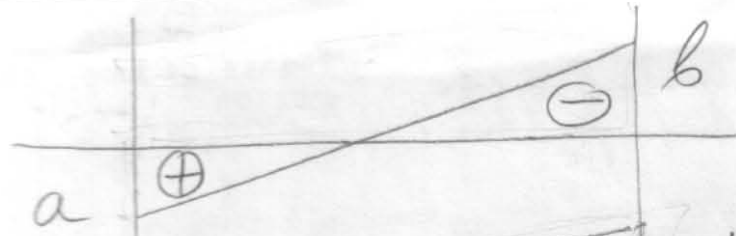
$$\int_0^l M_1 M_2 ds = A_1 \cdot y_T$$

H \int obanobuta
204/08

Musrose gijafans

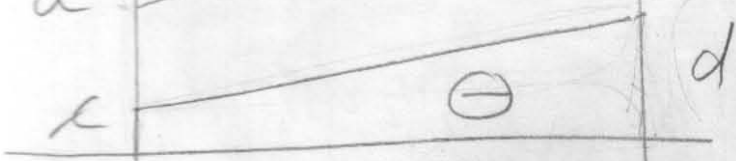


5)



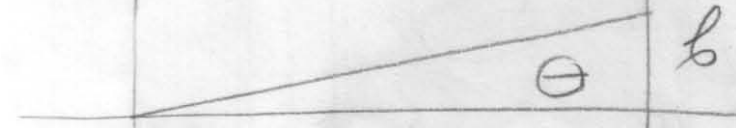
$$\frac{l}{6} [a(-2c-d) - b(-2d-c)]$$

c



$$\frac{l}{6} [-c(2a-b) - d(-2b+a)]$$

6)



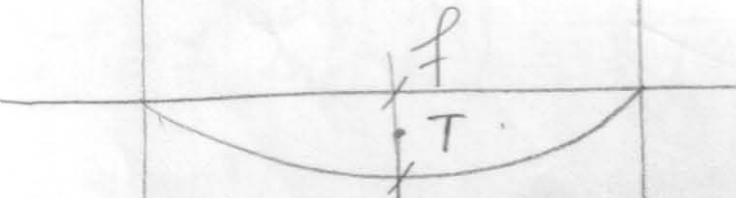
$$\frac{l}{6} [-b(-2d+c)]$$

c



$$f = \frac{1}{8} g l^2$$

7)



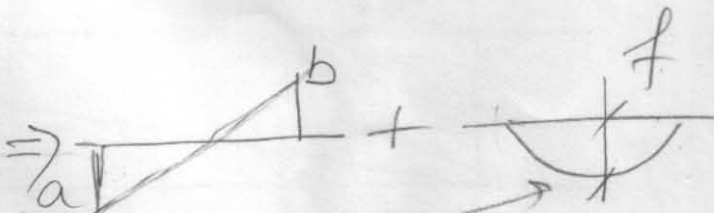
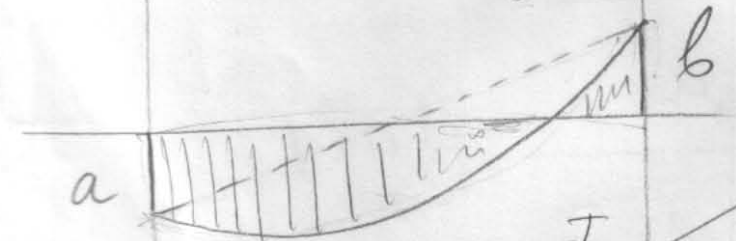
$$\left(\frac{2}{3} l f\right) \cdot \eta_T$$

c



$$\eta_T = \frac{c+d}{2}$$

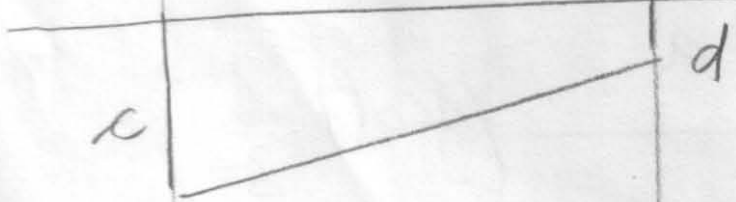
8)

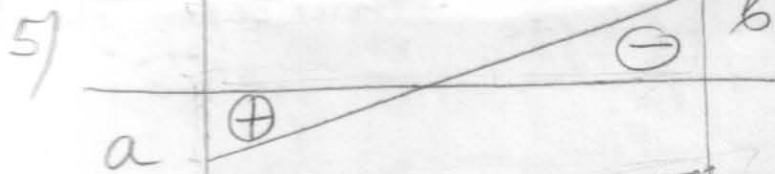


I

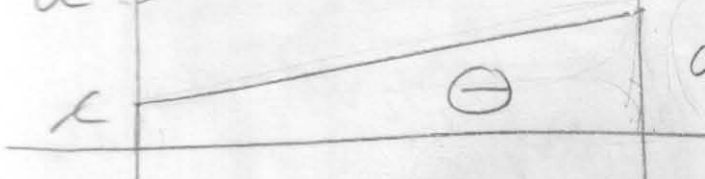
II

c

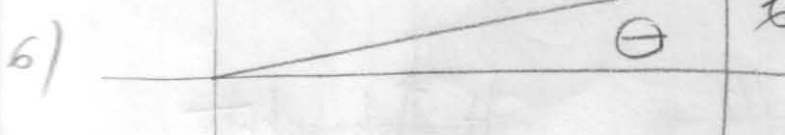




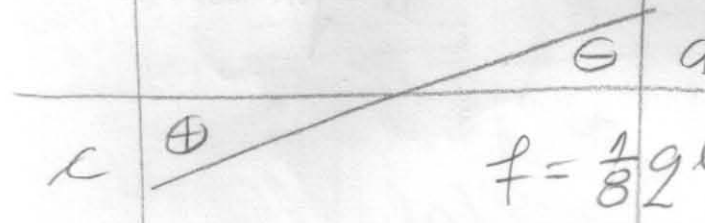
$$\frac{l}{6} [a(-2c-d) - b(-2d-c)]$$



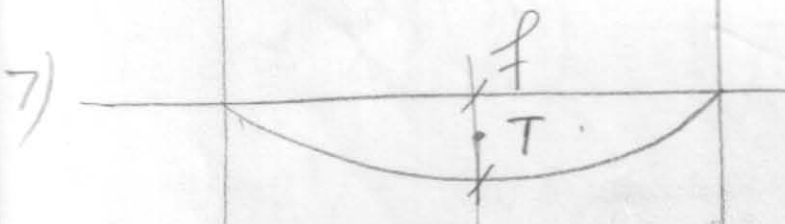
$$\frac{l}{6} [-c(2a-b) - d(-2b+a)]$$



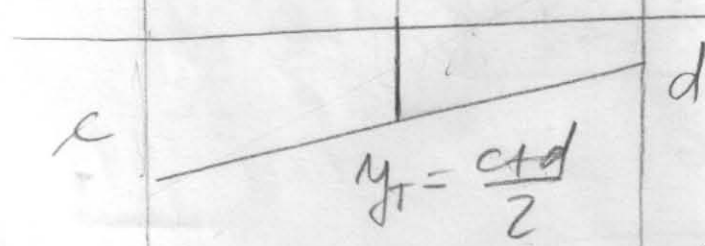
$$\frac{l}{6} [-b(-2d+c)]$$



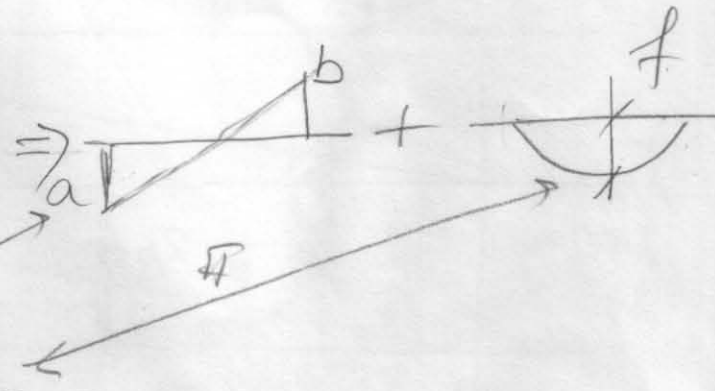
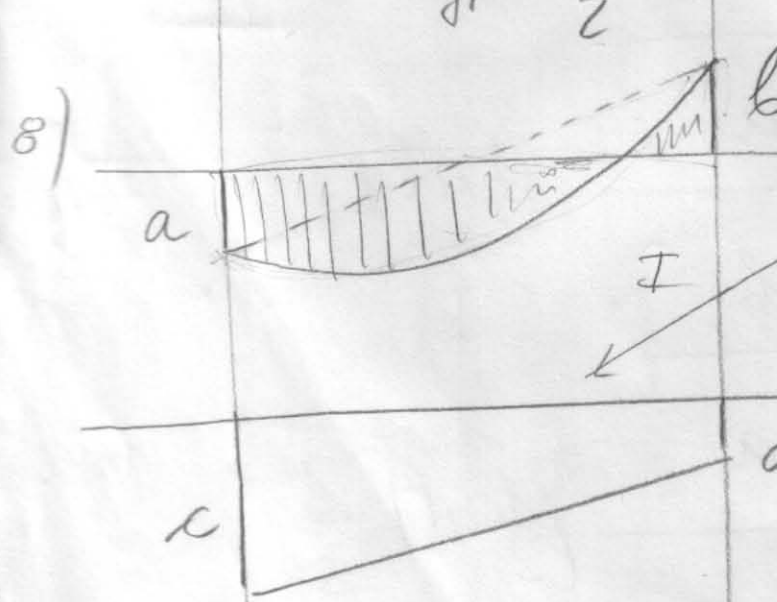
$$f = \frac{1}{8} g l^2$$



$$\left(\frac{2}{3} l f\right) \cdot \gamma$$



$$y_T = \frac{c+d}{2}$$



бх Нормали комбокейтари наџом

$$\sigma_x = \frac{N}{A}$$

$$\sigma_x^{M_y} = \left(\frac{M_y}{I_y} \right) \cdot z$$

$$I_y = \int z^2 t ds$$

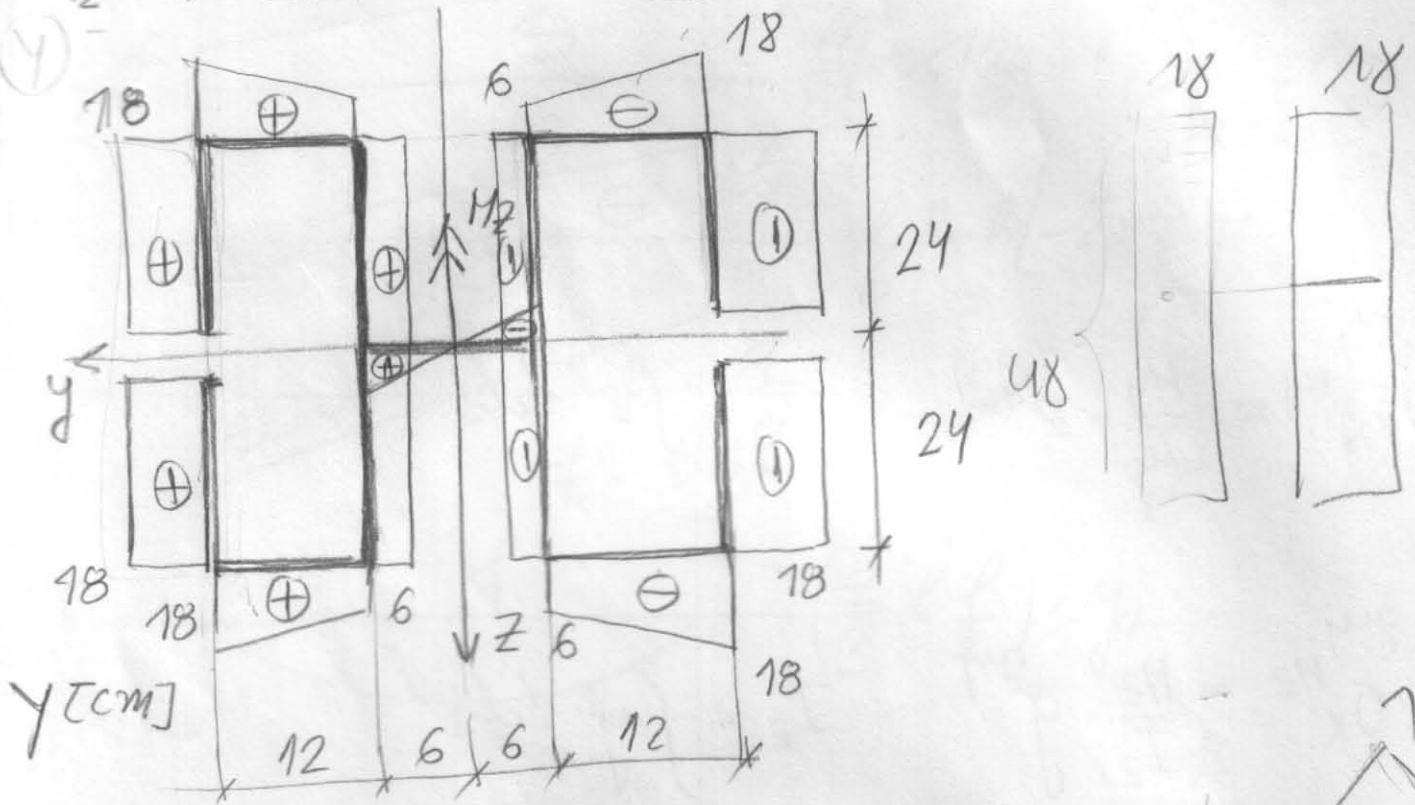
$$\sigma_x^{M_z} = - \left(\frac{M_z}{I_z} \right) \cdot y$$

$$I_z = \int y^2 t ds$$

$$N = 400 \text{ kN}$$

$$M_z = 70 \text{ kNm}$$

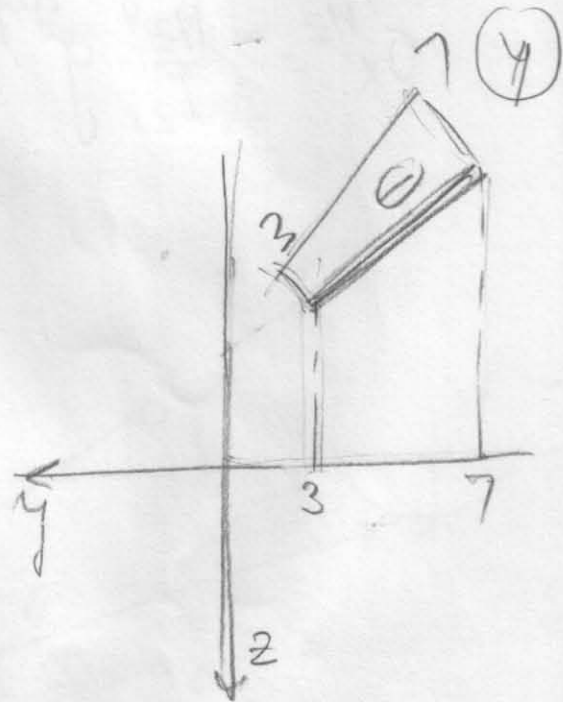
$$t = 1 \text{ cm}$$



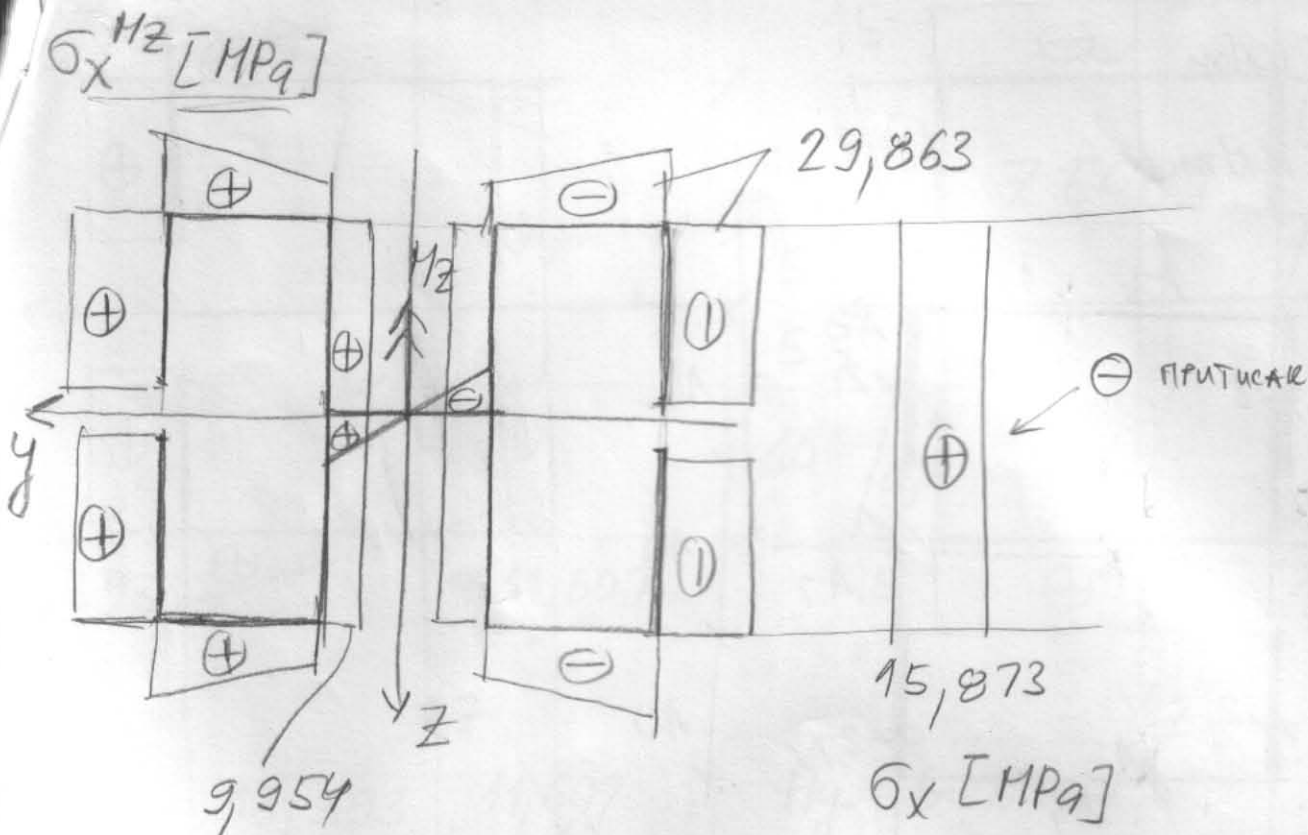
$$\sigma_x^N = \frac{N}{A}$$

$$\sigma_x^{Mz} = \left(\frac{Mz}{I_z} \right) y$$

$$I_z = \int y^2 t ds$$



$$I_z = 2 \cdot 1 \cdot (18 \cdot 48) \cdot 18 + 4 \cdot 1 \cdot \frac{12}{6} [18 | 2 \cdot 18 + 6 | + 6 | 2 \cdot 6 + 18 |] + 2 \cdot 1 \cdot (6 \cdot 48) \cdot 6 + 2 \cdot 1 \cdot \left(\frac{1}{2} \cdot 6 \cdot 6 \right) \cdot \frac{2}{3} \cdot 6 = 42192 \text{ cm}^4$$



$$\sigma_x = \frac{M_z}{I_{yoy}} \cdot (6 \text{ cm}) = 9,954 \text{ MPa}$$

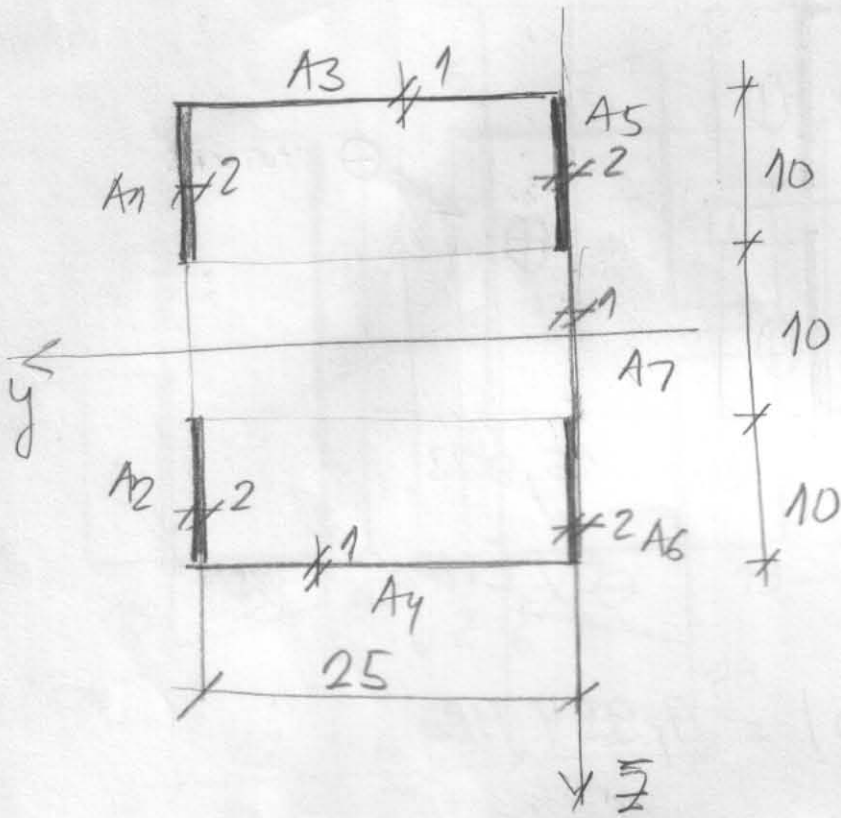
$$|18 \text{ cm}| = 29,863 \text{ MPa}$$

$$A = 5 \cdot 12 \cdot 1 + 4 \cdot 48 \cdot 1 = 252 \text{ cm}^2$$

$$\sigma_x^N = \frac{400 \text{ kN}}{252 \text{ cm}^2} = 15,873 \text{ MPa}$$

$$M_y = 5 \text{ kNm}$$

$$M_z = 3 \text{ kNm}$$



$$A_1 = 20 \quad \bar{T}_1(25; -10)$$

$$A_2 = 20 \quad \bar{T}_2(25; 10)$$

$$A_3 = 25 \quad \bar{T}_3(12,5; -15)$$

$$A_4 = 25 \quad \bar{T}_4(12,5; 15)$$

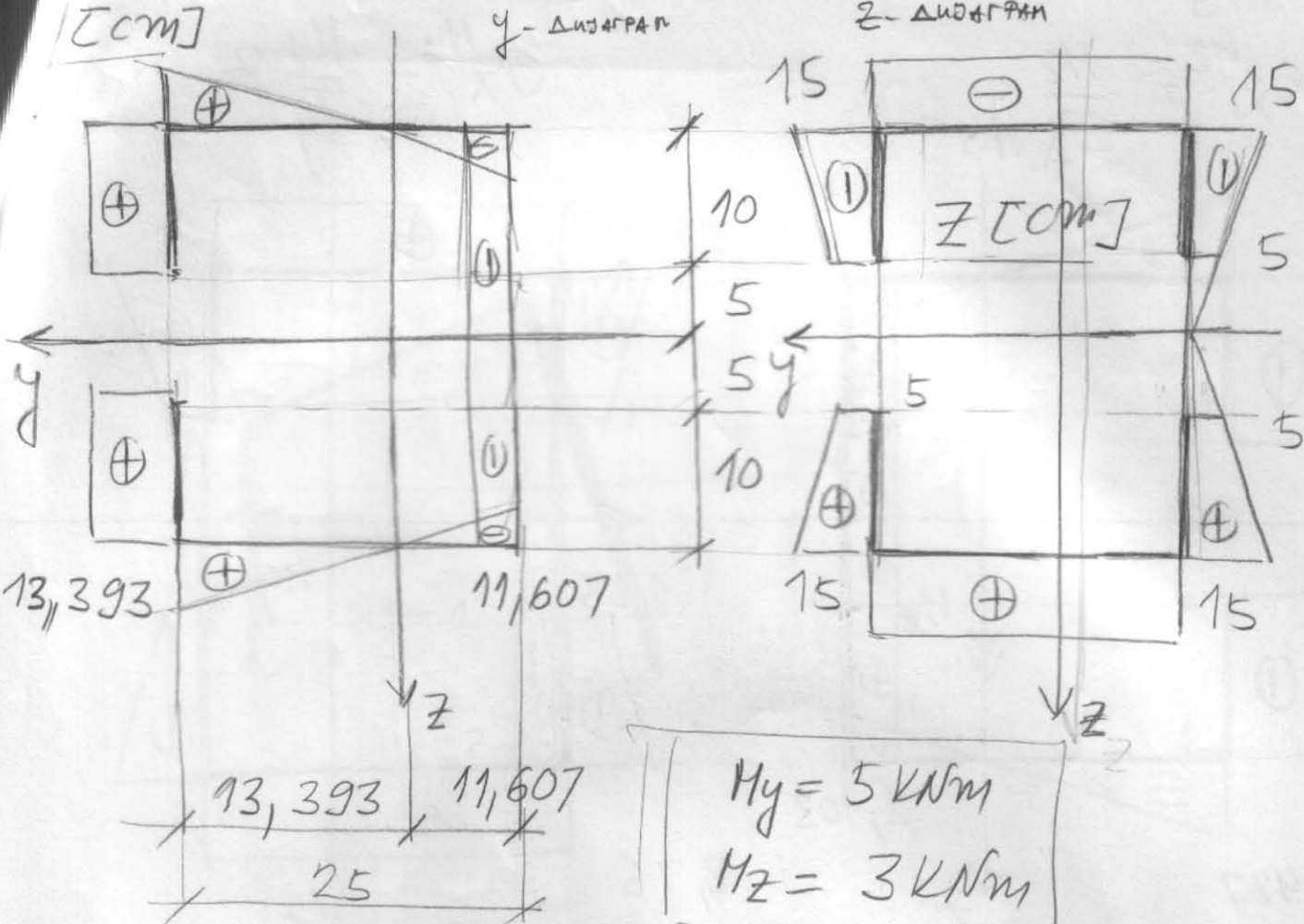
$$A_5 = 20 \quad \bar{T}_5(0; -10)$$

$$A_6 = 20 \quad \bar{T}_6(0; 10)$$

$$A_7 = 10 \quad \bar{T}_7(0; 0)$$

$$A = 140$$

$$y_{\bar{T}} = \frac{20 \cdot 25 \cdot 2 + 25 \cdot 12,5 \cdot 2}{140} = 11,607$$



$$M_y = 5 \text{ kNm}$$

$$M_z = 3 \text{ kNm}$$

$$I_z = \int y^2 t ds = 2 \cdot 2 \cdot (13,393 \cdot 10) \cdot 13,393 +$$

$$+ 2 \cdot 1 \cdot \frac{1}{2} (13,393 - 13,393) \cdot \frac{2}{3} \cdot 13,393 +$$

$$+ 2 \cdot 1 \cdot \frac{1}{2} (11,607 \cdot 11,607) \cdot \frac{2}{3} \cdot 11,607 +$$

$$+ 2 \cdot 2 \cdot (11,607 \cdot 10) \cdot 11,607 + 10 (11,607 \cdot 10) \cdot 11,607$$

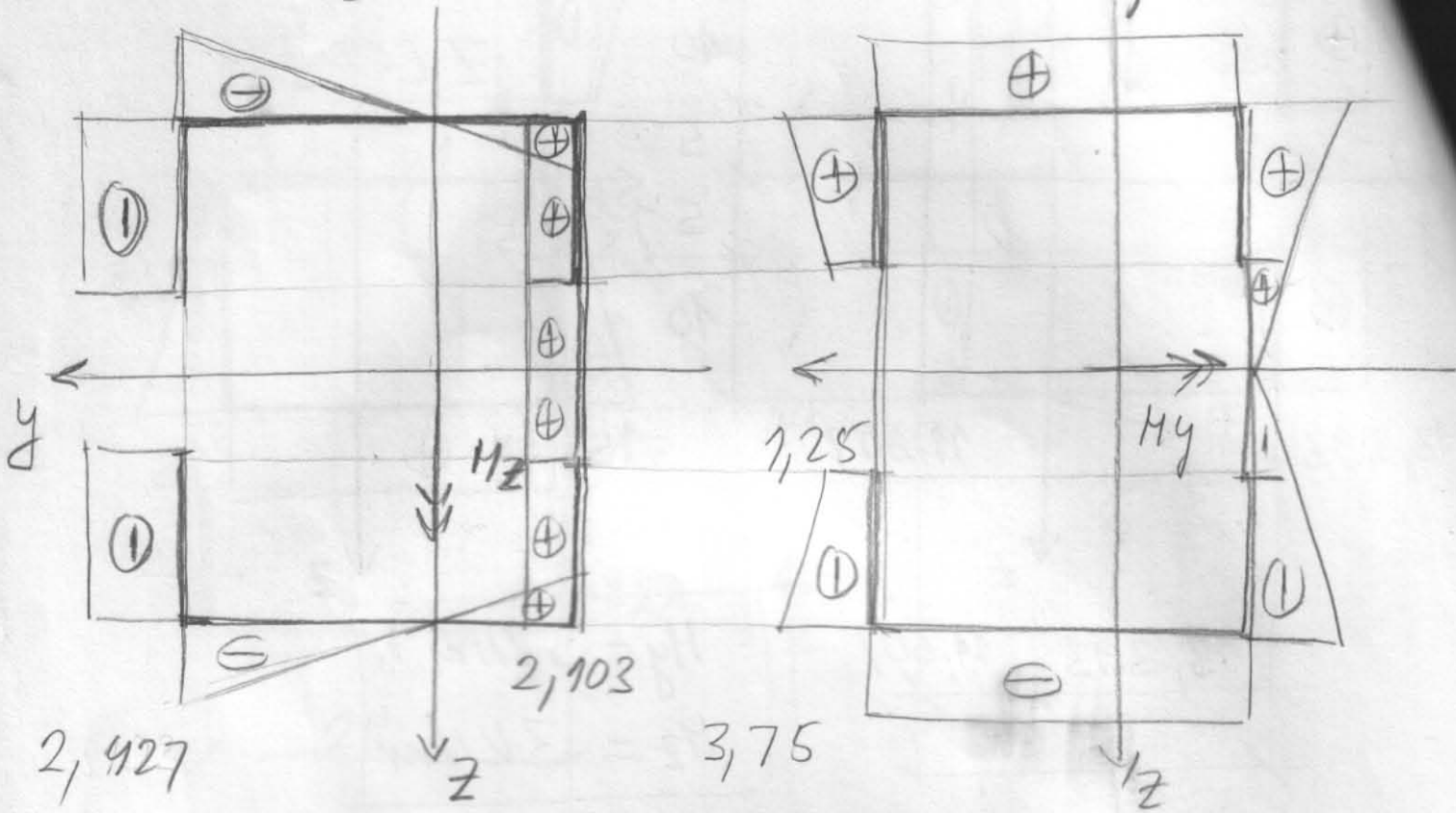
$$I_z = 16555,06 \text{ cm}^4$$

$$I_y = 4 \cdot 2 \cdot \frac{10}{6} [5(2 \cdot 5 + 15) + 15(2 \cdot 15 + 5)] +$$

$$+ 2 \cdot 1 \cdot (15 \cdot 25) \cdot 15 + 2 \cdot 1 \cdot \left(\frac{1}{2} \cdot 5 \cdot 5\right) \cdot \frac{2}{3} \cdot 5 = \underline{\underline{20000 \text{ cm}^4}}$$

$$\sigma_x^{Mz} = \frac{Mz}{I_z} y$$

$$\sigma_x^{My} = \frac{My}{I_y} z$$



$$\sigma_x^{Mz} = \frac{300 \text{ kNm}}{16555,06 \text{ cm}^4} \cdot 11,607 \text{ cm} = 2,103 \text{ MPa}$$

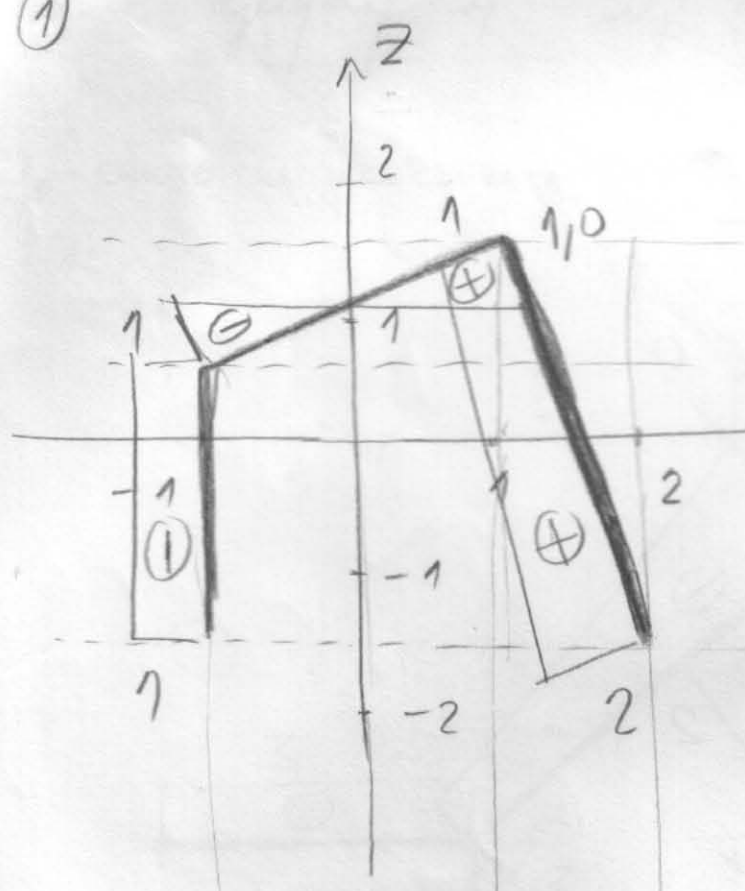
$$13,393 \text{ cm} = 2,427 \text{ MPa}$$

$$\sigma_x^{My} = \frac{500 \text{ kNm}}{20000 \text{ cm}^4} \cdot 5 \text{ cm} = 1,25$$

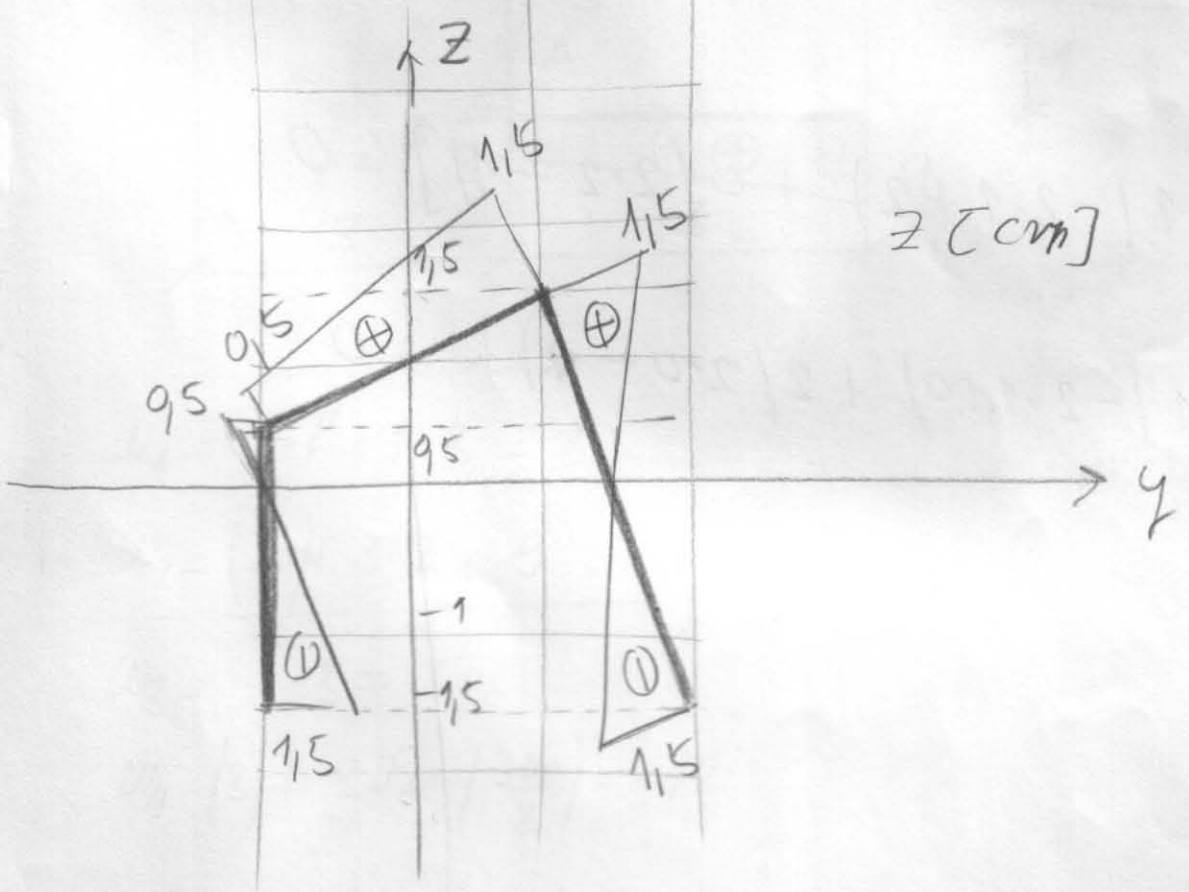
$$15 \text{ cm} = 3,75$$

1

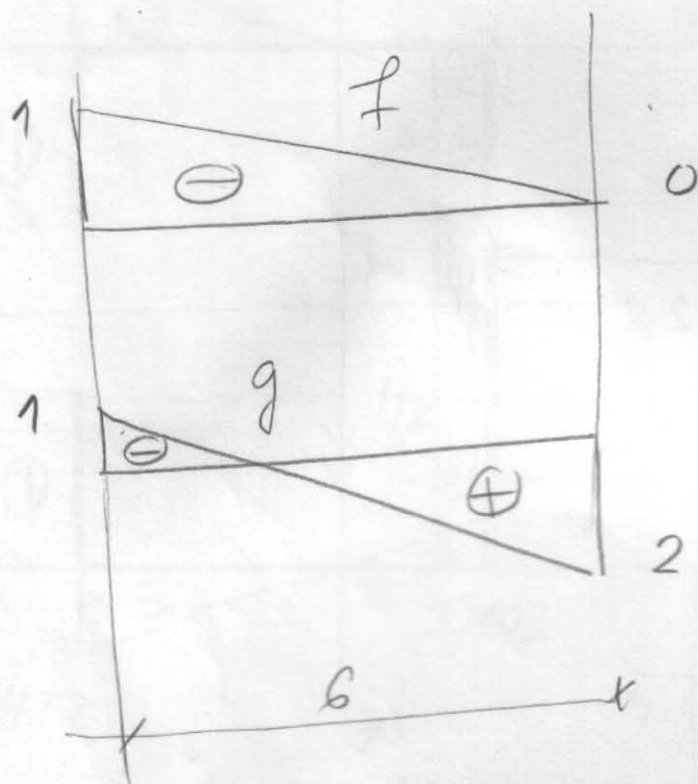
y [cm]



z [cm]



$$(2) \int f \cdot g \, ds$$



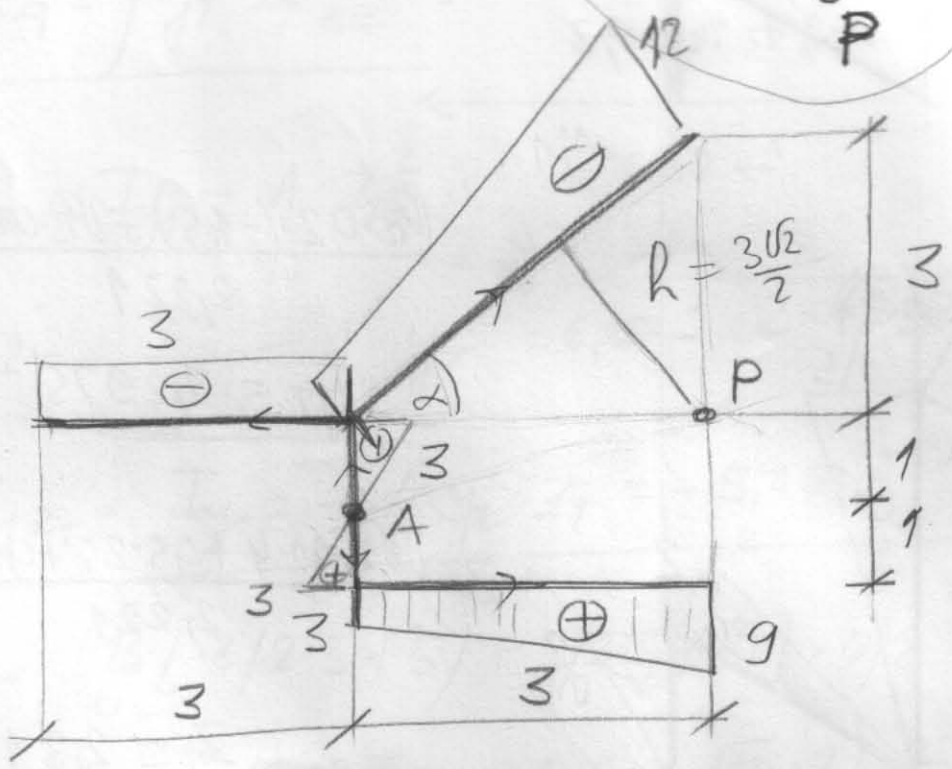
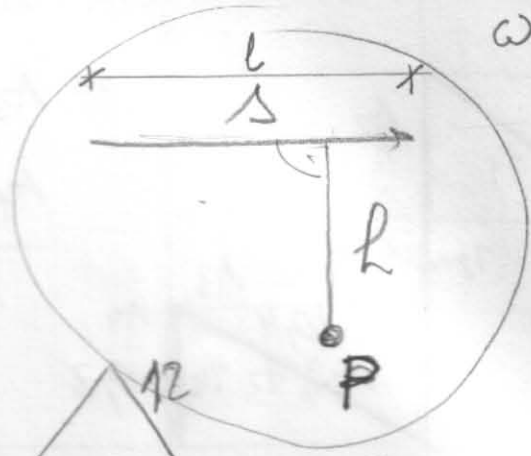
$$\frac{6}{6} [-1(-2 \cdot 1 + 2) + 0(2 \cdot 2 - 1)] = 0$$

$$\frac{6}{6} [-1(-2 \cdot 1 + 0) + 2(2 \cdot 0 - 1)] = 0$$

3. гравитационна $\omega_p^{(A)} = s \cdot h$

$\omega_p^{(A)} = s \cdot h = l \cdot h$

ω_p - СЕКТОРСКА КООРДИНАТА



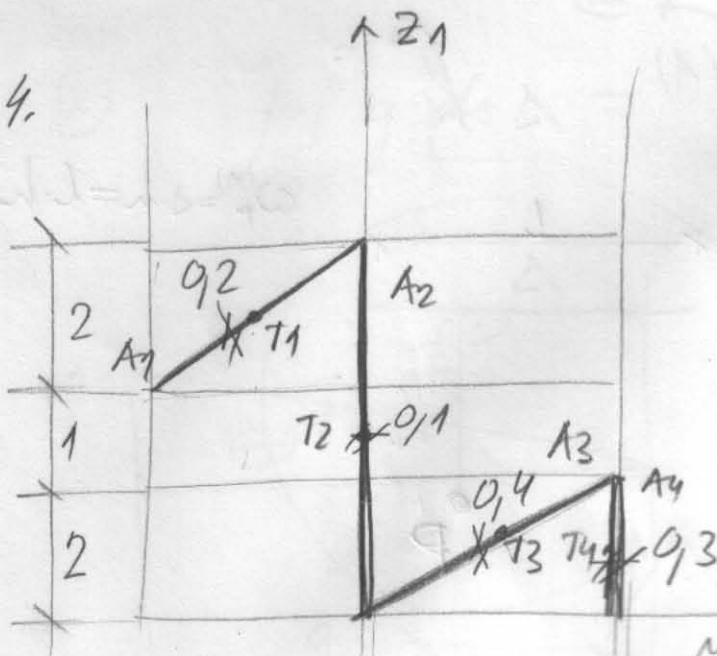
$\omega_1 = s \cdot h = 1 \cdot 3 = 3$

$\omega_2 = (3) + 3 \cdot 2 = 9$

$\omega_3 = 1 \cdot 3 = 3$

$\omega_4 = (3) + 3\sqrt{2} \cdot \left| \frac{3\sqrt{2}}{2} \right| = 12$

4.



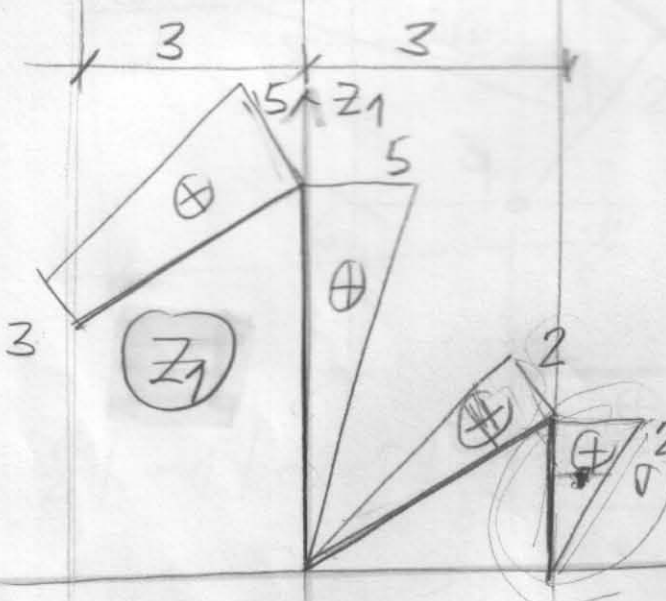
$$A_1 = \sqrt{13} \cdot 0,2 \quad T_1 / -1,5; 4$$

$$A_2 = 5 \cdot 0,1 = 0,5 \quad T_2 / 0; 2,5$$

$$A_3 = \sqrt{13} \cdot 0,4 \quad T_3 / 1,5; 1$$

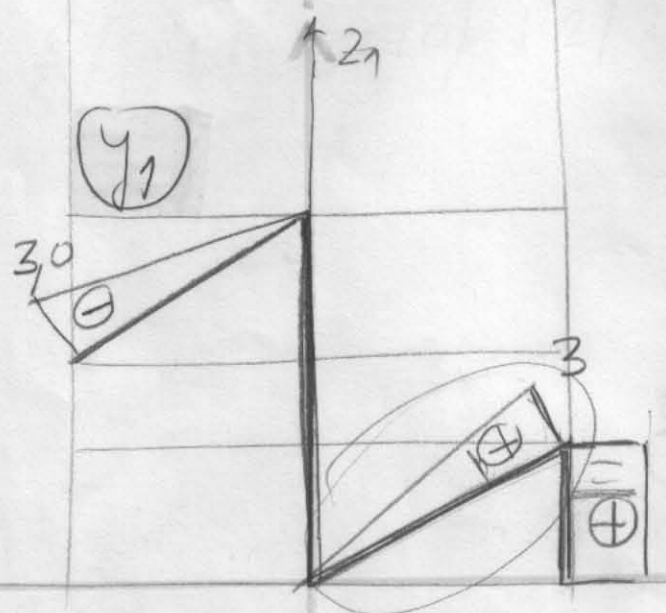
$$A_4 = 2 \cdot 0,3 = 0,6 \quad T_4 / 3; 1$$

$$A = 2,221$$



$$M_T = \frac{\sqrt{13} \cdot 0,2 \cdot (-1,5) + \sqrt{13} \cdot 0,4 \cdot 1,5 + 0,6}{2,221}$$

$$M_T = 1,2975$$



$$Z_T = \frac{\sqrt{13} \cdot 0,2 \cdot 4 + 0,5 \cdot 2,5 + 0,4 \cdot 1 + 0,6}{2,221}$$

$$Z_T = 2,312$$

$$I_{y_1} = \int z_1^2 \underline{t} ds$$

$$I_{z_1} = \int y_1^2 \underline{t} ds$$

$$I_{y_1 z_1} = \int y_1 \cdot z_1 \underline{t} ds$$

$$I_{y_T} = I_{y_1} - A \cdot z_T^2 = 6,80 \text{ cm}^4$$

$$I_{z_T} = I_{z_1} - A \cdot y_T^2 = 6,35 \text{ cm}^4 \text{ забрызано!}$$

$$I_{y z_T} = I_{y_1 z_1} - A \cdot y_T \cdot z_T = -5,95 \text{ cm}^4$$

$$I_{y_1} = \frac{\sqrt{13}}{6} [3/2 \cdot 3 + 5] + 5/2 \cdot 5 + 3] \cdot 0,2 +$$

$$+ \left(\frac{1}{2} \cdot 5 \cdot 5 \right) \cdot \frac{2}{3} \cdot 5 \cdot 0,1 + \left(\frac{1}{2} \sqrt{13} \cdot 2 \right) \cdot \frac{2}{3} \cdot 2 \cdot 0,4 +$$

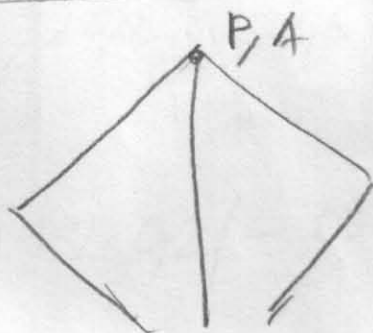
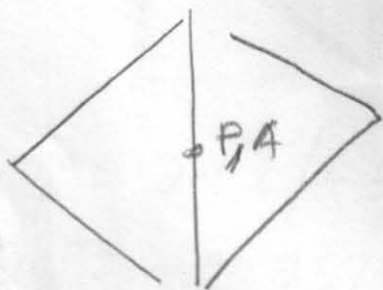
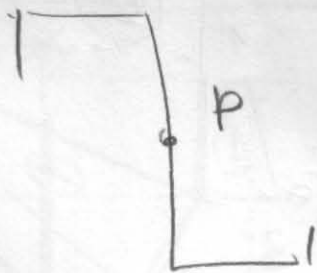
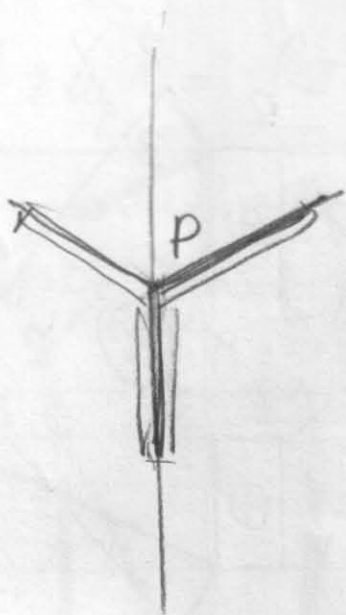
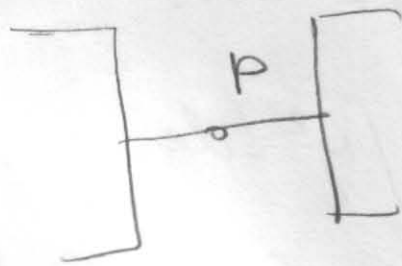
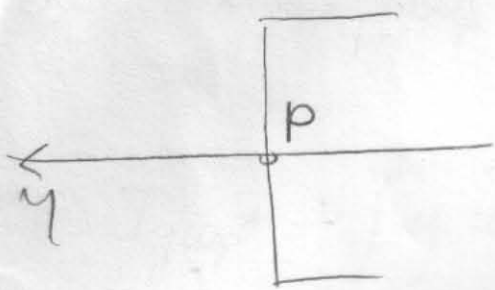
$$+ \left(\frac{1}{2} \cdot 2 \cdot 2 \right) \cdot \frac{2}{3} \cdot 2 \cdot 0,3 = 18,67 \text{ cm}^4 \checkmark$$

$$I_{z_1} = \left(\frac{1}{2} \sqrt{13} \cdot 3 \right) \cdot \frac{2}{3} \cdot 3 \cdot 0,2 + \left(\frac{1}{2} \sqrt{13} \cdot 3 \right) \cdot \frac{2}{3} \cdot 3 \cdot 0,4 +$$

$$+ (2 \cdot 3) \cdot 3 \cdot 0,3 = 10,09 \text{ cm}^4 \checkmark$$

$$I_{y_1 z_1} = - \frac{\sqrt{13}}{6} [3/2 \cdot 3 + 5] \cdot 0,2 + \left(\frac{1}{2} \sqrt{13} \cdot 3 \right) \cdot \frac{2}{3} \cdot 2 \cdot 0,4 +$$

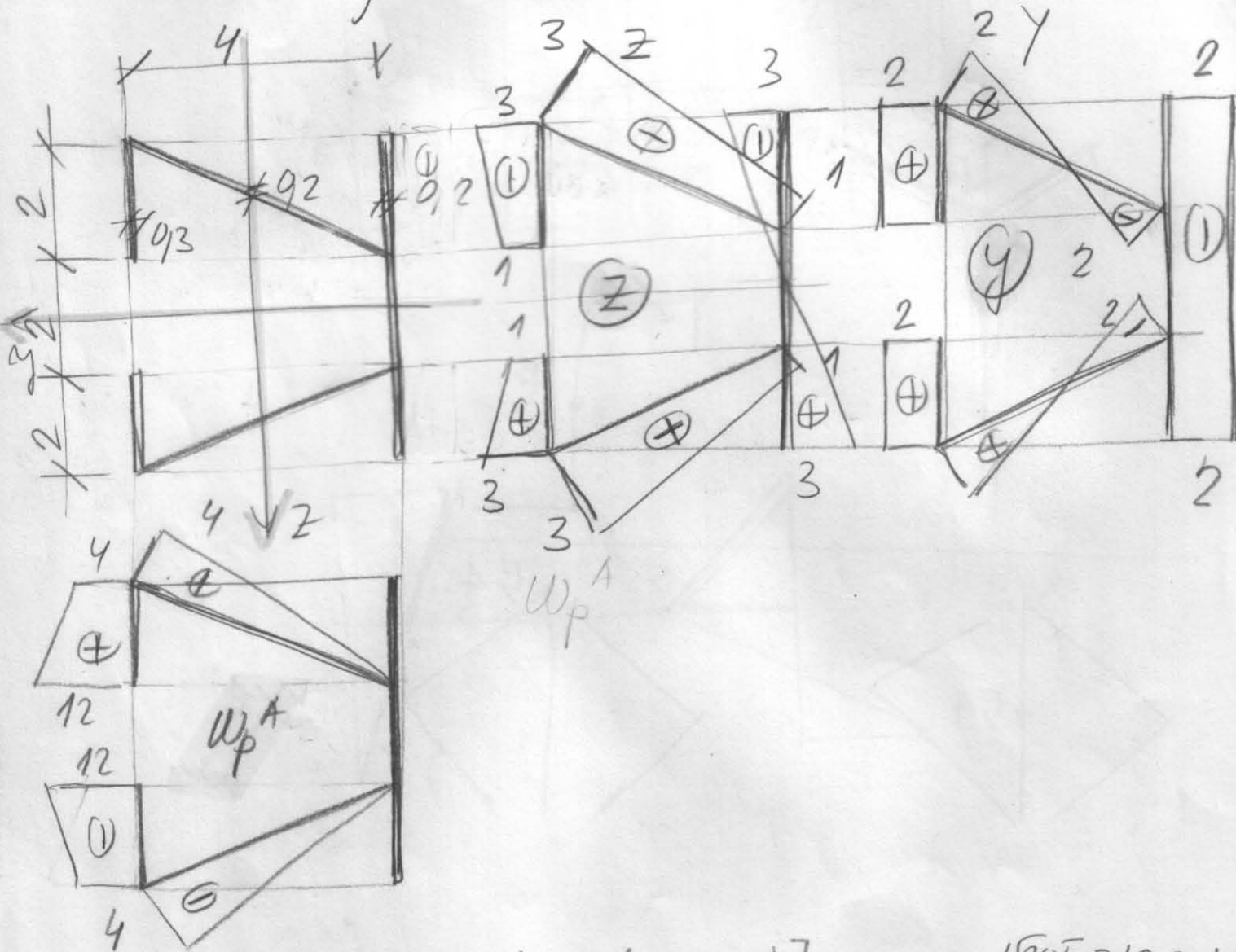
$$+ \left(\frac{1}{2} \cdot 2 \cdot 2 \right) \cdot 3 \cdot 0,3 = 0,718 \text{ cm}^4 \checkmark$$



$$6. \quad I_y = \int z^2 t ds$$

$$I_z = \int y^2 t ds$$

$$I_{zw} = \int z \cdot w \cdot t ds$$



$$I_y = 2 \cdot \frac{2}{6} [1/2 \cdot 1 + 3] + 3 [2 \cdot 3 + 1] \cdot 0,3 + 2 \cdot \frac{\sqrt{20}}{6} [3/2 \cdot 3 + 1/2 \cdot 1 + 3] \cdot 0,2 + 2 \cdot \left(\frac{1}{2} \cdot 3 \cdot 3 \right) \cdot \frac{2}{8} \cdot 3 \cdot 0,2 = 16,55 \text{ cm}^4$$

$$I_z = 2 \cdot (2 \cdot 2) \cdot 2 \cdot 0,3 + 2 \cdot \frac{\sqrt{20}}{6} [2/2 \cdot 2 - 2] - 2 [-2 \cdot 2 + 2] \cdot 0,2 + (2 \cdot 6) \cdot 2 \cdot 0,2 = 11,985$$

$$I_{zw} = - \frac{2}{6} [12 \cdot 12 \cdot 1 + 3] + 4 [2 \cdot 3 + 1] \cdot 0,3 \cdot 2 - \frac{\sqrt{20}}{6} [4/2 \cdot 3 + 1] \cdot 2 \cdot 0,2 = -25,95 \text{ cm}^4$$

8. y_1, z_1, ω_p^A

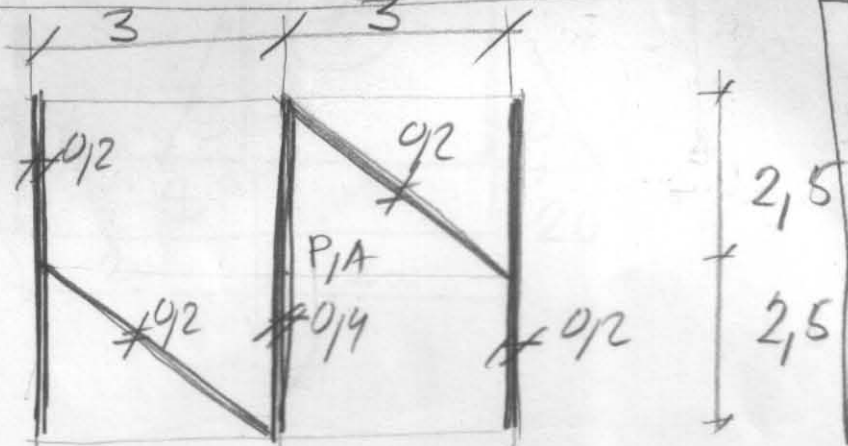
$$I_y \omega_p^A = \int y \cdot \omega_p^A \cdot t \, ds$$

СЕКТОРСКИ ЦЕНТРИФАГАЛНИ МОМЕНТ ИНЕРЦИЈЕ

$$I_z \omega_p^A = \int z \cdot \omega_p^A \cdot t \, ds$$

у центару симетричног пресека
 $\omega = \omega_p^A - \frac{S \omega_p^A}{A}$ цифра

$$S \omega_p^A = \int \omega_p^A \cdot t \, ds$$



$$A = (5 \cdot 0,2) \cdot 2 + 5 \cdot 0,4 + 2 \cdot 3,905 \cdot 0,2 = 5,562 \text{ cm}^2$$

$$S \omega_p^A = 2 \cdot 0,12 \left(-\frac{1}{2} \cdot 15 \cdot 5 \right) + 2 \cdot 0,12 \left(-\frac{1}{2} \cdot 3,905 \cdot 7,5 \right)$$

$$S \omega_p^A = -20,85765 \text{ cm}^4$$

$$\omega_p^A = \Delta \cdot h$$

$$\sin \alpha = \frac{h}{2,5} = \frac{3}{3,905}$$

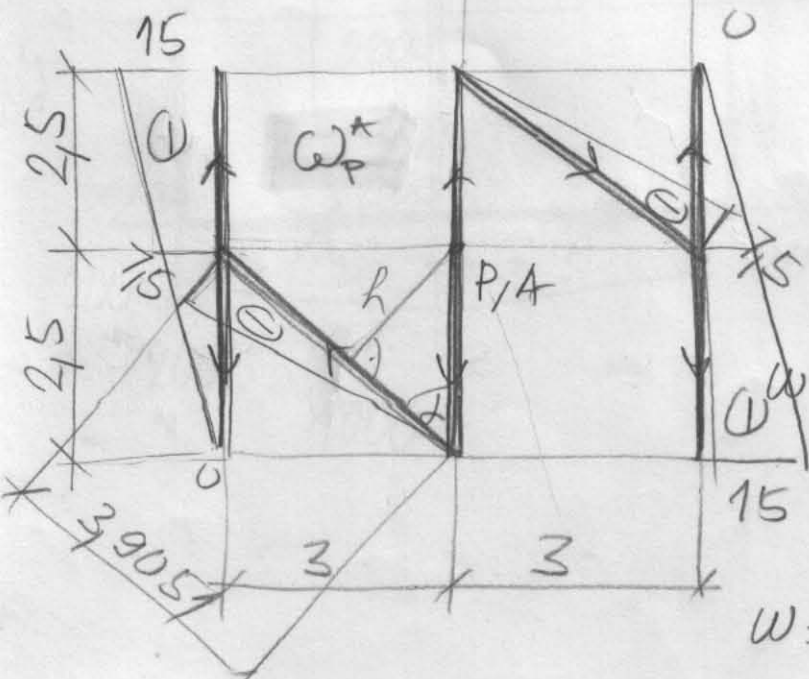
$$h = 1,9206$$

$$\omega = \Delta h = 3,905 \cdot 1,9206 = 7,5$$

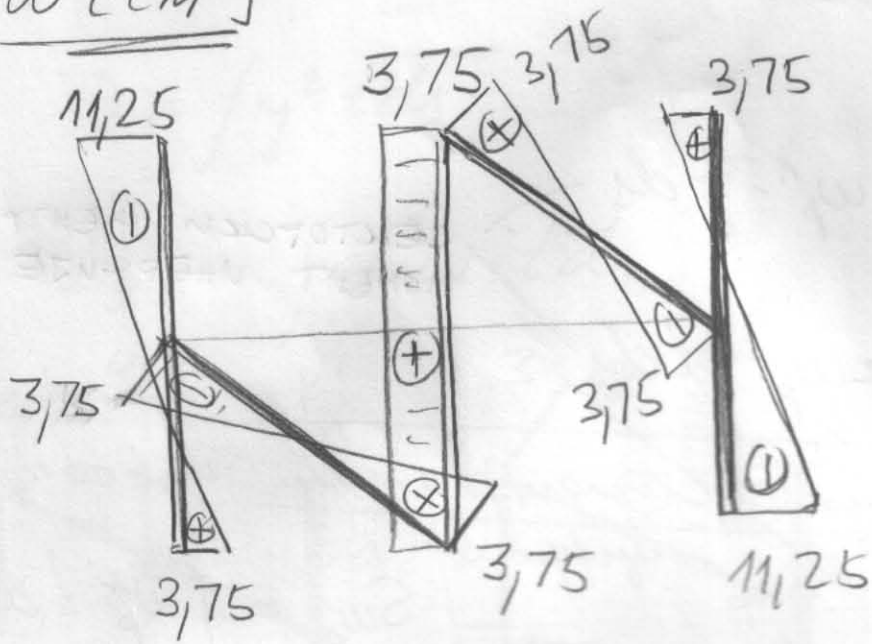
$$\omega = 7,5 + 2,5 \cdot 3 =$$

$$15 \quad \omega = \omega_p^A - \frac{-20,85765 \text{ cm}^4}{5,562 \text{ cm}^2}$$

$$\omega = \omega_p^A + 3,75$$



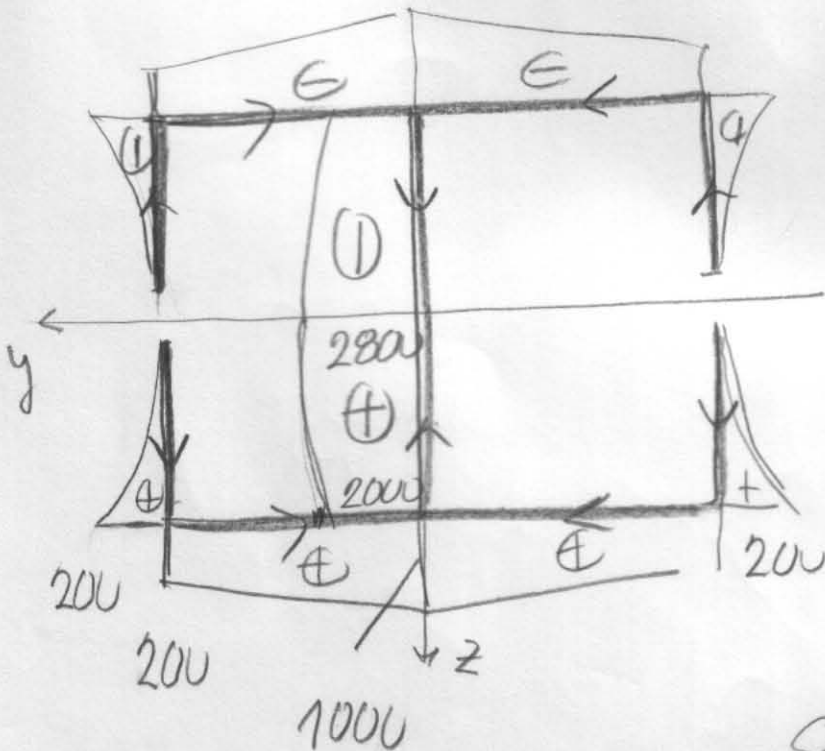
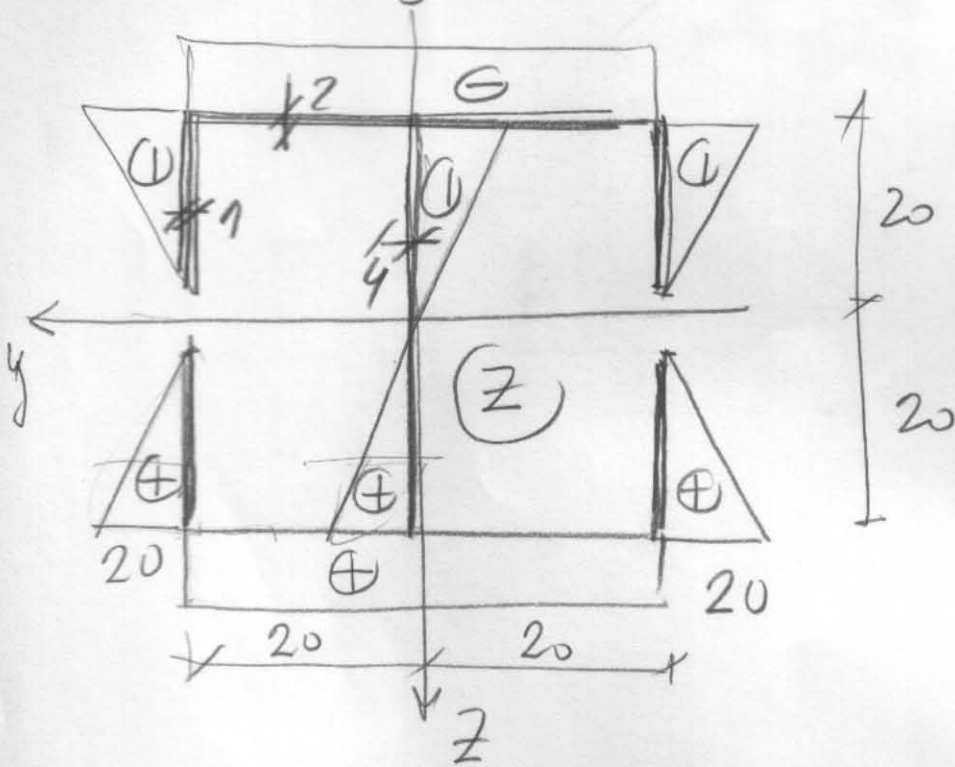
W [cm²]



$$S_y = \int z t ds \rightarrow \text{ог ексцентричних крајеве}$$

$$S_z = \int y t ds \rightarrow \text{СТАТИЧКИ МОМЕНТИ ИЛИ ПЕРЦЕНТЕ}$$

$$S_w = \int w t ds \rightarrow \text{НОРМАЛНА СЕКТОРСКА КООРДИНАТА (СЕКТОРСКИ СТАТИЧКИ МОМЕНТ)}$$



$$S_y \text{ [cm}^3\text{]}$$

$$S_{y1} = \frac{1}{2} \cdot 20 \cdot 20 \cdot 1 =$$

$$S_{y1} = 200$$

$$S_{y2} = 200 + 20 \cdot 20 \cdot 2 =$$

$$S_{y2} = 1000$$

$$S_{y3} = 2000 + \frac{1}{2} \cdot 20 \cdot 20 \cdot 4$$

Z_x ко линовени ару

капои

$$Z_x^{T_y} = - \frac{T_y \cdot S_z^*}{I_z \cdot t}$$

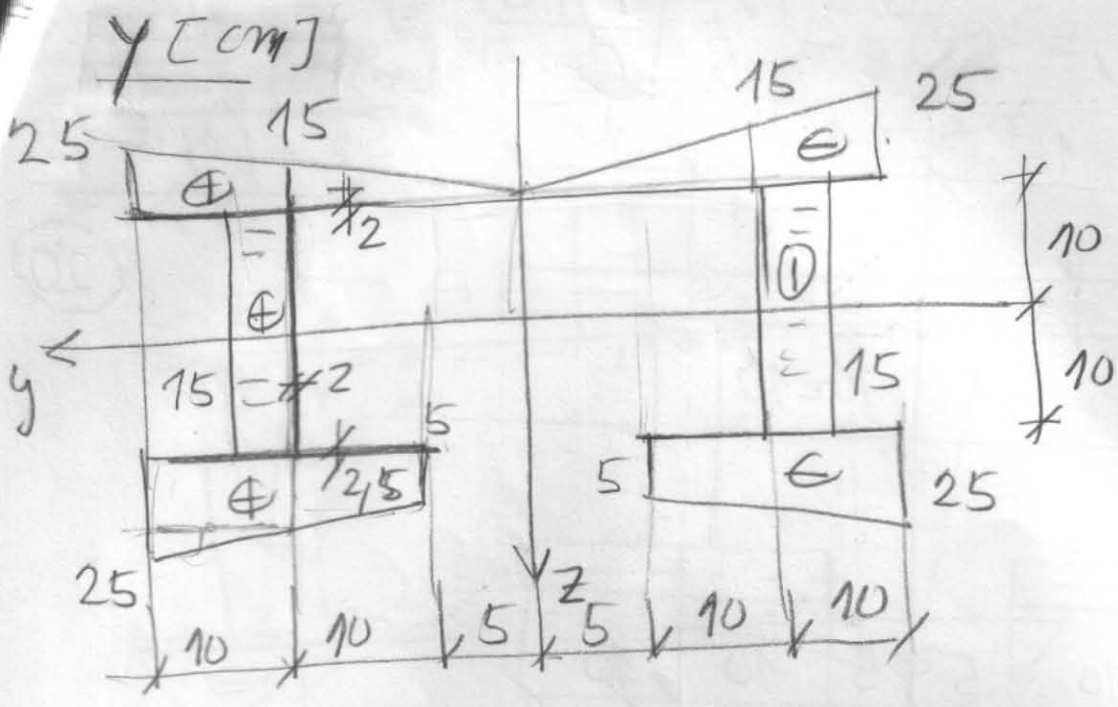
$$S_z^* = \int y t ds$$

$$I_z = \int y^2 t ds$$

$$Z_x^{T_z} = - \frac{T_z \cdot S_y^*}{I_y \cdot t}$$

$$S_y^* = \int z t ds$$

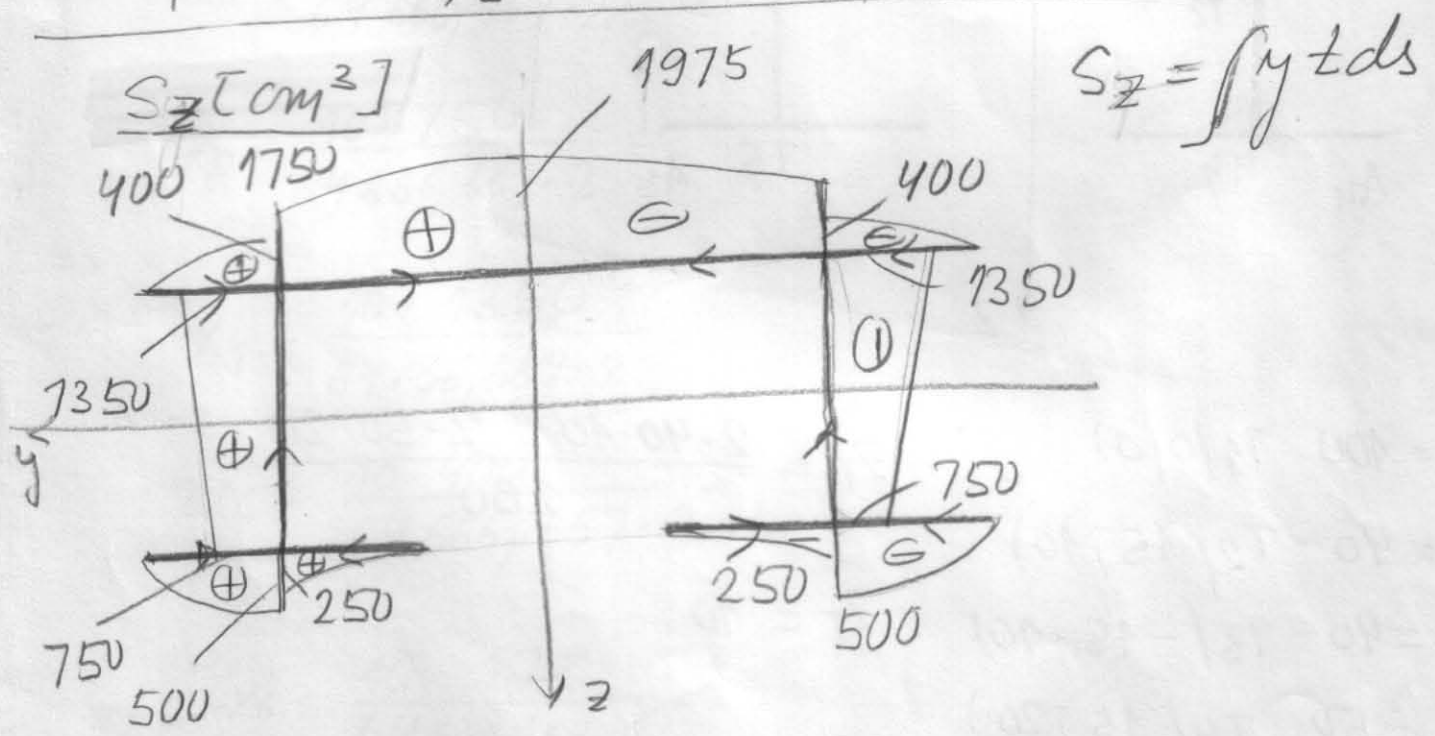
$$I_y = \int z^2 t ds$$



$$I_z = \int y^2 t ds = 2 \left(\frac{1}{2} \cdot 25 \cdot 25 \right) \cdot \frac{2}{3} \cdot 25 \times 2 +$$

$$+ 2 \cdot (20 \cdot 15) \cdot 15 \times 2 + 2 \cdot 5 \cdot \frac{20}{6} [25 \cdot (2 \cdot 25 + 5) +$$

$$5(2 \cdot 5 + 25)] \times 2 = 64666,667 \text{ cm}^4$$



$$S_z = \int y t ds$$

$$S_{z1} = \frac{15 + 25}{2} \cdot 10 \cdot 2,5 = 500 \quad S_{z2} = \frac{15 + 5}{2} \cdot 10 \cdot 2,5 = 250$$

$$S_{z3} = 750 + 15 \cdot 20 \cdot 2 = 1350 \quad S_{z4} = \frac{15 + 25}{2} \cdot 10 \cdot 2 = 400$$

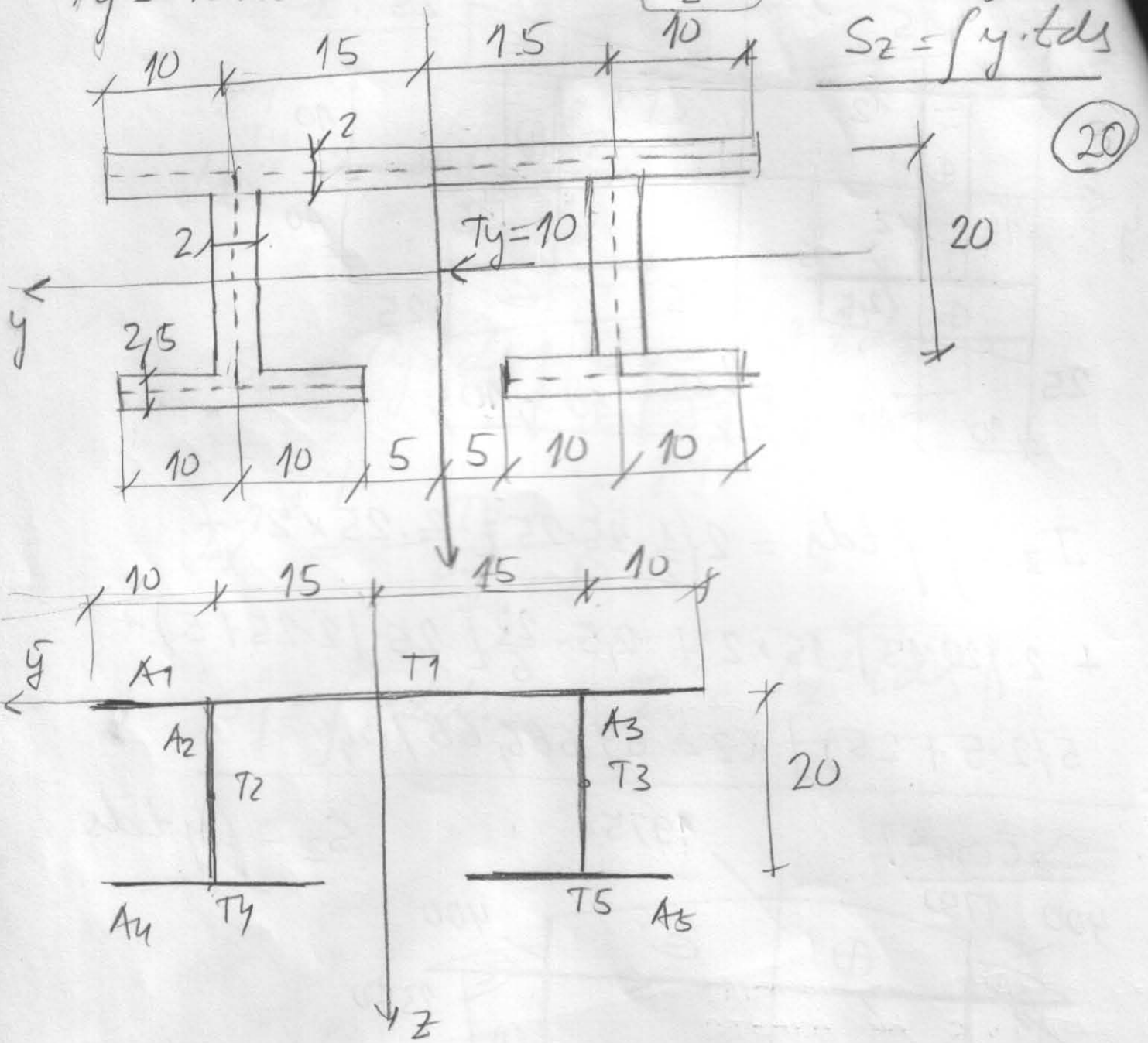
$$S_{z5} = 1750 + \frac{1}{2} \cdot 15 \cdot 15 \cdot 2 = 1975$$

$$T_y = 10 \text{ kN}$$

$$\frac{d^2 T_y}{dx^2} = \frac{T_y \cdot S_z}{I_z \cdot t}$$

$$I_z = \int y^2 t$$

$$S_z = \int y \cdot t \cdot ds$$



$$A_1 = 100 \quad T_1(0|0)$$

$$z_T = \frac{2 \cdot 40 \cdot 10 + 2 \cdot 50 \cdot 20}{280}$$

$$A_2 = 40 \quad T_2(15|10)$$

$$z_T = 10$$

$$A_3 = 40 \quad T_3(-15|10)$$

$$A_4 = 50 \quad T_4(15|20)$$

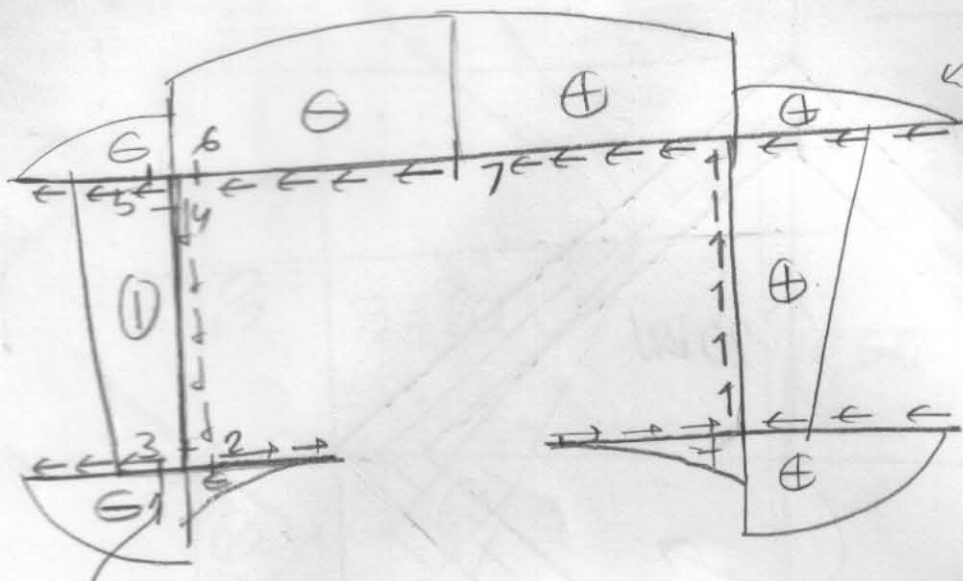
$$A_5 = 50 \quad T_5(-15|20)$$

$$A = 280$$

$$\tau_x^{\tau_y} [\text{MPa}]$$

$$\tau_x = - \frac{T_y \cdot S_z}{I_z \cdot t}$$

(21)



0,309

$$\tau_{x1} = \frac{10 \text{ kN} \cdot 500 \text{ cm}^3}{64666,667 \text{ cm}^4 \cdot 2,5 \text{ cm}} = 0,309 \text{ MPa}$$

$$\tau_{x2} = \frac{10 \cdot 250}{64666,667 \cdot 2,5} =$$

$$\tau_{x3} = \frac{10 \cdot 750}{64666,667 \cdot 2} =$$

$$\tau_{x4} = \frac{10 \cdot 1350}{64666,667 \cdot 2} =$$

$$\tau_{x5} = \frac{10 \cdot 400}{64666,667 \cdot 2} =$$

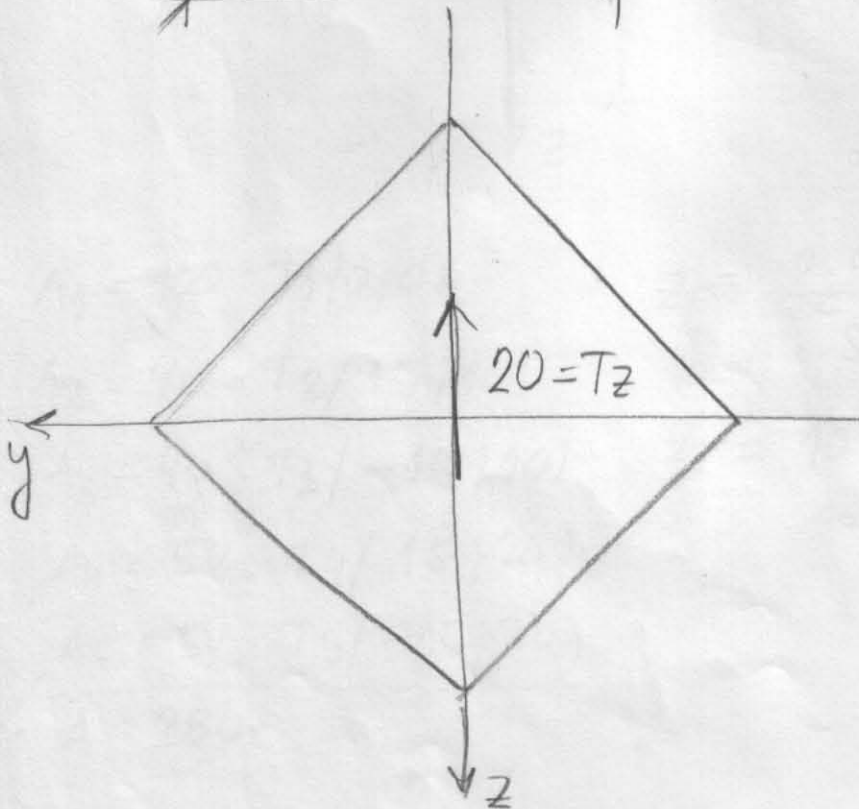
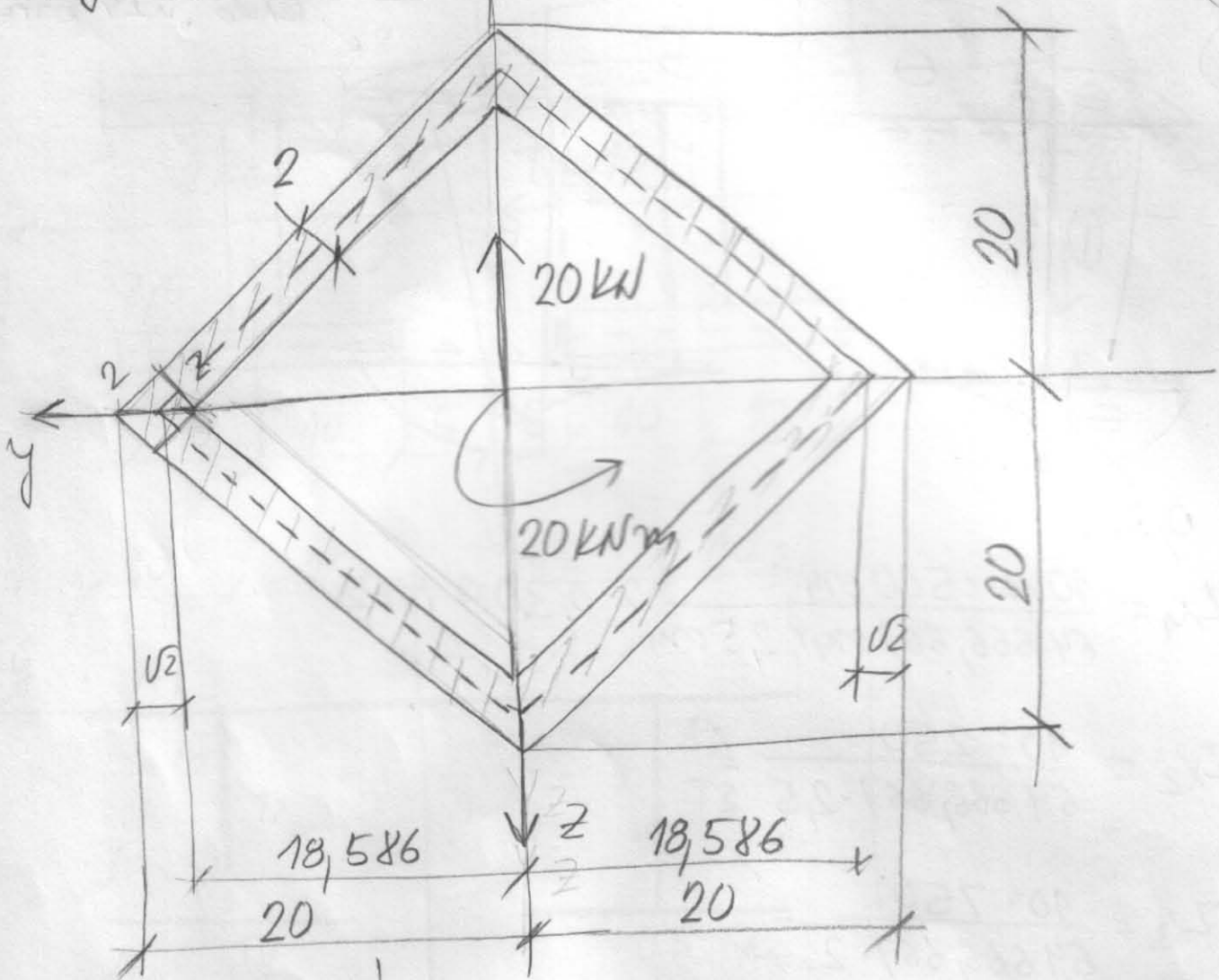
$$\tau_{x6} = \frac{10 \cdot 1750}{64666,667 \cdot 2} =$$

$$\tau_{x7} = \frac{10 \cdot 1975}{64666,667 \cdot 2} =$$

Зачворени танкозидни пресеци

$$I_y = 24395,5 \text{ cm}^4$$

(22)



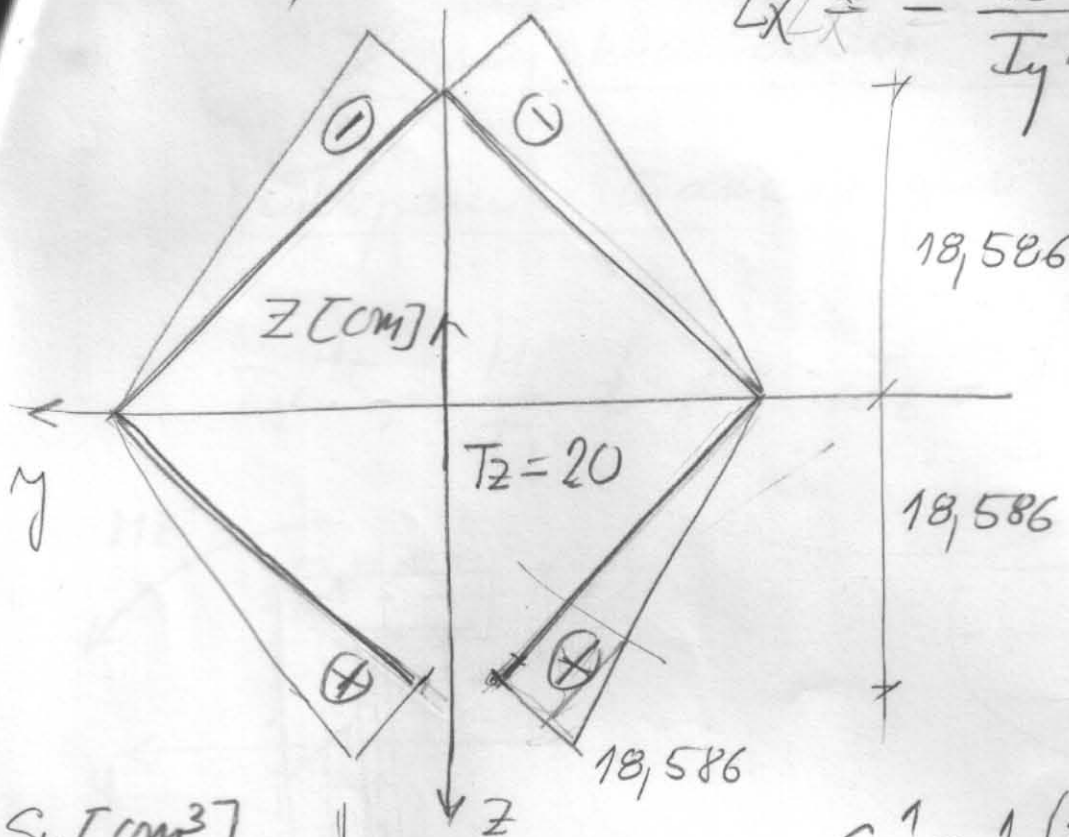
ТАНКОЗИДНИ ПРЕСЕК СЕ
ОТВАРА НА ОСИ НА
КОЈОЈ СЕ НАЛАЗИ
ТРАНСВЕРЗАЛНА СИЛА

18,586

$$I_x = I_y = \frac{Tz^3}{3} = \frac{Tz - S_y}{I_y \cdot t}$$

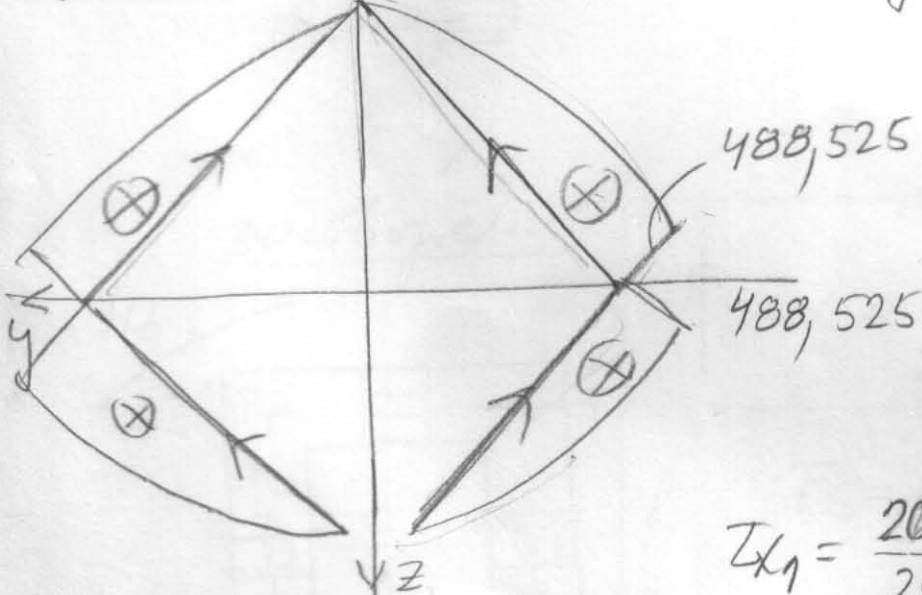
$$S_y = \int z t ds$$

(23)



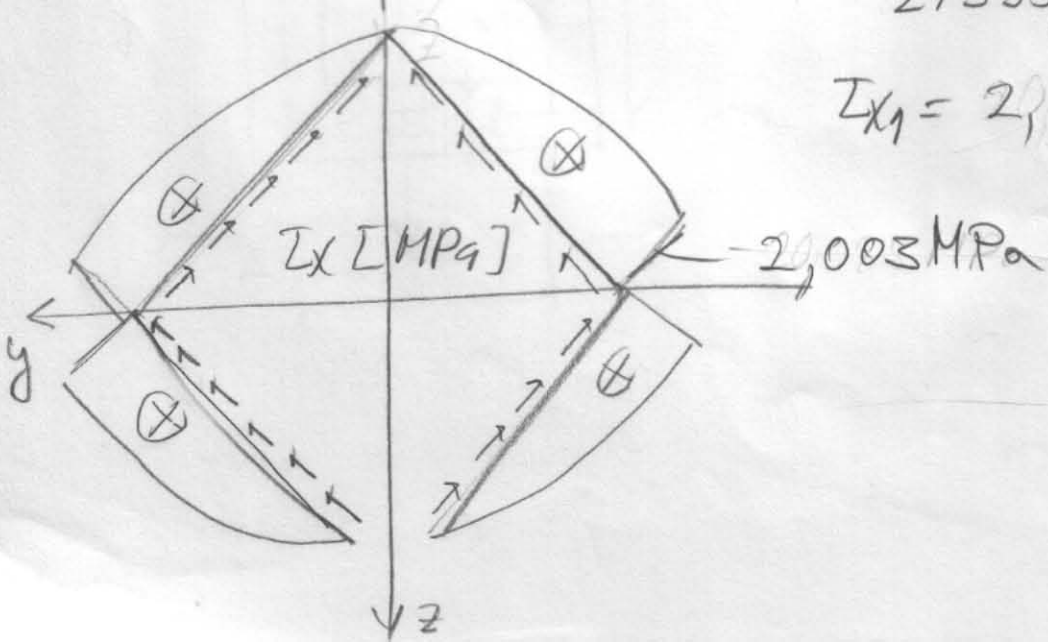
$S_y [cm^3]$

$$S_y^1 = \frac{1}{2} (18,586 \sqrt{2}) \cdot 18,586 \cdot 2$$



$$I_{x1} = \frac{20 \text{ kN} \cdot 488,525 \text{ cm}^3}{24395,5 \text{ cm}^4 \cdot 2 \text{ cm}}$$

$$I_{x1} = 2,003 \text{ MPa} \quad 2,003 \text{ MPa}$$

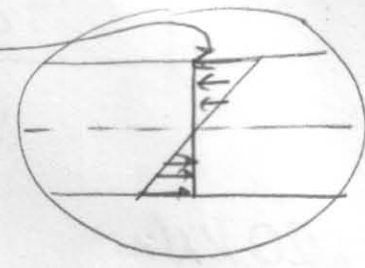
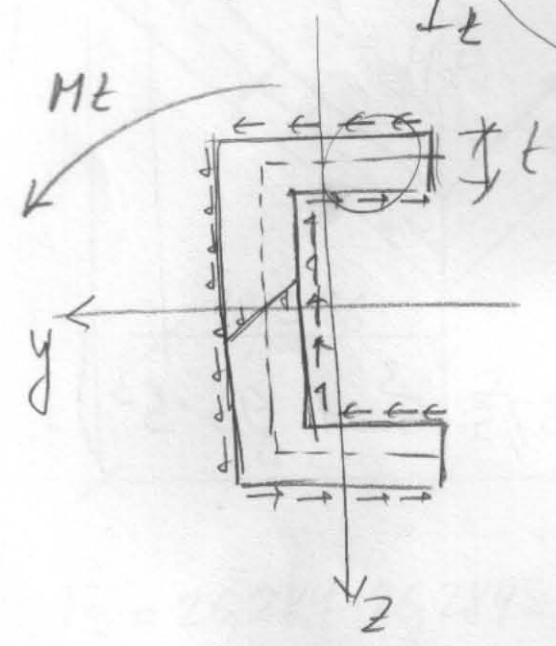


Компоновка и осей Мт

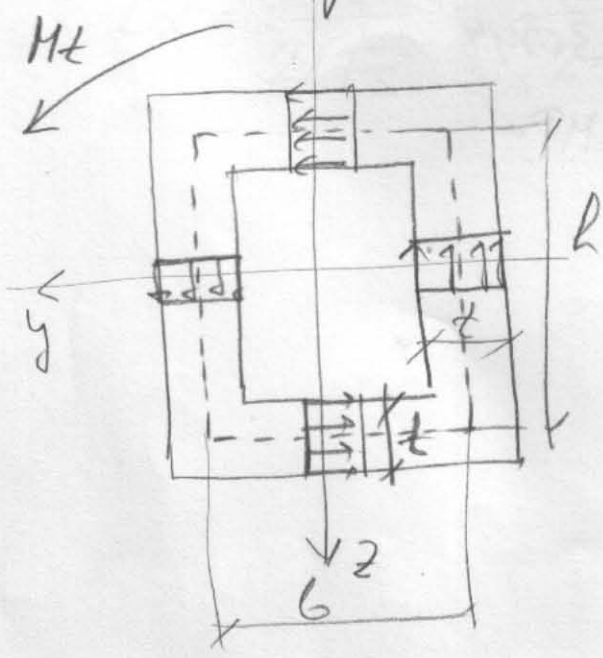
выборем так называемую ось

$$\Sigma X^{Mt} = \frac{Mt}{I_t} \cdot t$$

$$I_t = \frac{1}{3} \Sigma (b_i \cdot t_i^3)$$

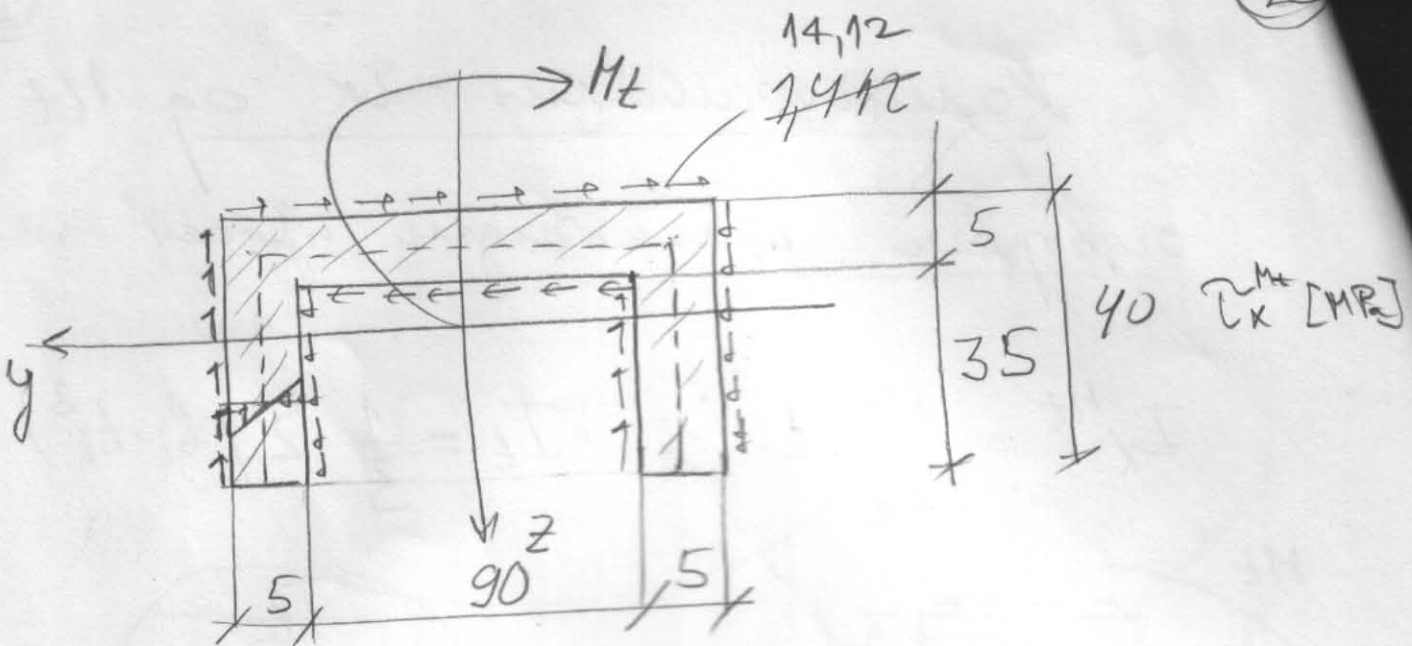


забодем



$$I_x = \frac{M_t}{2t \cdot F_s}$$

$$F_s = b \cdot h$$



$M_z = 20 \text{ kNm}$

$$I_z = \frac{1}{3} \sum (b_i \cdot t_i^3) = \frac{1}{3} \cdot (2 \cdot 37,5 \cdot 5^3 + 95 \cdot 5^3)$$

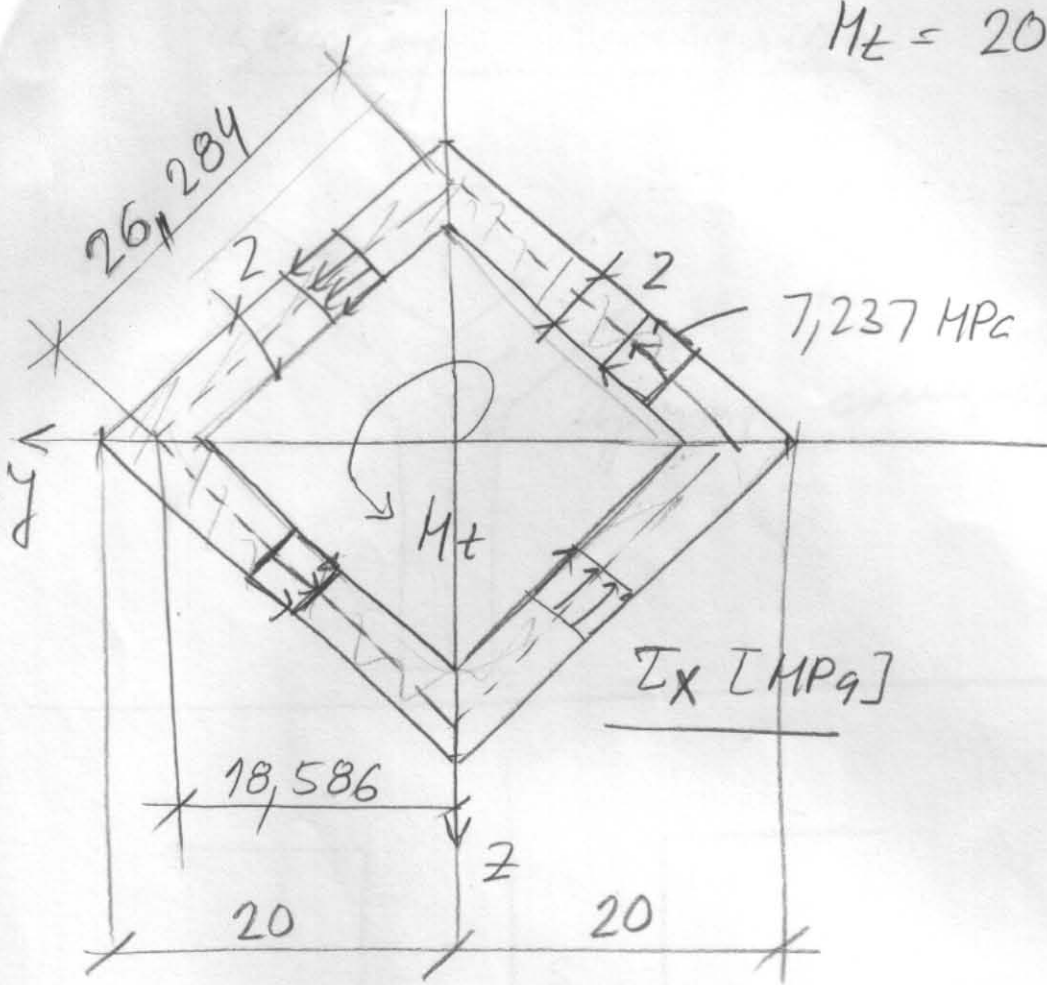
$I_z = 7083,333 \text{ cm}^4$

$$\sigma_{x1} = \frac{M_z}{I_z} \cdot t = \frac{2000 \text{ kNm}}{7083,333 \text{ cm}^4} \cdot 5 \text{ cm}$$

$\sigma_{x1} = 1,412 \frac{\text{kN}}{\text{cm}^2} = 14,12 \text{ MPa}$

$$M_t = 20 \text{ kNm}$$

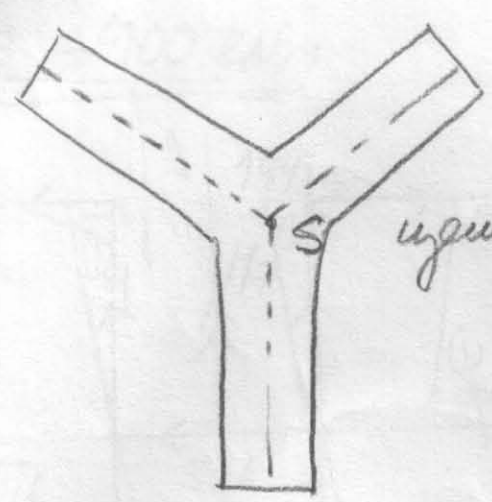
26



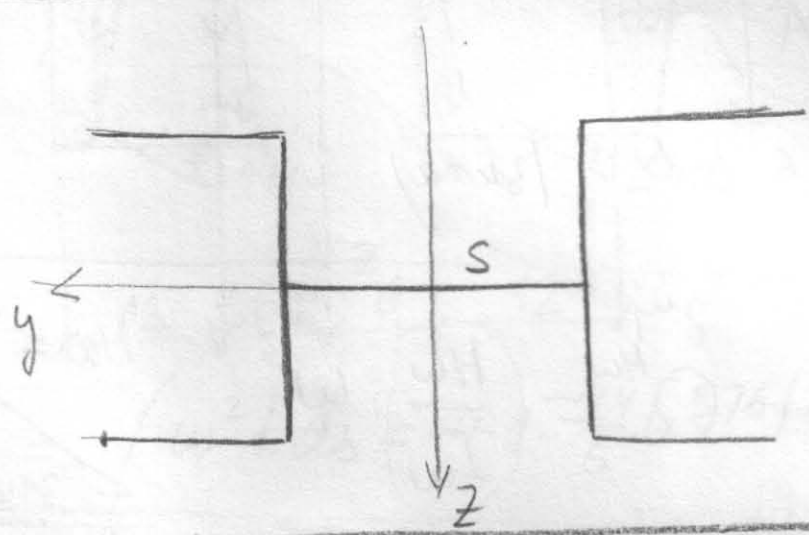
$$F_s = 26,284 \cdot 26,284 = 690,849 \text{ cm}^2$$

$$\tau_x = \frac{M_t}{2 \cdot F_s} = \frac{2000 \text{ kNm}}{2 \cdot 2 \cdot 690,849 \text{ cm}^2} = 7,237 \text{ MPa}$$

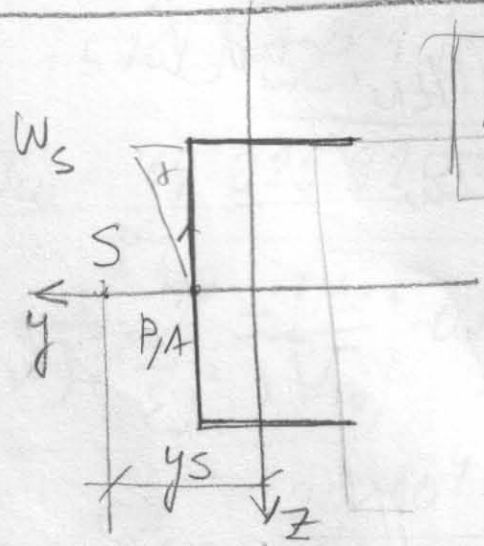
универсальная швеллер



универсальная швеллер



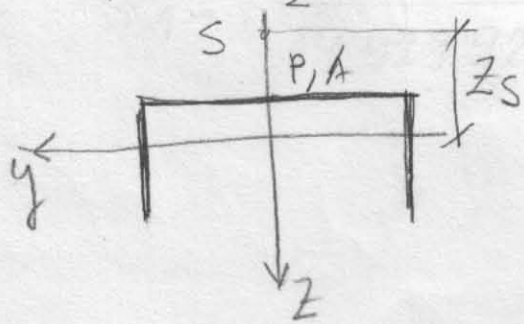
$$w = s \cdot h$$



$$y_s = y_p + \frac{I_{z w_p^A}}{I_y}$$

$$I_y = \int z^2 t ds$$

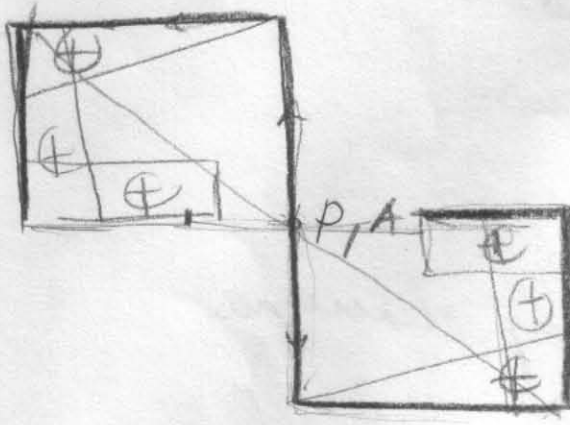
$$I_{z w_p^A} = \int z w_p^A t ds$$



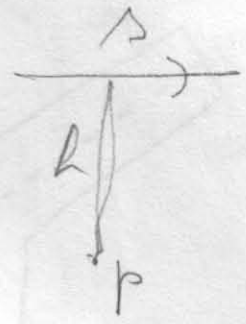
$$z_s = z_p - \frac{I_y w_p^A}{I_z}$$

$$I_y w_p^A = \int y w_p^A t ds$$

$$I_z = \int y^2 t ds$$



$$\omega_p^A [\text{cm}^2] = s \cdot h$$



$$W = \omega_p^A - \frac{S_{\omega_p^A}}{A}$$

$$S_{\omega_p^A} = \int \omega_p^A \cdot t \, ds \quad (\text{знак})$$

$$M_w [\text{KNm}^2]$$

$$\sigma_x = \frac{M_w}{I_w} \cdot w$$

$$M_w = \sum (P_i \cdot w_i)$$

$$M_{tw} [\text{KNm}]$$

$$I_x = - \frac{M_{tw} \cdot S_w}{I_w \cdot t}$$

$$M_{ts} [\text{KNm}]$$

$$I_x = \frac{M_{ts} \cdot t}{I_t}$$

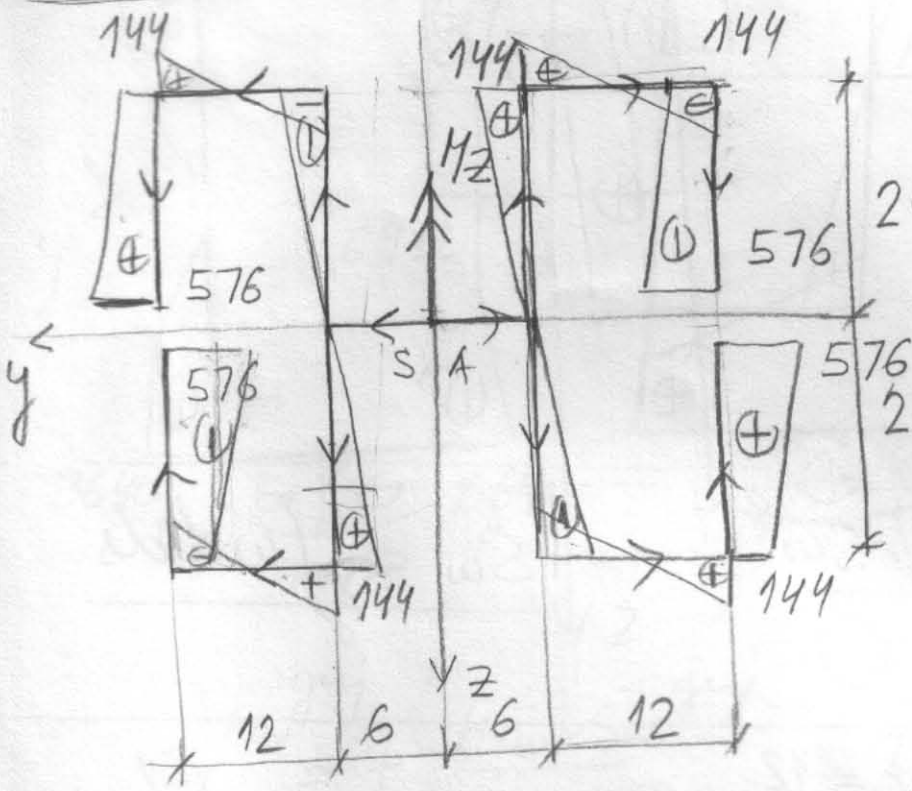
$$I_t = \frac{1}{3} \sum (b_i \cdot d_i^3)$$

$\oplus \leftarrow \omega = \Delta \cdot h$

$M_w = 20 \text{ kNm}^2$

$M_{tw} = -100 \text{ kNm}$

$\omega \text{ [cm}^2\text{]}$



$\omega_1 = 24 \cdot 6 = 144$

$24 \omega_2 = 144 - 12 \cdot 24 = -144$

$\omega_3 = -144 - 24 \cdot 18$

$t = 1 \text{ cm}$

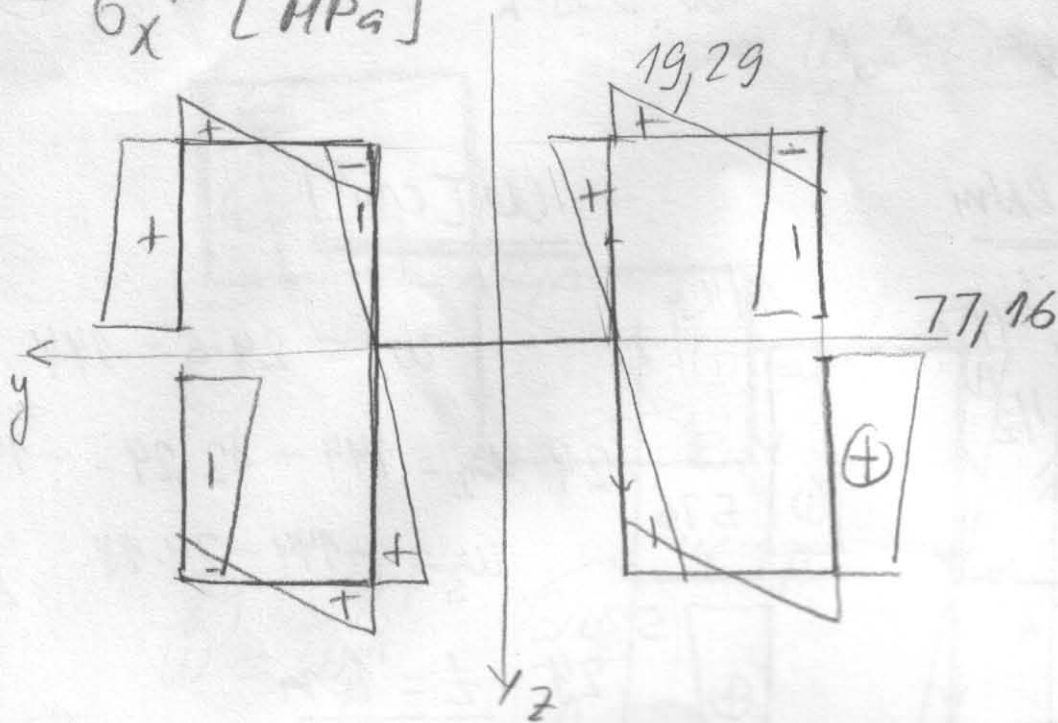
$$I_w = \int \omega^2 t ds = 4 \cdot 1 \cdot \frac{24}{6} [576/2 \cdot 576 + 144] + 144(2 \cdot 144 + 576/2) + 8 \cdot 1 \left(\frac{1}{2} \cdot 6 \cdot 144 \right) \cdot \frac{2}{3} \cdot 144 + 4 \cdot 1 \cdot \left(\frac{1}{2} \cdot 24 \cdot 144 \right) \cdot \frac{2}{3} \cdot 144$$

$I_w = 14\,929\,920 \text{ cm}^6$

$\sigma_x = \frac{M_w}{I_w} \cdot \omega$

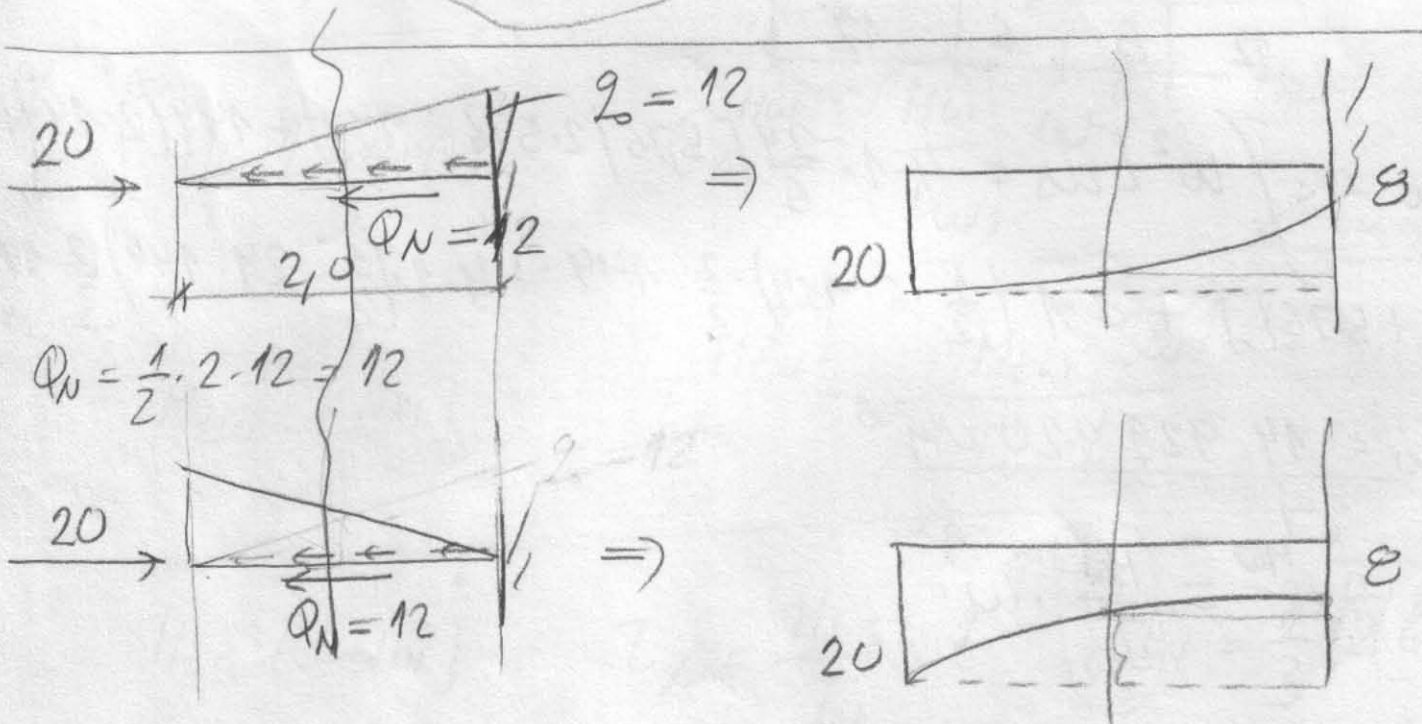
$\sigma_{x1} = \frac{20 \cdot 10^4 \text{ kNm}^2}{14\,929\,920} \cdot (144) = 19,29 \text{ MPa}$
 $\sigma_{x2} = \frac{20 \cdot 10^4 \text{ kNm}^2}{14\,929\,920} \cdot (576) = 77,16 \text{ MPa}$

σ_x [MPa]

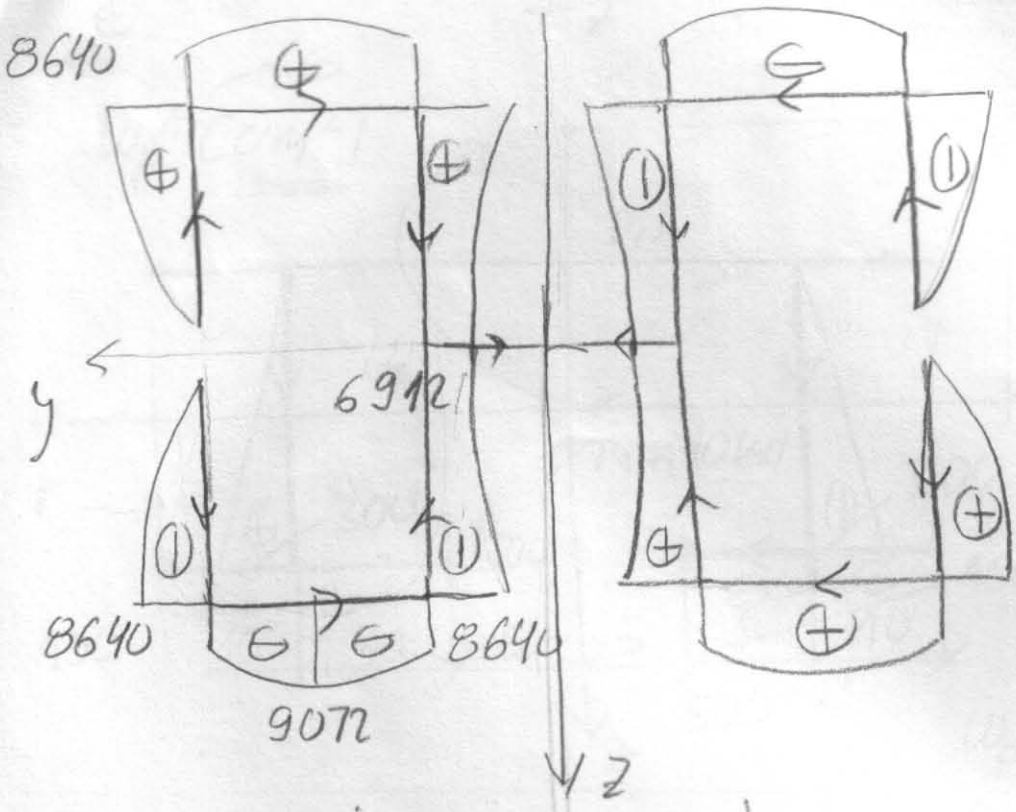


$$\sigma_x = - \frac{M_{tw} \cdot S_w}{I_w \cdot t}$$

$$S_w = \int w t ds$$



$S_w = \int w t ds$ $S_w [cm^4]$



$S_{w1} = \frac{576 + 144 \cdot 24}{2}$

$S_{w2} = 8640 + \frac{1}{2} \cdot 6 \cdot 144$

$S_{w3} = -8640 + \frac{1}{2} \cdot 24 \cdot 144$

$$I_x = - \frac{M_{tw} \cdot S_w \cdot g_{ij}}{I_w \cdot t}$$

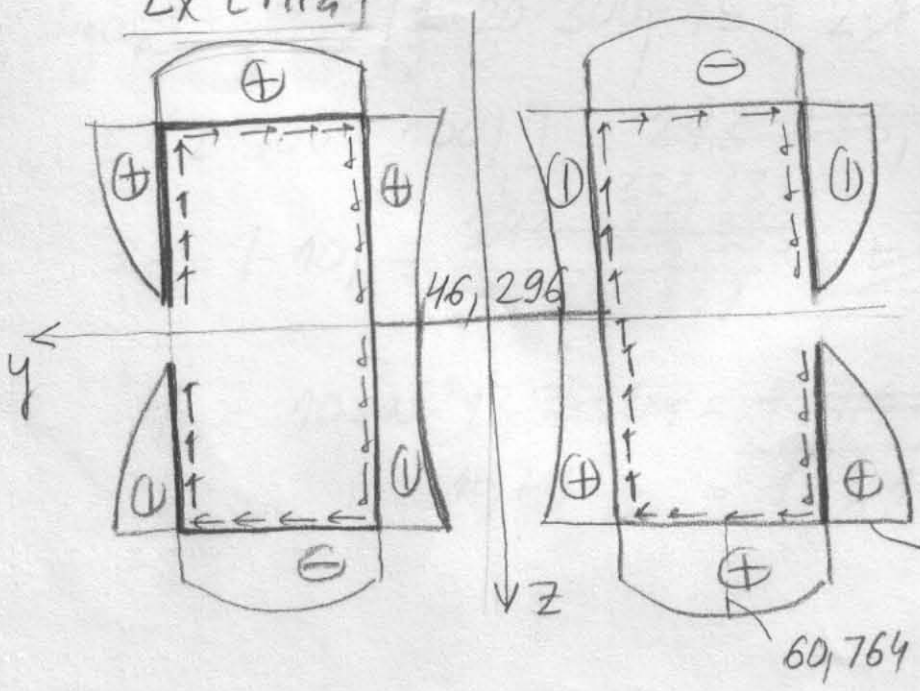
$$I_{x1} = \frac{10000 kNm \cdot 8640}{14929920 cm^6 \cdot 1 cm}$$

$I_x [MPa]$

$I_{x1} = 57,870 MPa$

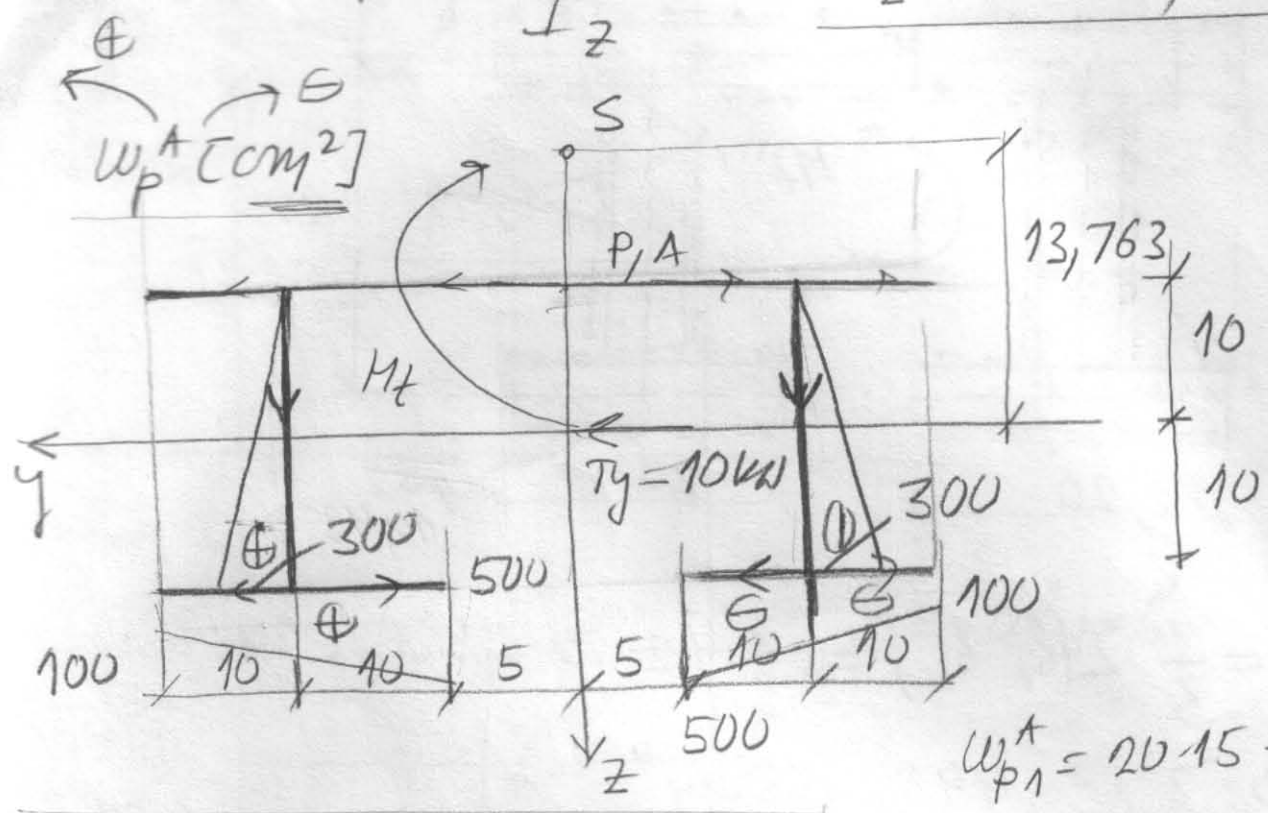
$I_{x2} = \frac{10000}{19072} = 60,764 MPa$

$I_{x3} = \frac{10000}{6912} = 46,296 MPa$



$$z_s = z_p - \frac{I_y w_p^A}{I_z}$$

$$I_z = 64\,666,667 \text{ cm}^4$$



$$w_{p1}^A = 20 \cdot 15 = 300$$

$$w_{p2}^A = 300 + 10 \cdot 20 = 500$$

$$w_{p3}^A = 300 - 10 \cdot 20 = 100$$

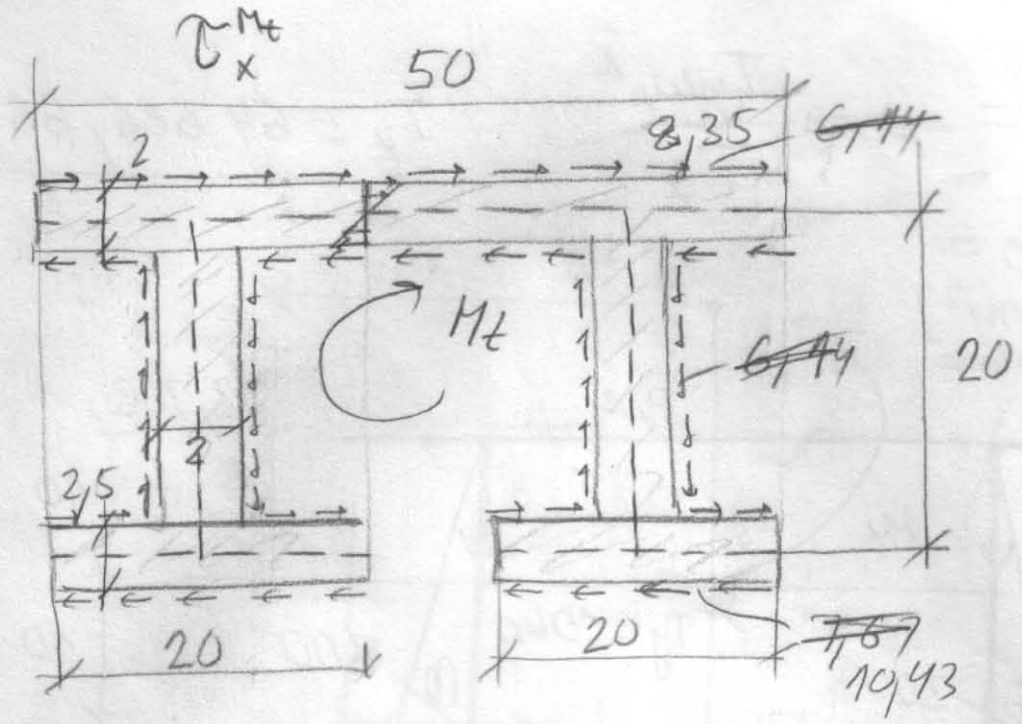
$$I_y w_p^A = \int y \cdot w_p^A \cdot t \, ds$$

$$I_y w_p^A = 2 \left[\frac{1}{2} \cdot (20 - 300) \cdot 15 + 2 \cdot \frac{20}{6} [25 (2 \cdot 100 + 500) + 5 \cdot (2 \cdot 500 + 100)] \right] = 243\,333,333 \text{ cm}^5$$

$$z_s = (-10) - \frac{243\,333,333}{64\,666,667} = -43,763 \text{ cm} - 18,711$$

$$M_t = 10 \text{ kN} \cdot 13,763 \text{ cm} = 137,63 \text{ kNcm}$$

$$18,711 \text{ cm} = 187,11 \text{ kNcm}$$



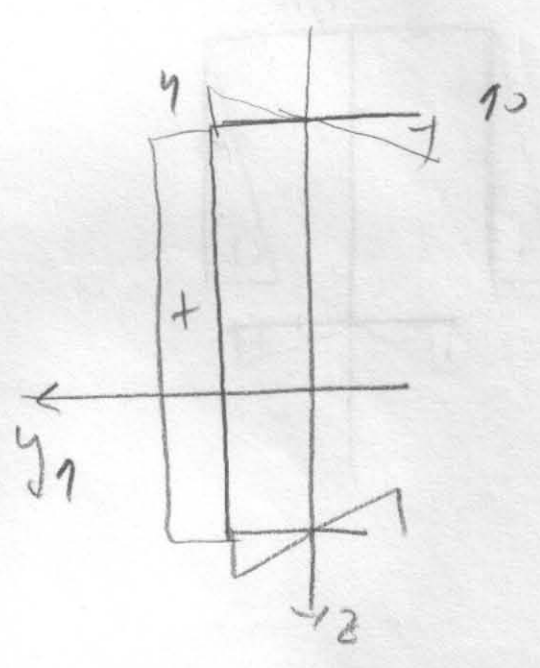
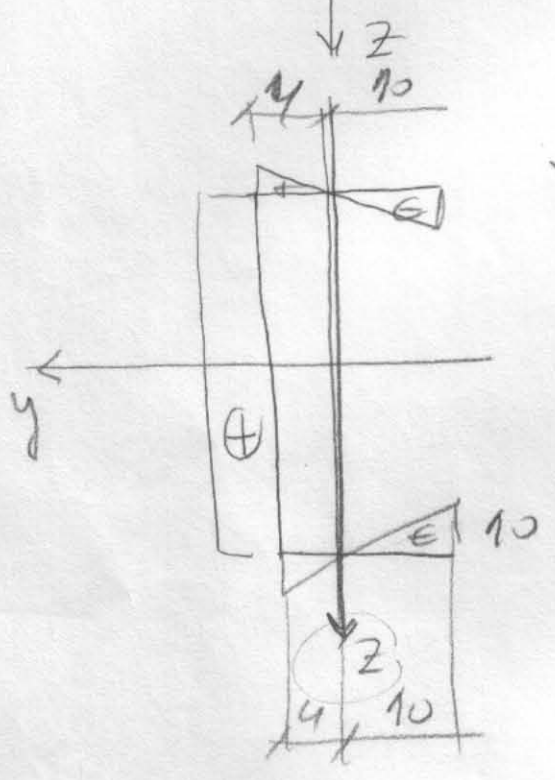
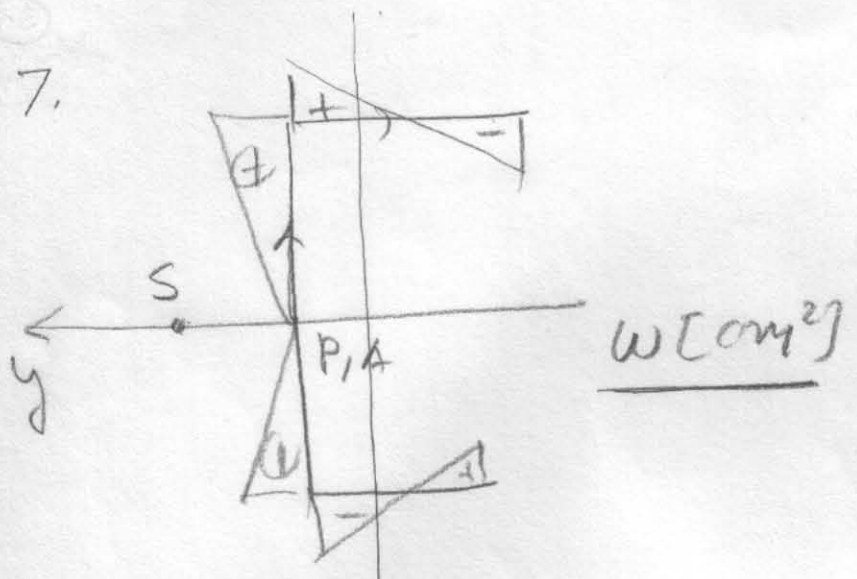
$$I_t = \frac{1}{3} \sum (b_i \cdot t_i^3) = \frac{1}{3} (2 \cdot 20 \cdot 2,5^3 + 2 \cdot 20 \cdot 2^3 + 50 \cdot 2^3) = 448,333 \text{ cm}^4$$

$$Z_x = \frac{M_t}{I_t} \cdot t \quad Z_{x1} = \frac{187,113}{448,333 \text{ cm}^4} \cdot 20 \text{ cm} = 8,35 \text{ MPa}$$

$$Z_x = \frac{M_t}{I_t} \cdot t \quad Z_{x2} = \frac{137,63}{448,333 \text{ cm}^4} \cdot 20 \text{ cm} = 6,14 \text{ MPa}$$

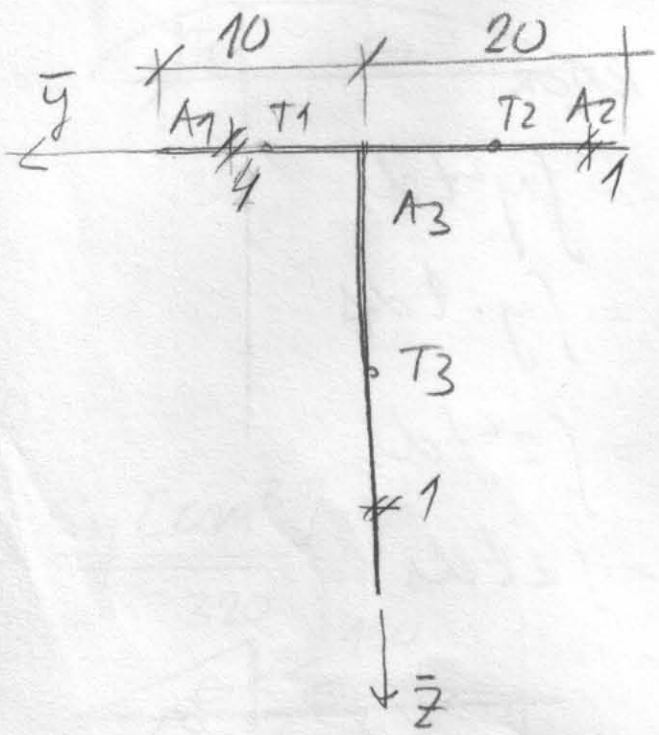
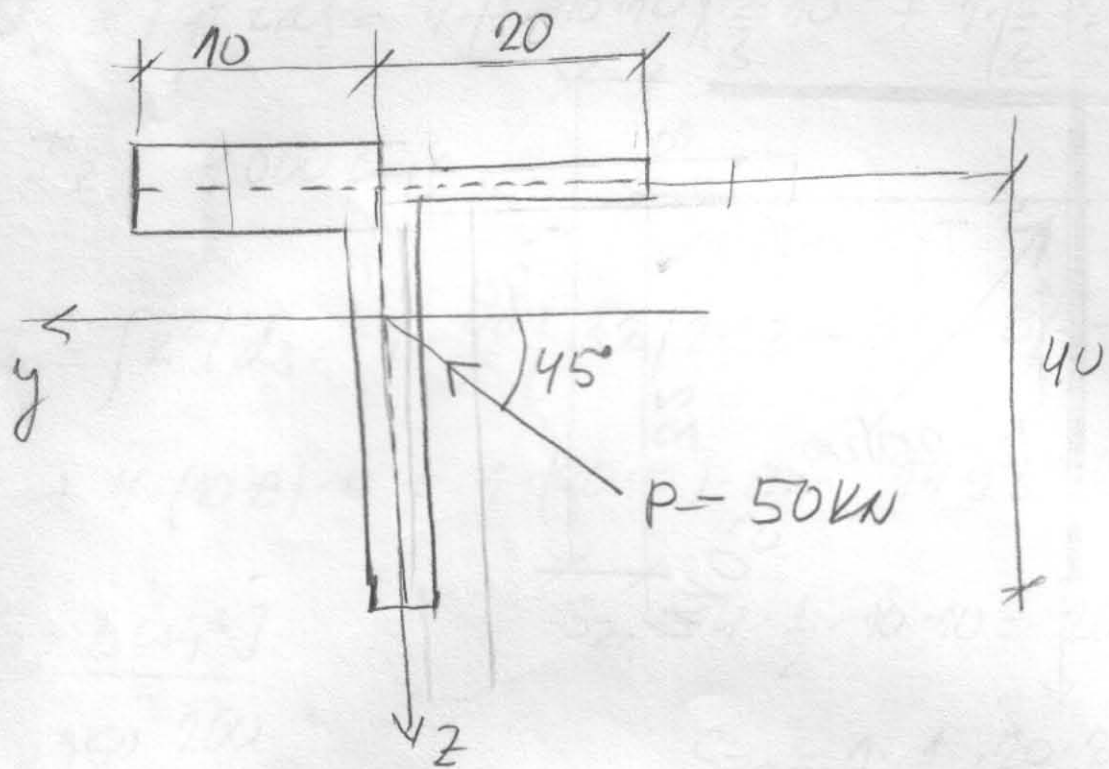
$$Z_{x3} = \frac{10,43}{2,5 \text{ cm}} = 4,17 \text{ MPa}$$

7.



$y \text{ gaj}$

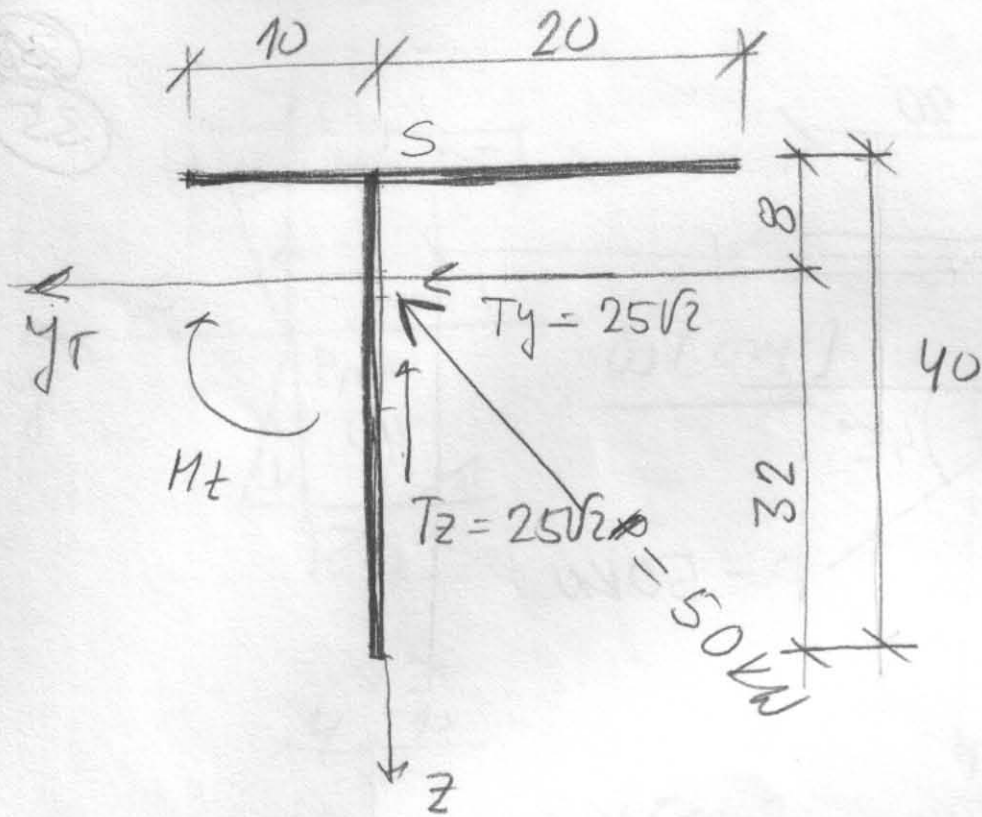
$$I_{y_{wp}} = \int y_{wp}^2 \cdot b \cdot dy = \text{cm}^4$$



$A_1 = 40$	$T_1(5; 0)$
$A_2 = 20$	$T_2(-10; 0)$
$A_3 = 40$	$T_3(0; 20)$
<hr/>	
$A = 100$	

$$\bar{z}_T = \frac{40 \cdot 20}{100} = 80\text{cm}$$

$$\bar{y}_T = \frac{40 \cdot 5 + 20(-10)}{100} = 0$$



$$M_t = 25\sqrt{2} \cdot 8 \text{ kNm} = 200\sqrt{2} \text{ kNm}$$

$$\tau_x^{T_y} = - \frac{T_y \cdot S_z}{I_z \cdot t}$$

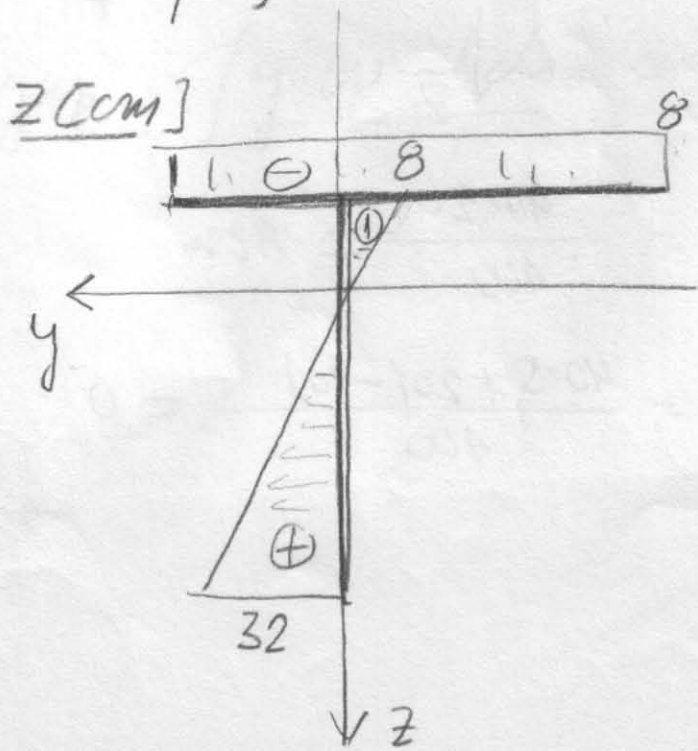
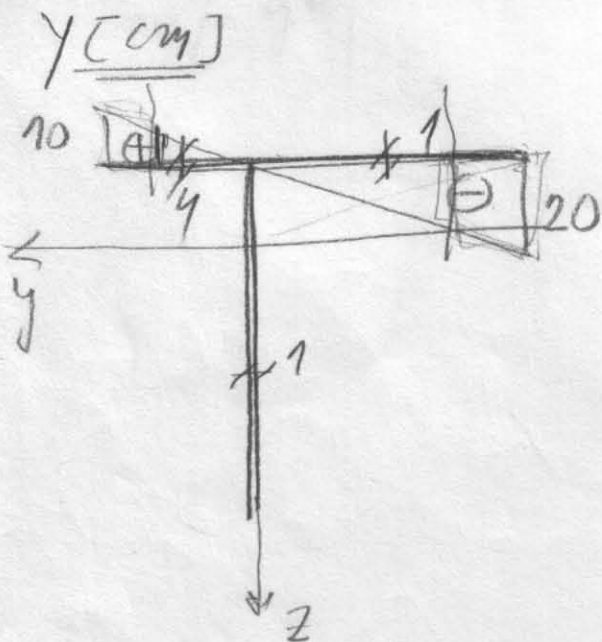
$$I_z = \int y^2 t ds$$

$$S_z = \int y \cdot t ds$$

$$\tau_x^{T_z} = - \frac{T_z \cdot S_y}{I_y \cdot t}$$

$$I_y = \int z^2 t ds$$

$$S_y = \int z t ds$$



$$I_z = \int y^2 t ds = 4 \cdot \left(\frac{1}{2} \cdot 10 \cdot 10 \right) \cdot \frac{2}{3} \cdot 10 + 1 \cdot \left(\frac{1}{2} \cdot 20 \cdot 20 \right) \cdot \frac{2}{3} \cdot 20 \quad (37)$$

$$I_z = 4000 \text{ cm}^4$$

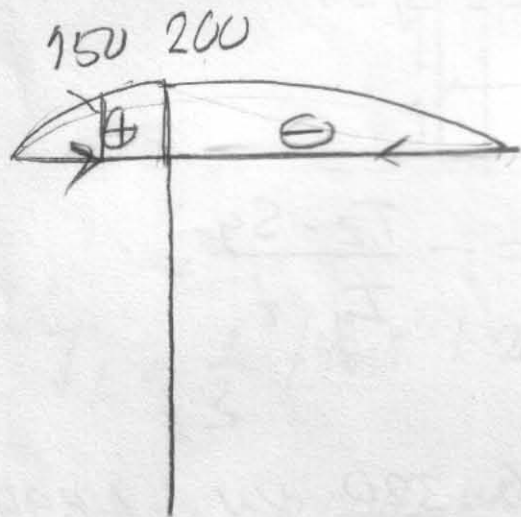
$$I_y = \int z^2 t ds = 4 \cdot \frac{40}{6} \left[32(2 \cdot 32 - 8) - 8(-2 \cdot 8 + 32) \right]$$

$$+ 4 \cdot (10 \cdot 8) \cdot 8 + 1 \cdot (20 \cdot 8) \cdot 8 = 14933,333 \text{ cm}^4$$

$$S_z [\text{cm}^3]$$

$$S_{z1} = 4 \cdot \frac{1}{2} \cdot 10 \cdot 10 = 200$$

$$S_{z2} = 1 \cdot \frac{1}{2} \cdot 20 \cdot 20 = 200$$



$$S_A = 4 \cdot \frac{1}{2} (10 + 5) \cdot 5$$

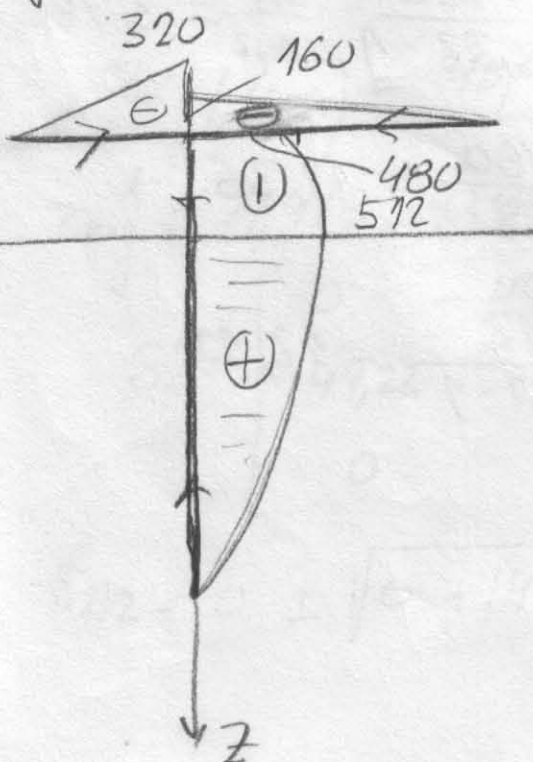
$$S_y [\text{cm}^3]$$

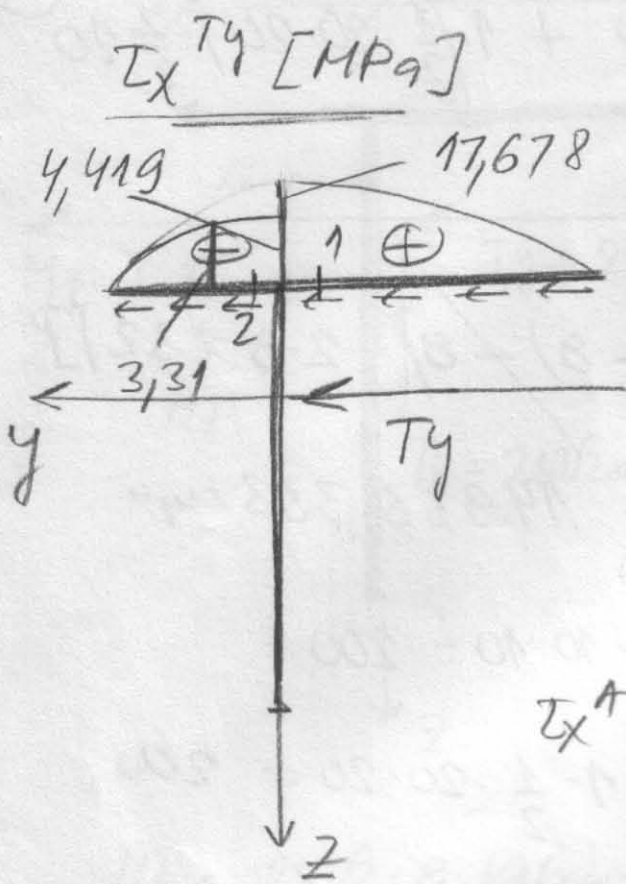
$$S_{y1} = 4 \cdot (8 \cdot 10) = 320$$

$$S_{y2} = 1 \cdot (8 \cdot 20) = 160$$

$$S_{y3} = 480 + 1 \cdot \frac{1}{2} \cdot 8 \cdot 8 = 512$$

$$S_{y4} = 1 \cdot \frac{1}{2} \cdot 32 \cdot 32 = 512$$



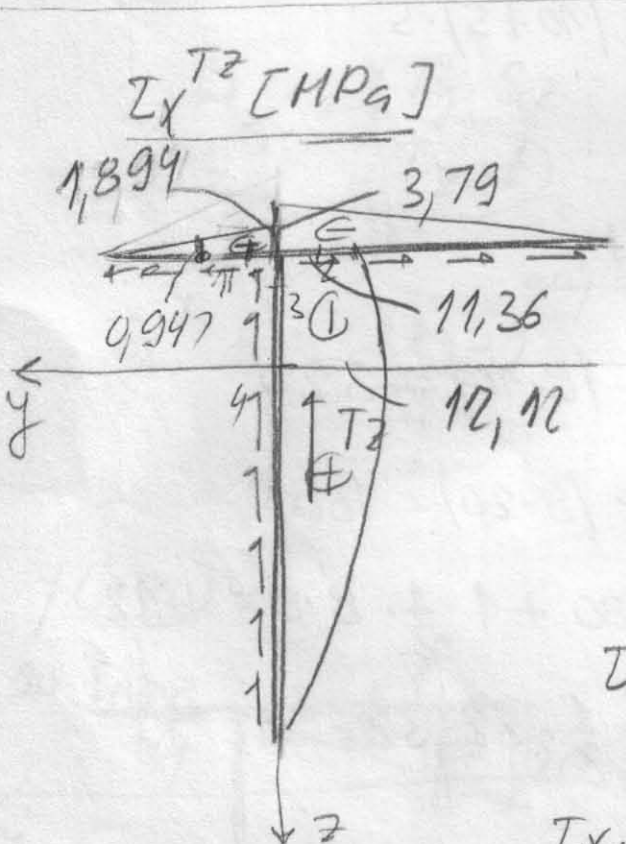


$$\tau_x^{T_y} = - \frac{T_y \cdot S_z}{I_z \cdot t}$$

$$\tau_{x1} = \frac{25\sqrt{2} \text{ kN} \cdot 200 \text{ cm}^3}{4000 \text{ cm}^4 \cdot 1 \text{ cm}} = 17,678 \text{ MPa}$$

$$\tau_{x2} = \frac{25\sqrt{2} \text{ kN} \cdot 200 \text{ cm}^3}{4000 \text{ cm}^4 \cdot 4 \text{ cm}} = 4,419 \text{ MPa}$$

$$\tau_x^A = \frac{25\sqrt{2} \cdot 150}{4000 \cdot 4} = 3,31$$



$$\tau_x^{T_z} = - \frac{T_z \cdot S_y}{I_y \cdot t}$$

$$\tau_{x1} = \frac{25\sqrt{2} \cdot 320 \text{ kN}}{14933,33 \cdot 4 \text{ cm}^2} = 1,899 \text{ MPa}$$

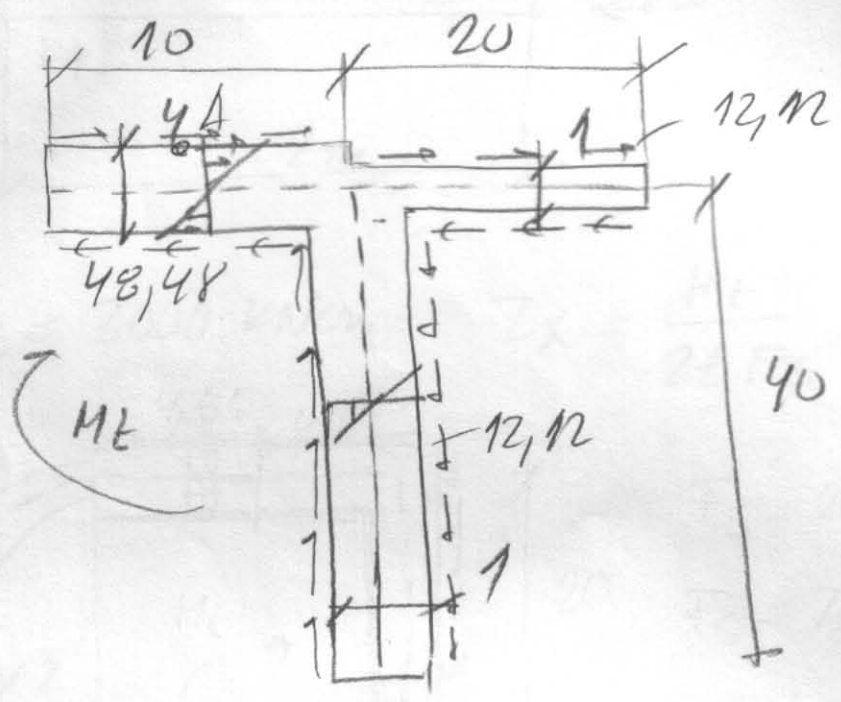
$$\tau_{x2} = \frac{25\sqrt{2} \cdot 160 \text{ kN}}{14933,33 \cdot 1 \text{ cm}^2} = 3,79$$

$$\tau_{x3} = \frac{25\sqrt{2} \cdot 480}{14933,33 \cdot 1} = 11,36$$

$$\tau_{x4} = \frac{25\sqrt{2} \cdot 512}{14933,33 \cdot 1} = 12,11$$

σ_x [MPa]

H ∇ Jobanobuta
204/08



$$I_t = \frac{1}{3} (40 \cdot 1^3 + 20 \cdot 1^3 + 10 \cdot 4^3) = 233,33 \text{ cm}^4$$

$$\sigma_{x1} = \frac{2000 \sqrt{2} \text{ kNcm}, 1 \text{ cm}}{233,33 \text{ cm}^4} = 12,12 \text{ MPa}$$

$$\sigma_{x2} (4 \text{ cm}) = 48,48 \text{ MPa}$$

$$\sigma_{xy}^A = 4,419 + 9,947 - 48,48 = -44,22$$

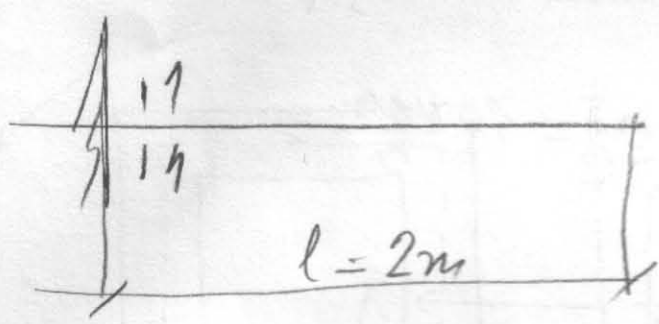
$$S^A = \begin{bmatrix} 0 & -44,22 & 0 \\ -44,22 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \text{ MPa}$$

$$\sigma_{1,2} = 0 \pm \sqrt{0 + (44,22)^2} =$$

$$\sigma_1 = 44,22 \text{ MPa}$$

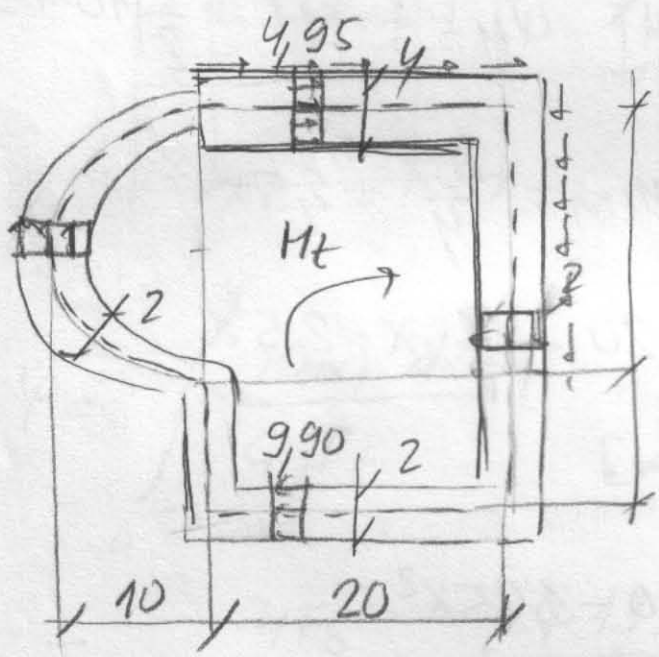
$$\sigma_2 = -44,22$$

$G = 80 \text{ GPa} = 80\,000 \text{ MPa} = 8000 \text{ kN/cm}^2$



$M_t = 30 \text{ kNm}$

$M_t = 3000 \text{ kNcm}$ $I_x = \frac{M_t}{2t F_s}$



$F_s = 20 \cdot 30 + \frac{1}{2} 10^2 \pi$

$F_s = 757,08 \text{ cm}^2$

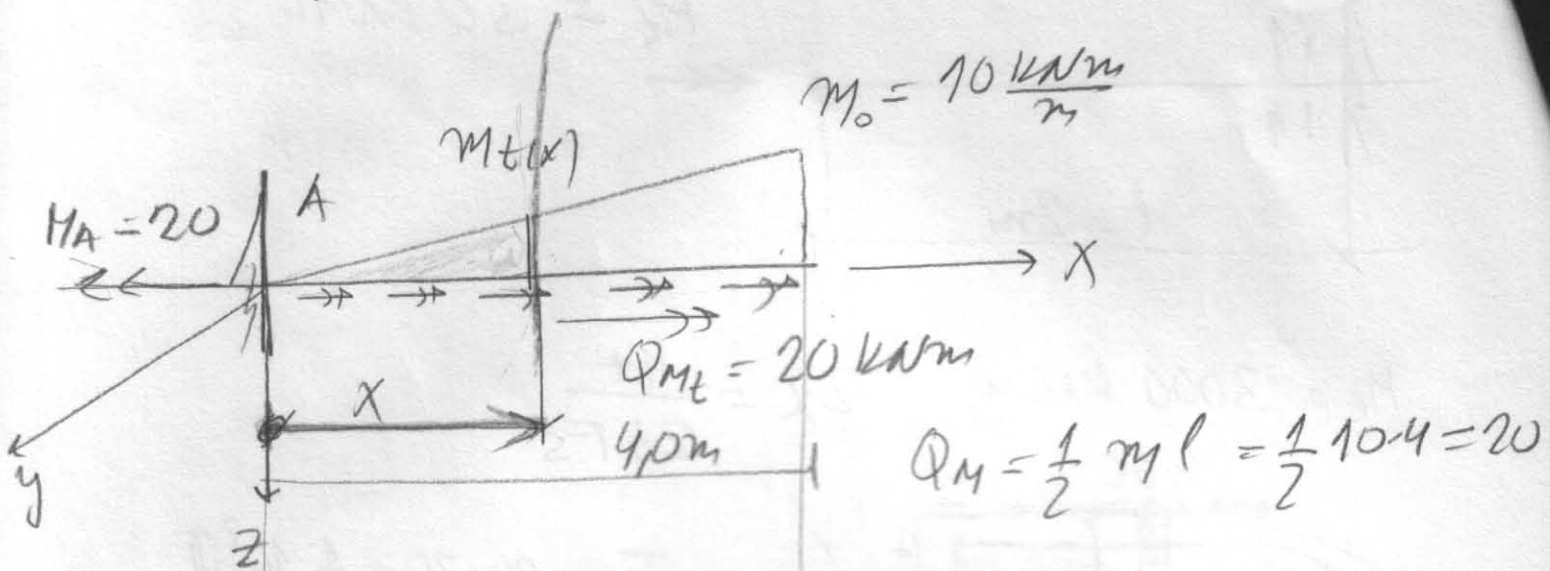
$I_{x1} = \frac{3000}{2 \cdot 2 \cdot 757,08} = 9,90 \text{ MPa}$

$I_{x2} = \frac{3000}{2 \cdot 4 \cdot 757,08} = 4,95 \text{ MPa}$

$I_t = \frac{4 F_s^2}{\sum \frac{G_i}{t_i}} = \frac{4 \cdot 757,08^2}{\left(\frac{20}{2} + \frac{30}{2} + \frac{20}{4} + \frac{10}{2} + \frac{10\pi}{2} \right)} = 45\,213,42 \text{ cm}^4$

$\varphi_{max} = \frac{M_t l}{G I_t} = \frac{3000 \text{ kNcm} \cdot 200 \text{ cm}}{8000 \frac{\text{kN}}{\text{cm}^2} \cdot 45\,213,42 \text{ cm}^4} = 1,65 \cdot 10^{-3} \text{ rad}$

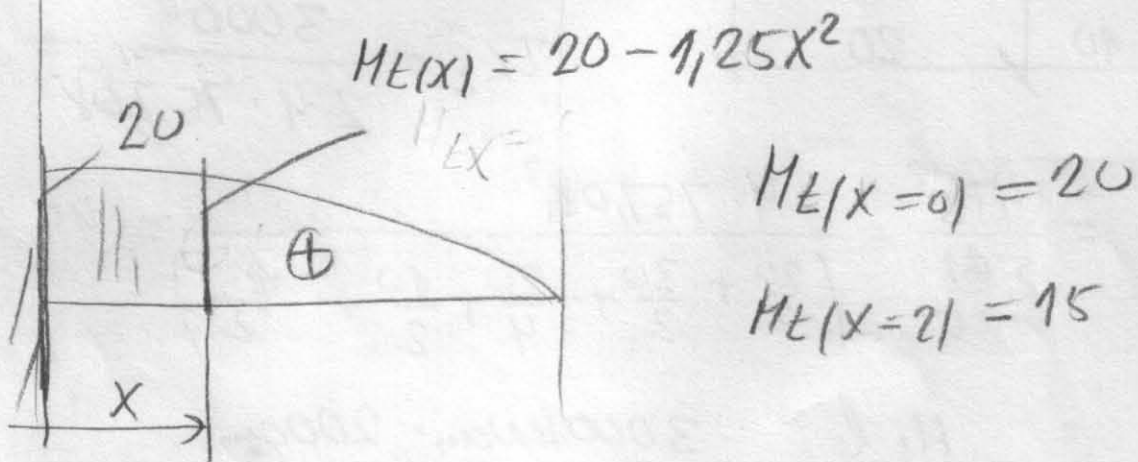
a) Напряжения в сечении Мт



$$m_{L(x)} = x = 10 \cdot 4 \quad m_{L(x)} = \frac{10x}{4} = 2,5x$$

$$M_L(x) = 20 - \frac{1}{2} \cdot x \cdot m_{L(x)} = 20 - \frac{1}{2} \cdot x \cdot 2,5x$$

$$\underline{M_L(x) = 20 - 1,25x^2 \text{ [kNm]}}$$

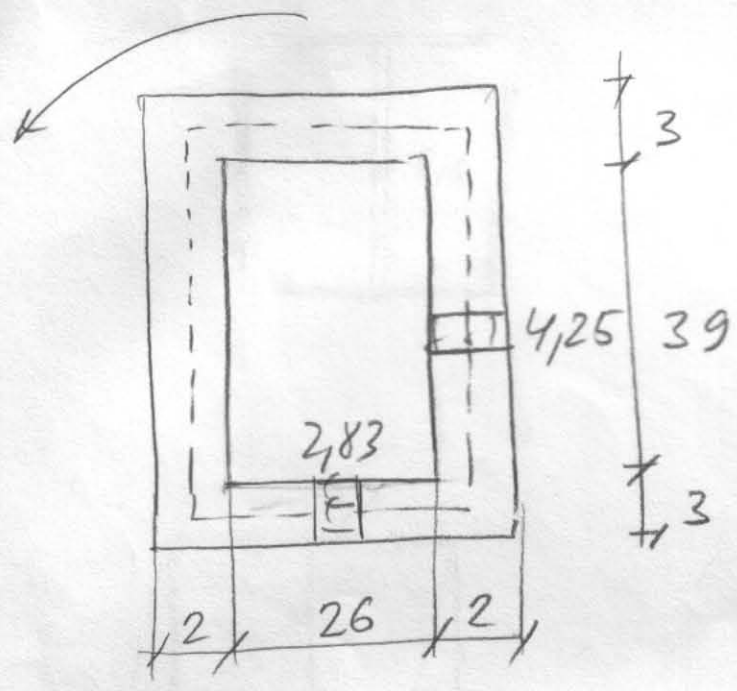


$$E = 20 \text{ GPa} = 20 \cdot 10^6 \text{ kPa} \left[\frac{\text{kN}}{\text{m}^2} \right] \quad \nu = 0,15$$

$$G = \frac{E}{2(1+\nu)} = \frac{20 \cdot 10^6}{2(1+0,15)} = 8,69 \cdot 10^6 \frac{\text{kN}}{\text{m}^2}$$

2-2

Me



$$F_s = 28 \cdot 42 = 1176 \text{ cm}^2$$

$$I_{x1} = \frac{2000 \text{ kNcm}}{2 \cdot 2 \text{ cm} \cdot 1176}$$

$$I_{x2} = \frac{2000 \text{ kNcm}}{2 \cdot 3 \cdot 1176}$$

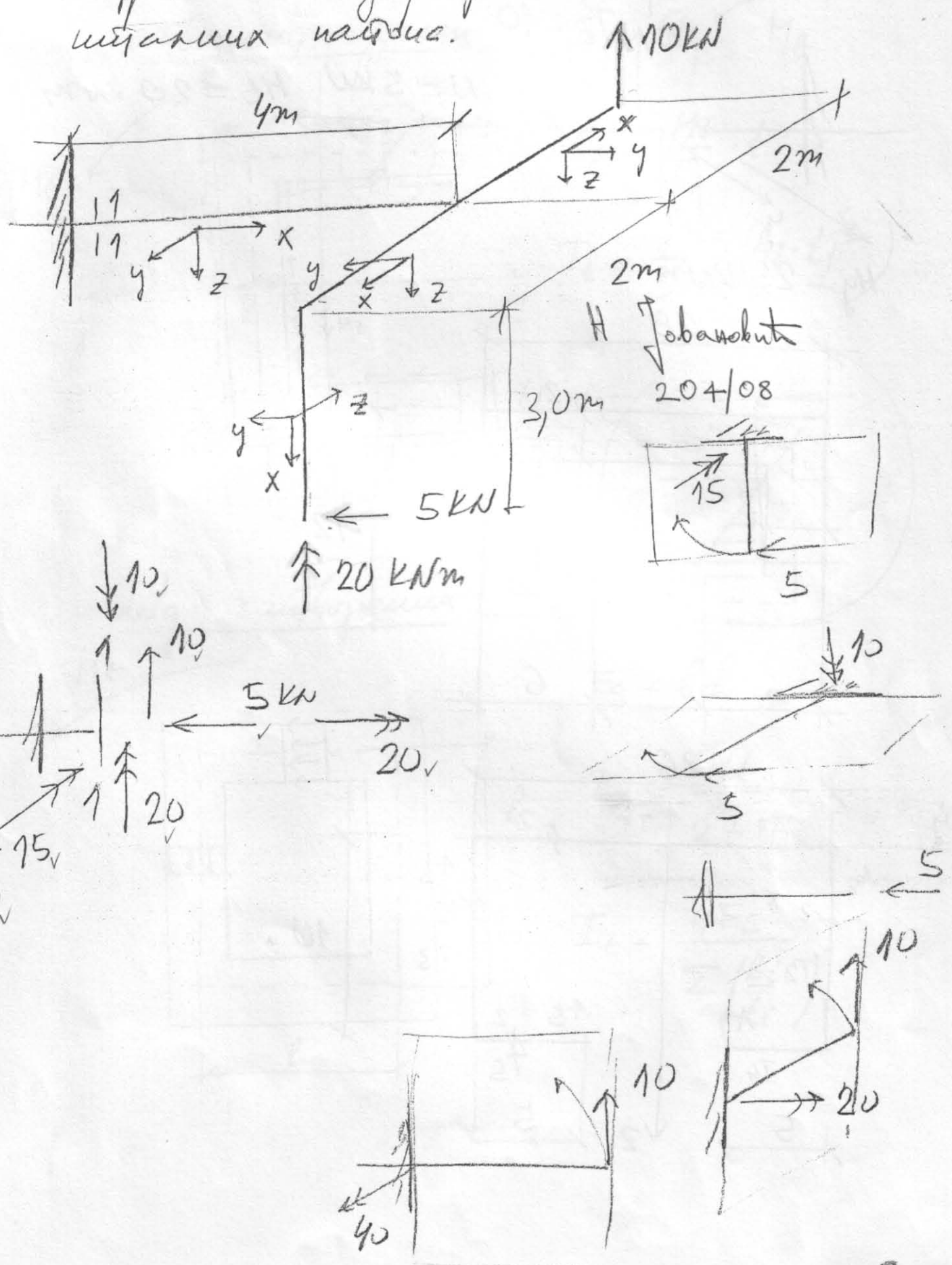
$$\varphi = \int_0^4 \frac{M(x) dx}{G I_t}$$

$$I_t = \frac{4 F_s^2}{\sum \frac{b^3}{6}} = \frac{4 \cdot 1176^2}{\left(\frac{42 \cdot 2}{2} + \frac{28 \cdot 2}{3} \right)} = 91\,185,23 \text{ cm}^4$$

$$\varphi = \int_0^4 \frac{(20 - 1,25 x^2) dx}{8,69 \cdot 10^6 \frac{\text{kN}}{\text{m}^2} \cdot 91\,185,23 \cdot 10^{-8}}$$

$$\varphi = \frac{1}{7929,15} \cdot \left[20x - 1,25 \frac{x^3}{3} \right]_0^4 = 6,73 \cdot 10^{-3} \text{ rad}$$

За пресеци 1-1 и 2-2 у зидовима
 нацртајте дијаграме колико-
 штакних напон.

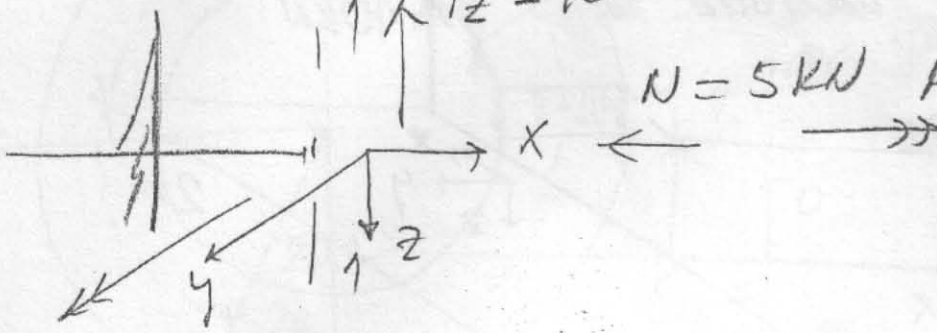


Процес 1-1

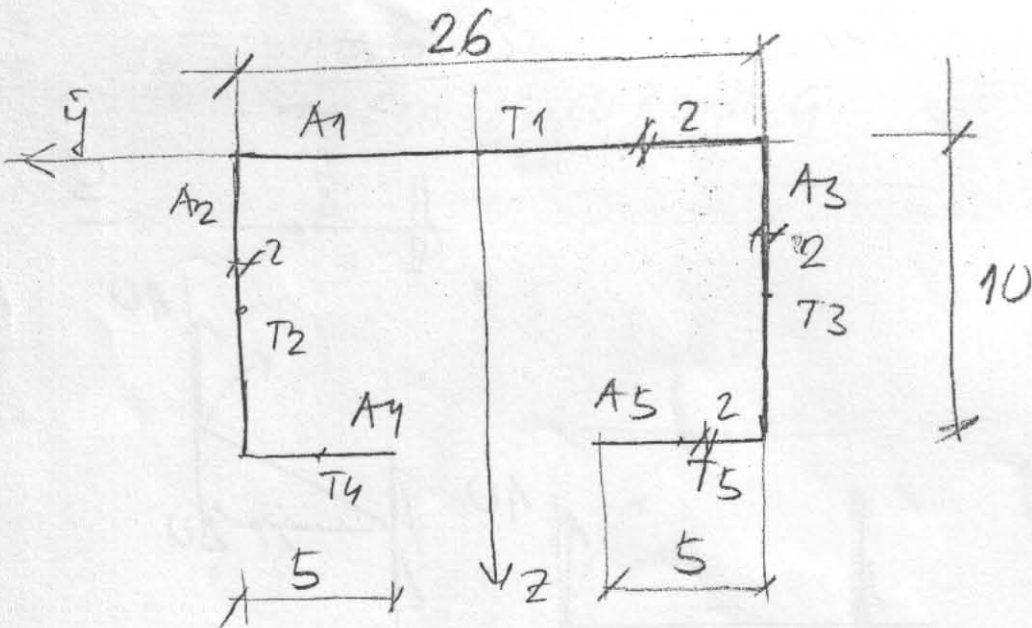
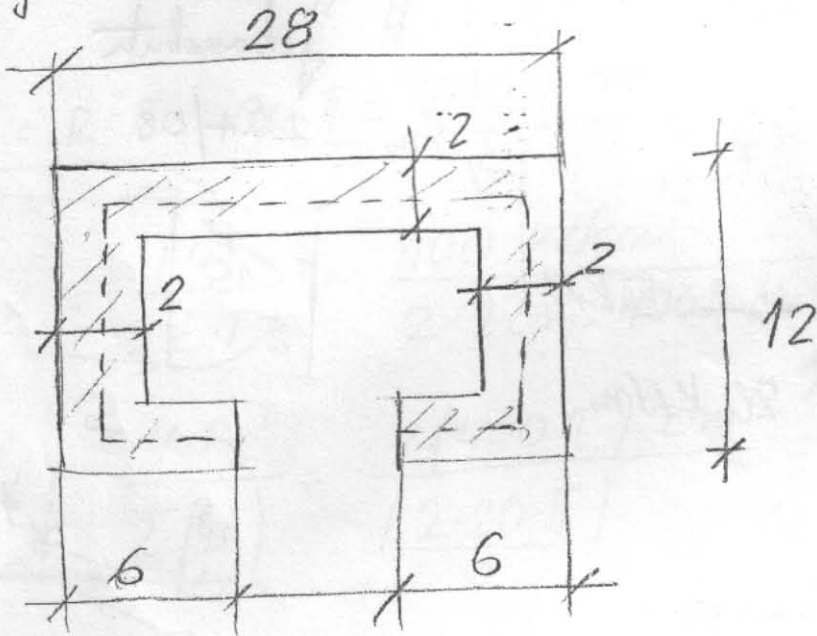
$M_2 = 10 \text{ kNm}$

$T_2 = 10$

$N = 5 \text{ kN} \quad M_E = 20 \text{ kNm}$



$M_y = 25 \text{ kNm}$

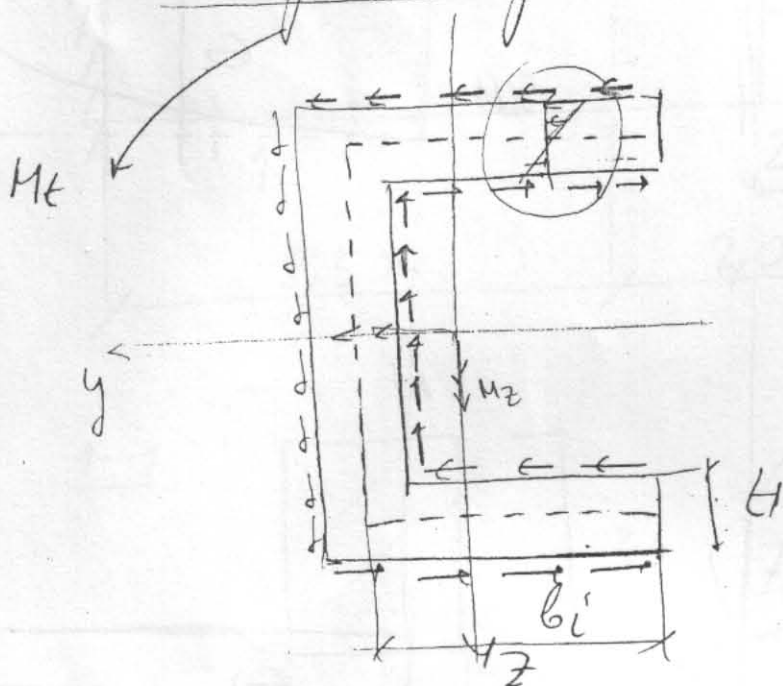


Z_x и M_t

* $\overrightarrow{M_t} \leftarrow \epsilon$

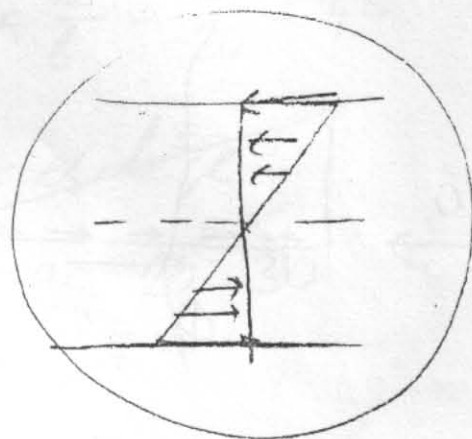
отборщина фрезен

$\oplus \overleftarrow{M_t}$

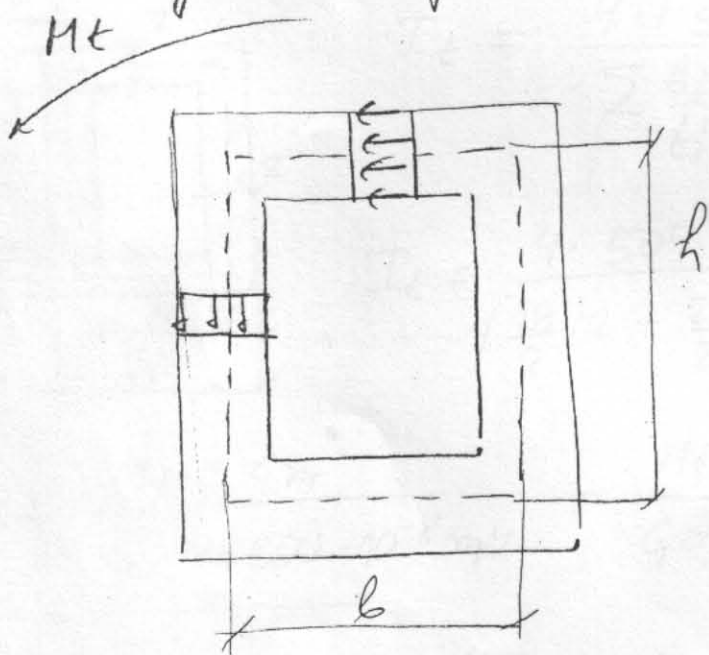


$$Z_x = \frac{M_t \cdot t}{I_t}$$

$$I_t = \frac{1}{3} \sum (b_i \cdot t_i^3)$$



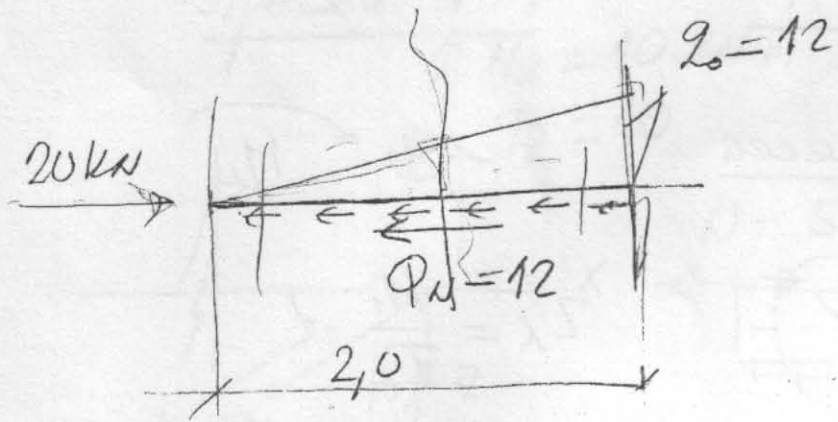
пог заборщина



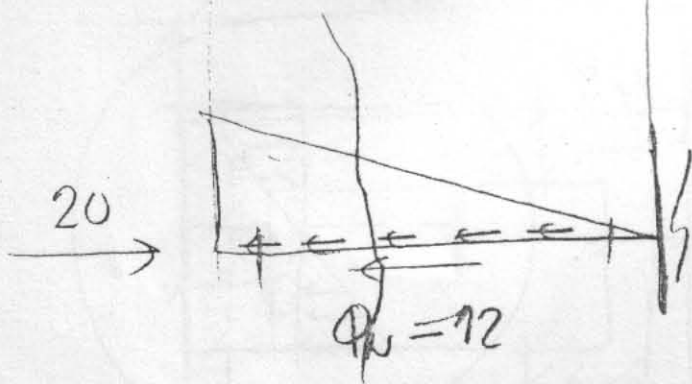
$$F_s = b \cdot h$$

$$Z_x = \frac{M_t}{2t \cdot F_s}$$

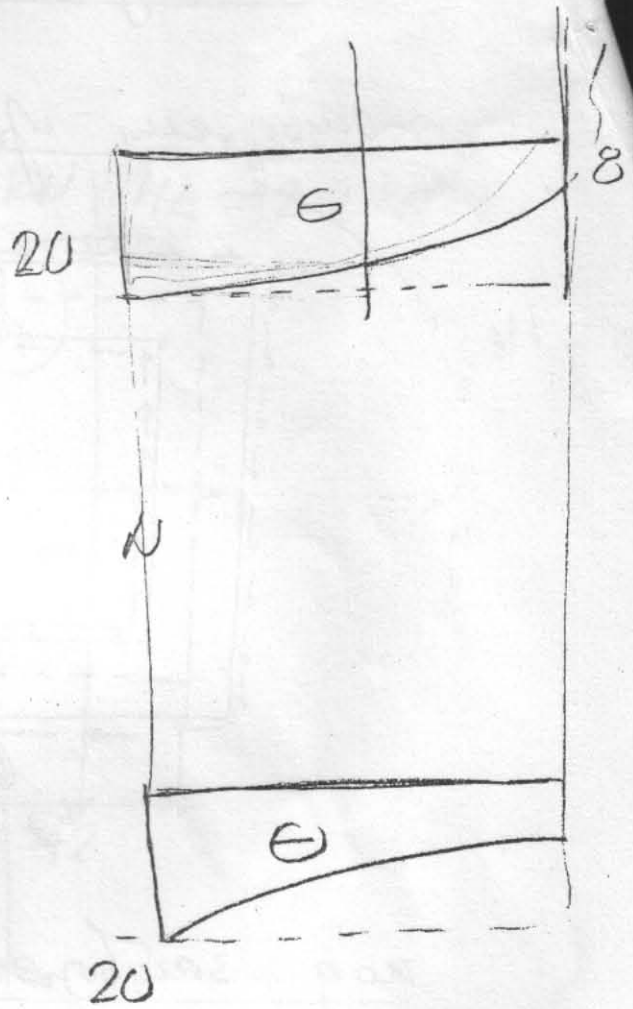
$$I_t = \frac{4F_s^2}{\sum \left(\frac{b_i}{t_i} \right)}$$



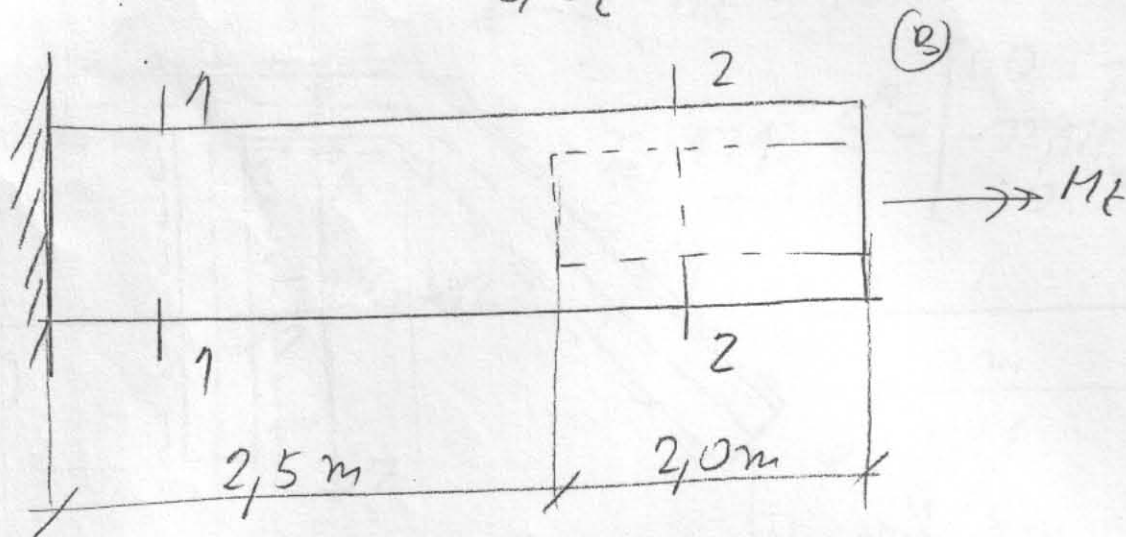
$$Q_N = \frac{1}{2} \cdot 12 \cdot 2 = 12$$



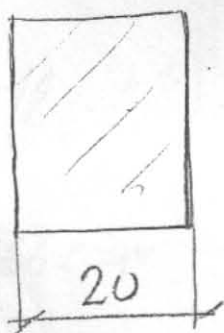
M



$$\varphi = \frac{M_L l}{G I_t}$$



1-1

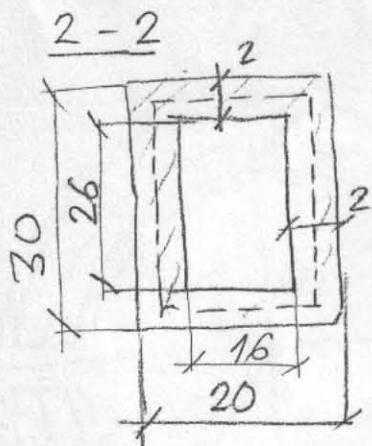


$$\mu = \frac{h}{b} = \frac{30}{20} = 1,5$$

$$I_t = \alpha \cdot b^3 \cdot h$$

$$I_t = 0,195 \cdot 20^3 \cdot 30$$

$$I_t = 46800 \text{ cm}^4$$



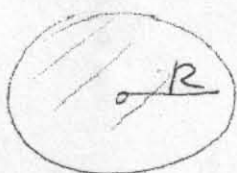
$$I_t = \frac{4 \cdot F_S^2}{\sum \frac{b_i}{t_i}}$$

$$F_S = 18 \cdot 28$$

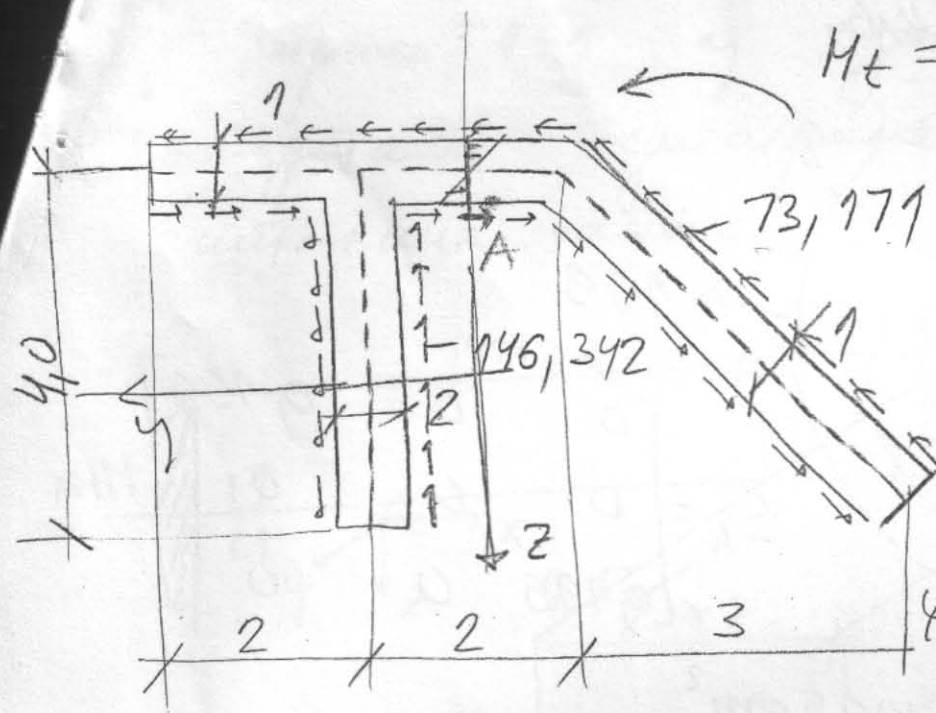
$$F_S = 504 \text{ cm}^2$$

$$I_t = \frac{4 \cdot 504^2}{\left(\frac{18 \cdot 2}{2} + \frac{28 \cdot 2}{2}\right)} = 22088,35 \text{ cm}^4$$

$$\varphi_B = \frac{M_L \cdot 2,5 \text{ m}}{G \cdot 46800 \cdot 10^{-8} \text{ m}^4} + \frac{M_L \cdot 2,0 \text{ m}}{G \cdot 22088,35 \cdot 10^{-8} \text{ m}^4}$$

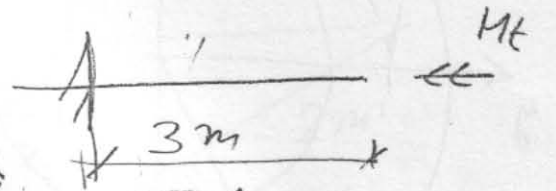


$$I_t = \frac{R^4 \pi}{2}$$



$$M_t = 1 \text{ kNm}$$

$$S^A = \begin{bmatrix} 0 & 0 & -73,171 & 0 \\ -73,171 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \text{ MPa}$$



$$\varphi = \frac{M_t \cdot l}{G I_t}$$

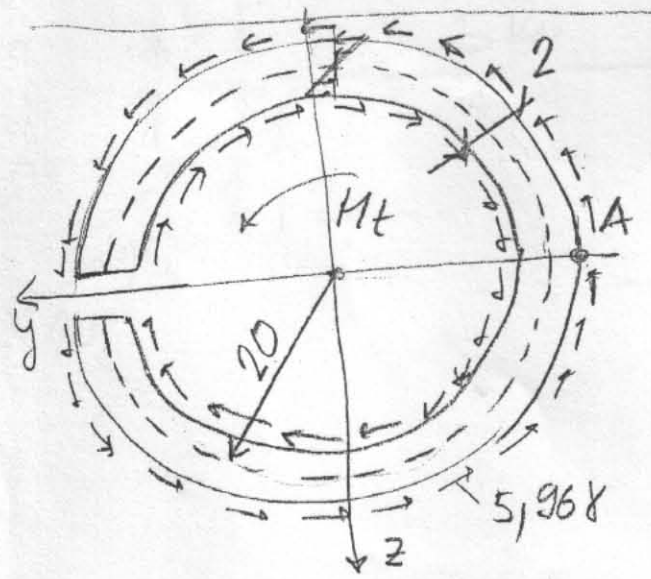
$$\varphi = \frac{1 \text{ kNm} \cdot 3 \text{ m}}{G \cdot 13,666 \cdot 10^{-8} \text{ m}^4}$$

$$I_t = \frac{1}{3} \sum (b_i \cdot t_i^3) = \frac{1}{3} \cdot (4 \cdot 2^3 + 4 \cdot 1^3 + 5 \cdot 1^3)$$

$$I_t = 13,666 \text{ cm}^4$$

$$\tau_x = \frac{M_t}{I_t} \cdot t = \frac{100 \text{ kNm}}{13,666 \text{ cm}^4} \cdot (1 \text{ cm}) = 73,171 \text{ MPa}$$

$$(12 \text{ cm}) = 146,342 \text{ MPa}$$



$$I_t = \frac{1}{3} \sum (b_i \cdot t_i^3) \quad M_t = 1 \text{ kNm}$$

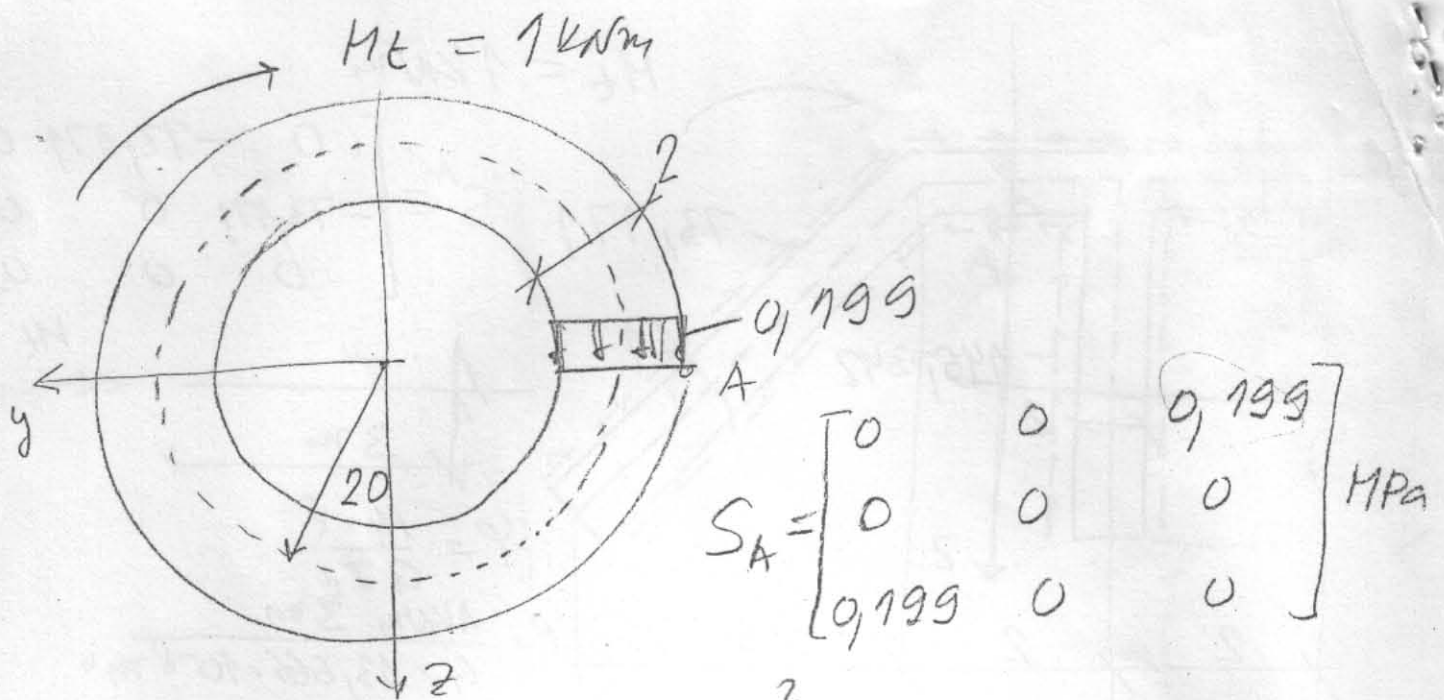
$$I_t = \frac{1}{3} \cdot (2 \cdot 20\pi \cdot 2^3)$$

$$I_t = 335,103 \text{ cm}^4$$

$$S^A = \begin{bmatrix} 0 & 0 & -5,968 \\ 0 & 0 & 0 \\ -5,968 & 0 & 0 \end{bmatrix} \text{ MPa}$$

$$\tau_x = \frac{M_t}{I_t} \cdot t = \frac{100 \text{ kNm}}{335,103 \text{ cm}^4} \cdot 2 \text{ cm} = 5,968 \text{ MPa}$$

$$\varphi = \frac{1 \text{ kNm} \cdot 3 \text{ m}}{G \cdot 335,103 \cdot 10^{-8} \text{ m}^4}$$



$$F_s = R^2 \pi = 20^2 \pi = 400 \pi \text{ cm}^2$$

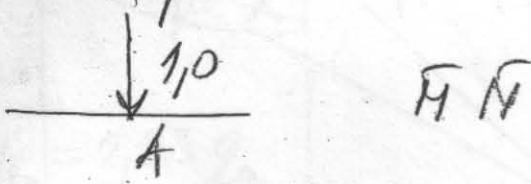
$$\tau_x = \frac{M_t}{2t \cdot F_s} = \frac{100 \text{ kNm}}{2 \cdot 2 \text{ cm} \cdot 400 \pi \text{ cm}^2} = 0,199 \text{ MPa}$$

$$I_t = \frac{4 \cdot F_s^2}{\sum \left(\frac{b_i}{t_i} \right)} = \frac{4 (400 \pi)^2 \text{ cm}^4}{\left(\frac{2 \cdot 20 \cdot \pi}{2} \right)} = 100530,965 \text{ cm}^4$$

$$\varphi_B = \frac{1 \text{ kNm} \cdot 3 \text{ m}}{100530,965 \cdot 10^{-8} \text{ m}^4 \cdot G}$$

Томография

1. Векторная томография - узор

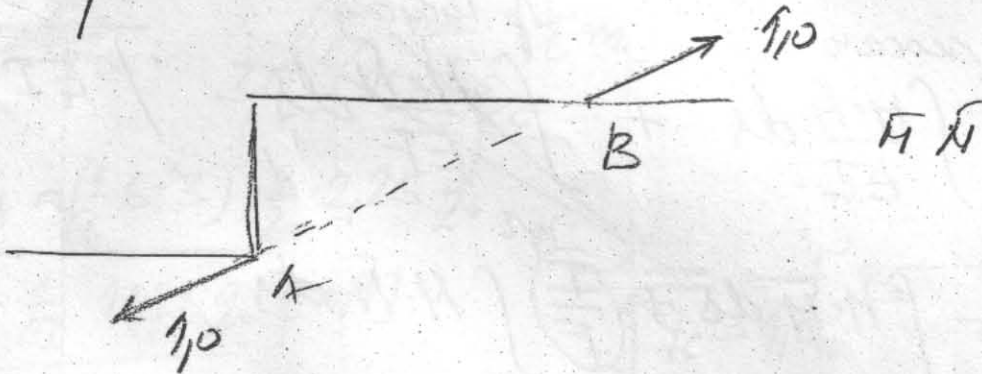


H. Jobanovits
204/08

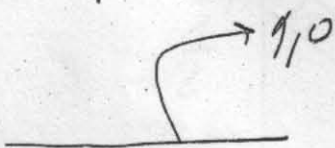
2. хор томография



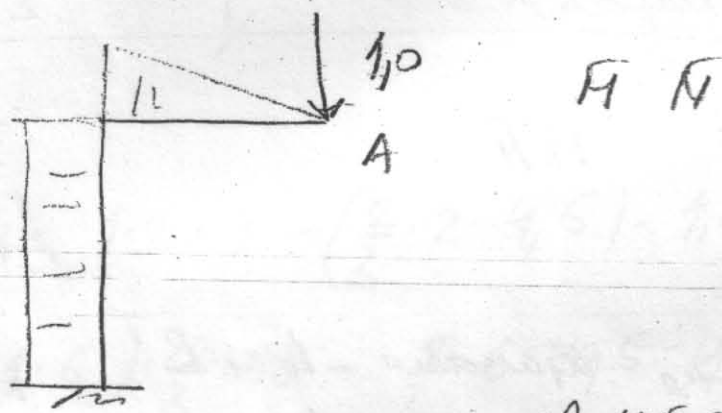
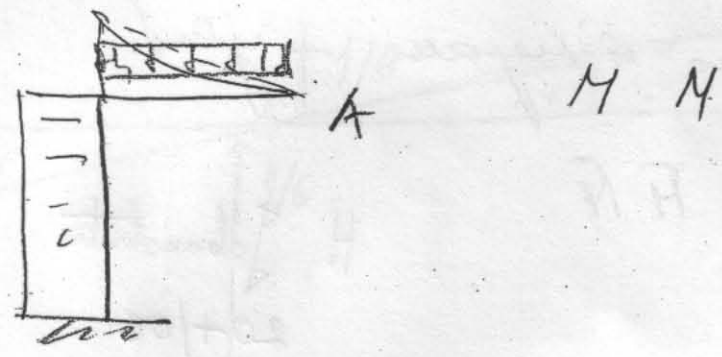
3. разделение стачане А и В



4. обрешетка-рейтингов - нарис



your answer A



$$U_A = \int \frac{M \cdot \bar{M}}{EI} ds + \int \frac{N \cdot \bar{N}}{EF} ds \cdot / EI$$

nocar
up uoyas

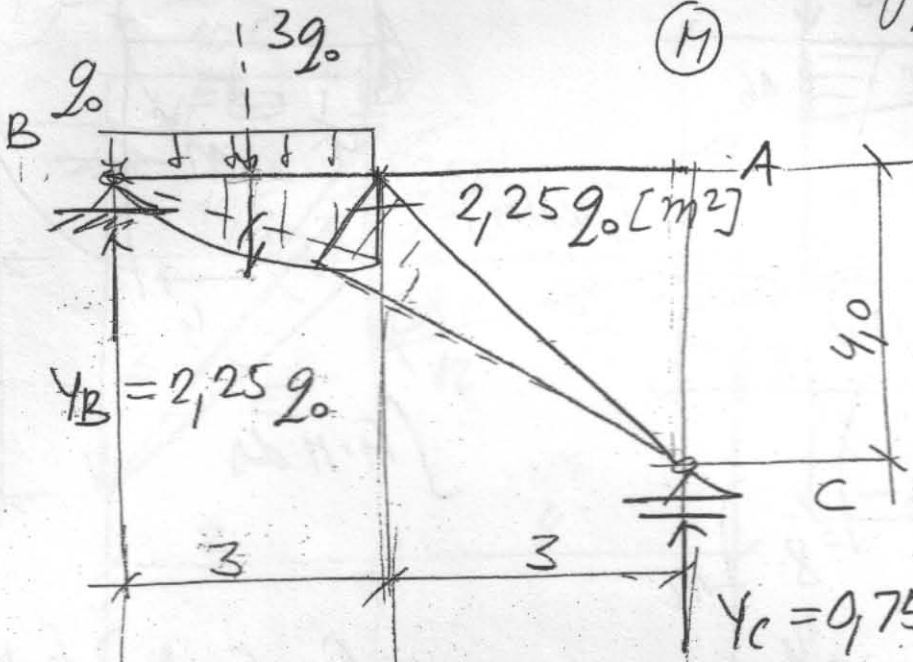
$$EI U_A = \int M \cdot \bar{M} ds + \left(\frac{I}{F} \right) \int N \cdot \bar{N} ds$$

$$[m] U_A = \frac{1}{EI} \cdot \left\{ \right.$$

$$U_A = \int M \cdot \delta ds \quad 3$$

(M)

ET = const

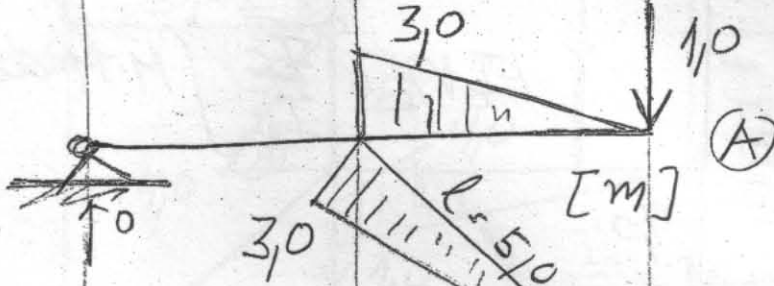


$$f = \frac{1}{8} q l^2$$

$$f = \frac{1}{8} \cdot 39 \cdot 3^2 = \frac{9}{8} \cdot 39$$

$$\sum M_B = 0$$

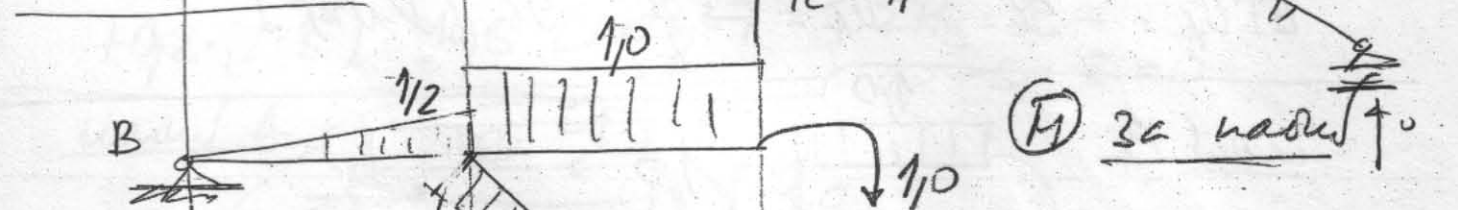
$$39 \cdot 1,5 - Y_c \cdot 6 = 0$$



(M) 3a yasad

$$EI U_A = \frac{(1,5 \cdot 3)}{2} \cdot \frac{2}{3} \cdot 2,25 g$$

$$U_A = \frac{1}{EI} 11,25 g \quad [m^4]$$



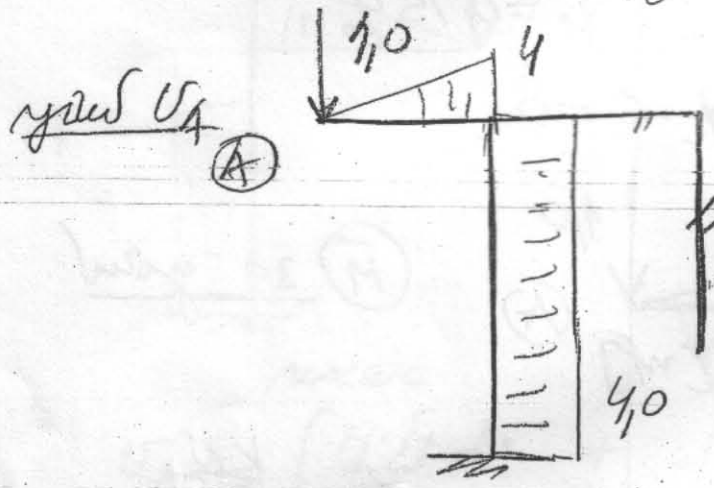
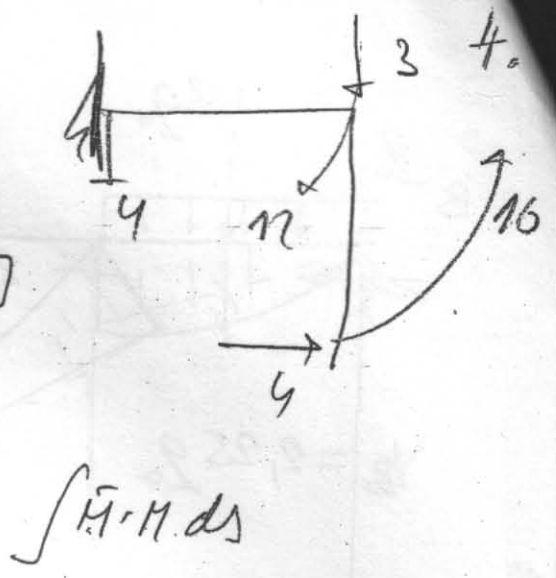
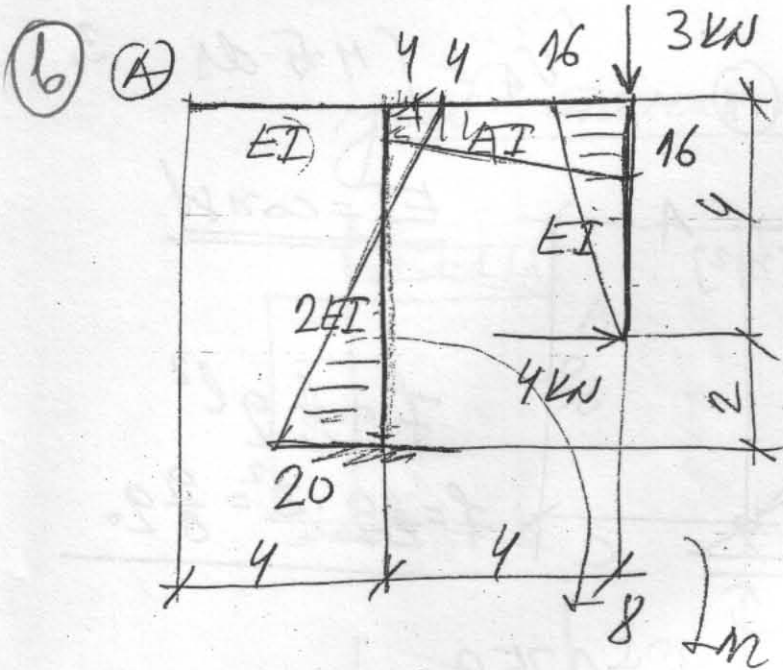
(M) 3a nasud

$$\frac{1}{6} = Y_B$$

$$\sum M_C = 0$$

$$-Y_B \cdot 6 + 1,0 = 0$$

$$EI U_A = \left(\frac{1}{2} \cdot 5 - \frac{1}{2} \right) \cdot \frac{2}{3} \cdot 2,25 g - \left(\frac{1}{2} \cdot 3 \cdot \frac{1}{2} \right) \cdot \frac{2}{3} \cdot 2,25 g - \frac{2}{3} \cdot 3 \cdot \left(\frac{9}{8} g \right) \cdot \frac{1}{4} \quad [m^4]$$

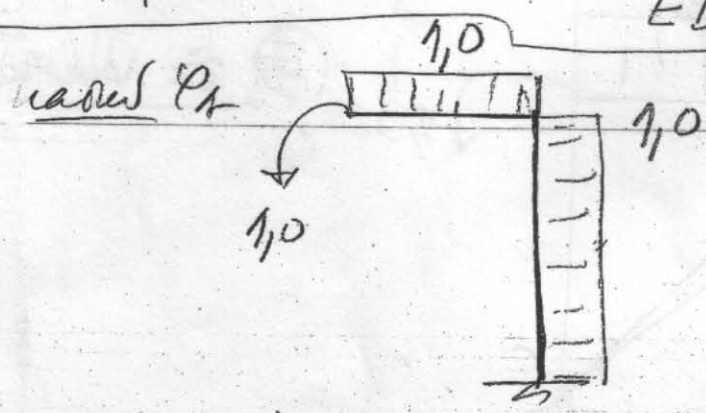


$$U_A = \int \frac{M \cdot \bar{M}}{EI} ds \quad / \cdot EI_c$$

$$EI_c U_A = \frac{I_c}{I_i} \int M \cdot \bar{M} ds$$

$$EI U_A = \frac{1}{2} \cdot \frac{6}{8} [4(2 \cdot 4 + 4) - 20(2 \cdot 4 + 4)]$$

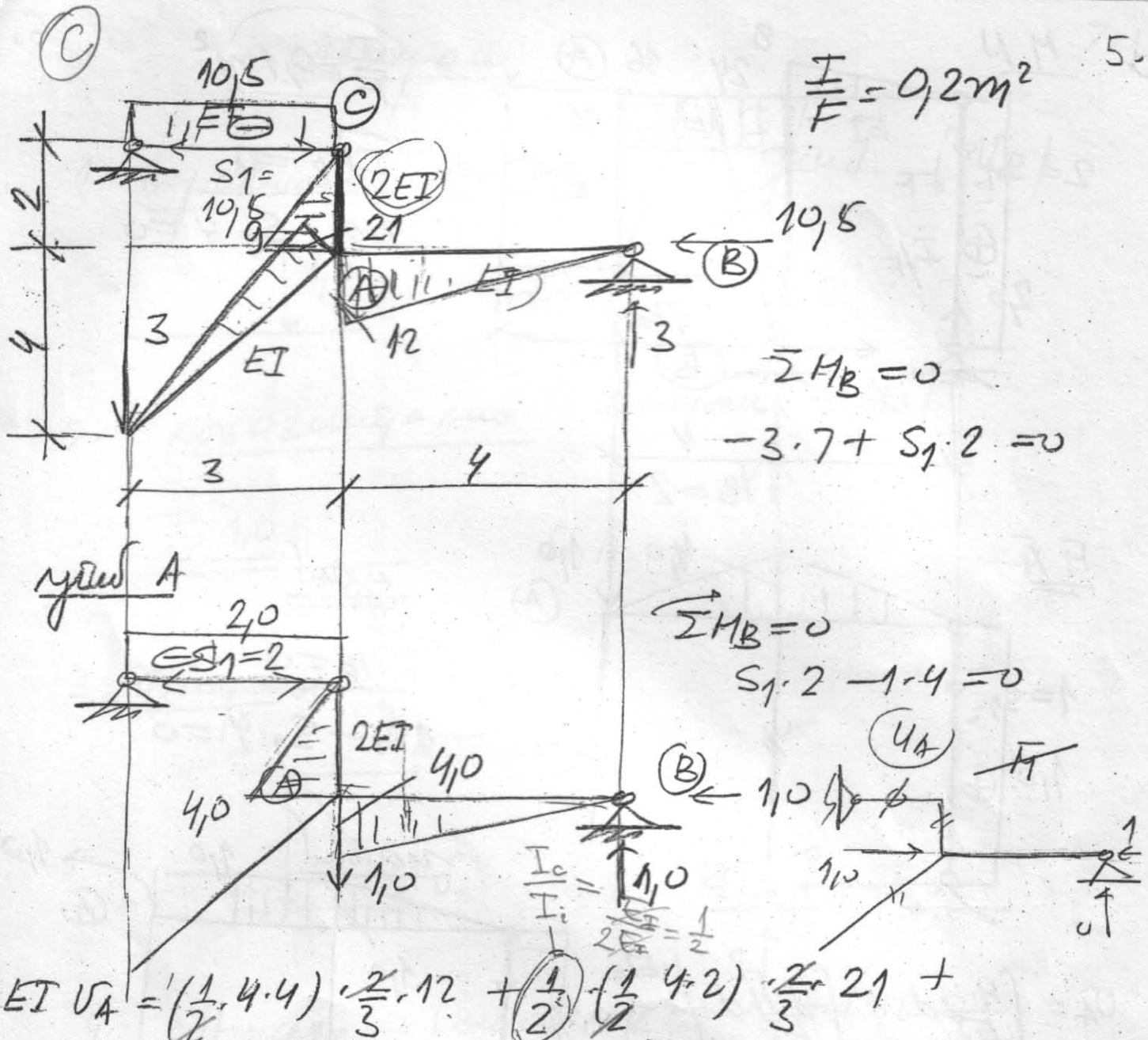
$$EI U_A = -96 \quad U_A = -\frac{1}{EI} \cdot 96 \text{ [kNm}^2\text{]}$$



$$E \cdot \varphi_A = \frac{1}{2} \cdot \frac{6}{8} [4 \cdot (2 \cdot 1 + 1) - 20 \cdot (2 \cdot 1 + 1)] \text{ [kNm}^2\text{]}$$

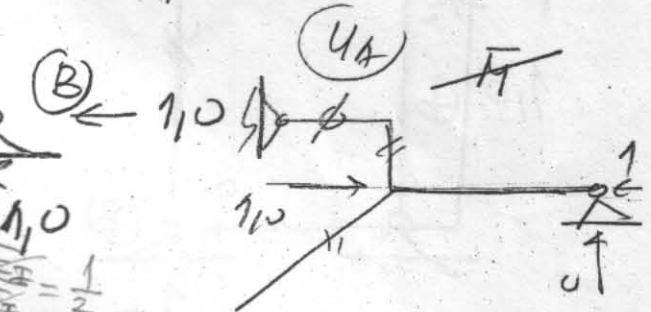
$$\varphi_A = \frac{1}{EI} [-24 \text{ kNm}^2]$$

$\frac{I}{F} = 0,2 \text{ m}^2$



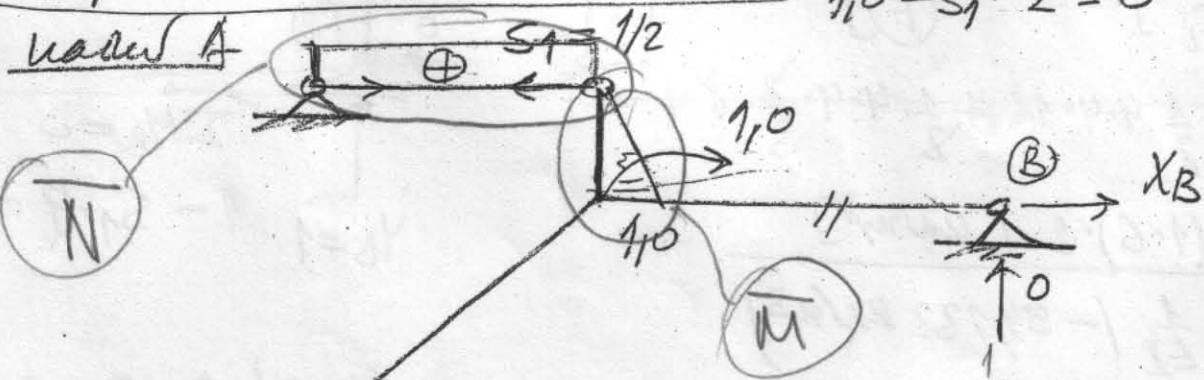
$\Sigma M_B = 0$
 $-3 \cdot 7 + S_1 \cdot 2 = 0$

$\Sigma M_B = 0$
 $S_1 \cdot 2 - 1 \cdot 4 = 0$



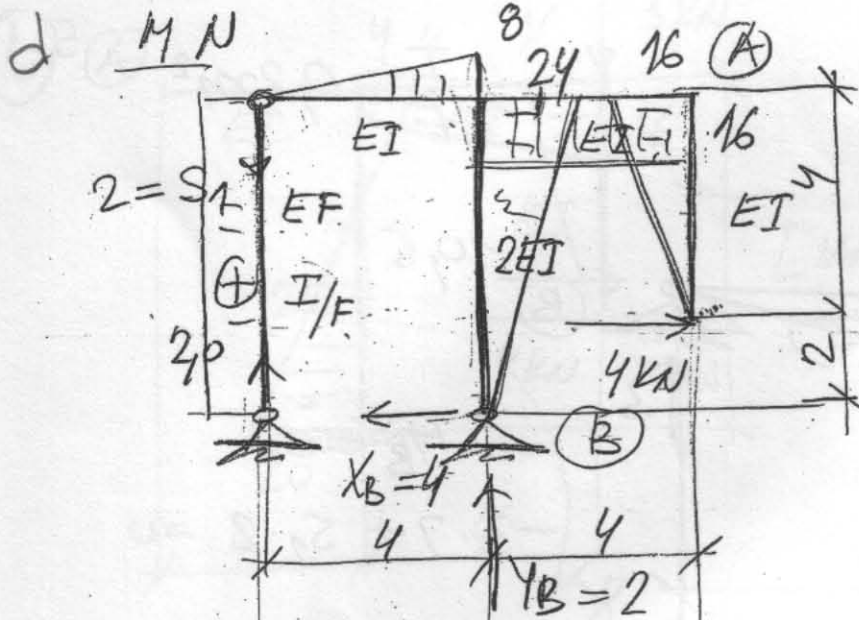
$EI v_A = \left(\frac{1}{2} \cdot 4 \cdot 4\right) \cdot \frac{2}{3} \cdot 12 + \left(\frac{1}{2}\right) \cdot \left(\frac{1}{2} \cdot 4 \cdot 2\right) \cdot \frac{2}{3} \cdot 21 +$
 $+ 0,2 \cdot (2 \cdot 3) \cdot 10,5 \text{ [kNm}^3]$

$\Sigma M_B = 0$
 $11,0 - S_1 \cdot 2 = 0$



$EI v_A = -\frac{1}{2} \cdot \left(\frac{1}{2} \cdot 2 \cdot 1\right) \cdot \frac{2}{3} \cdot 21 - 0,2 \cdot (3 \cdot 1) \cdot 10,5 \text{ [kNm}^3]$

$\frac{I}{F}$

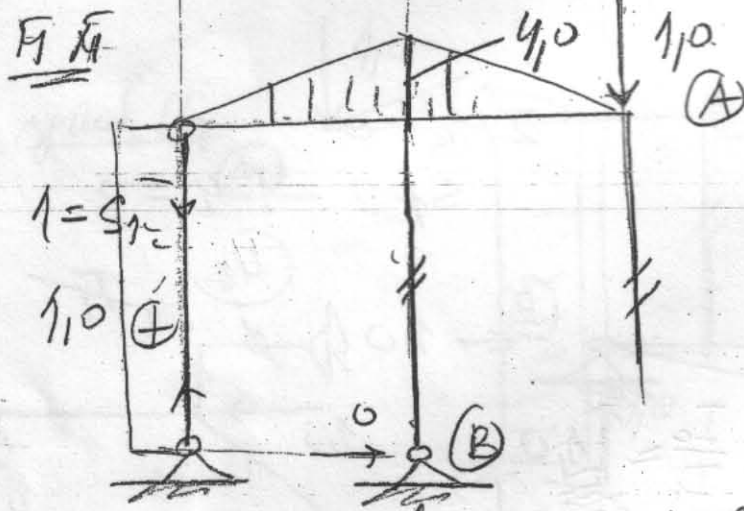


6.

$$\frac{I}{F} = 0,1 \text{ m}^2$$

$$\sum M_B = 0$$

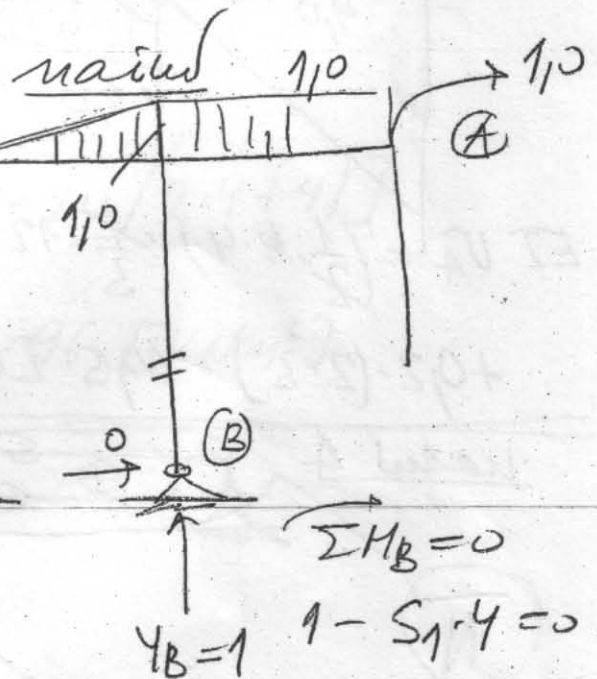
$$4 \cdot 2 - S_1 \cdot 4 = 0$$



youw

$$\sum M_B = 0$$

$$1 \cdot 4 - S_1 \cdot 4 = 0$$



$$U_A = \int \frac{M \cdot \bar{M}}{EI} ds + \int \frac{N \cdot \bar{N}}{EF} ds \quad S_1 = 1/4$$

$$EI U_A = \frac{I_c}{I_c} \int M \cdot \bar{M} ds + \left(\frac{I}{F} \right) \int N \cdot \bar{N} ds$$

$$EI U_A = -\frac{1}{2} \cdot 4 \cdot 4 \cdot 16 + \frac{1}{2} \cdot 4 \cdot 4 \cdot \frac{2}{3} \cdot 8 +$$

$$+ 0,1 \cdot (1 \cdot 6) \cdot 2 \quad [kNm^3]$$

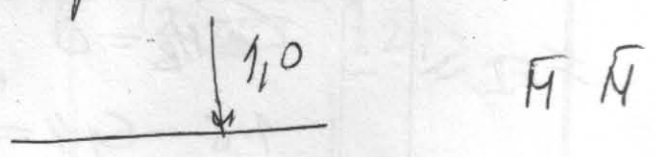
$$U_A = \frac{1}{EI} (-84,133 \text{ kNm}^3)$$

$$EI \varphi_A = -1 \cdot 4 \cdot 16 + \frac{1}{2} \cdot 1 \cdot 4 \cdot \frac{2}{3} \cdot 8 + 0,1 \cdot \left(\frac{1}{4} \cdot 6 \right) \cdot 2 \quad [kNm^2]$$

$$\varphi_A = -\frac{1}{EI} 53,035$$

Томографи

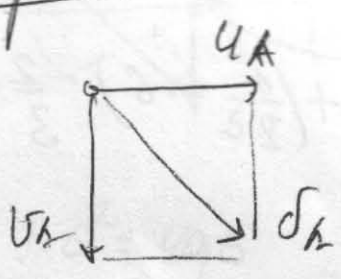
1. вертикално томографи - улис (УА)



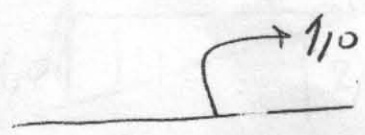
2. хоризонтално томографи (УА)



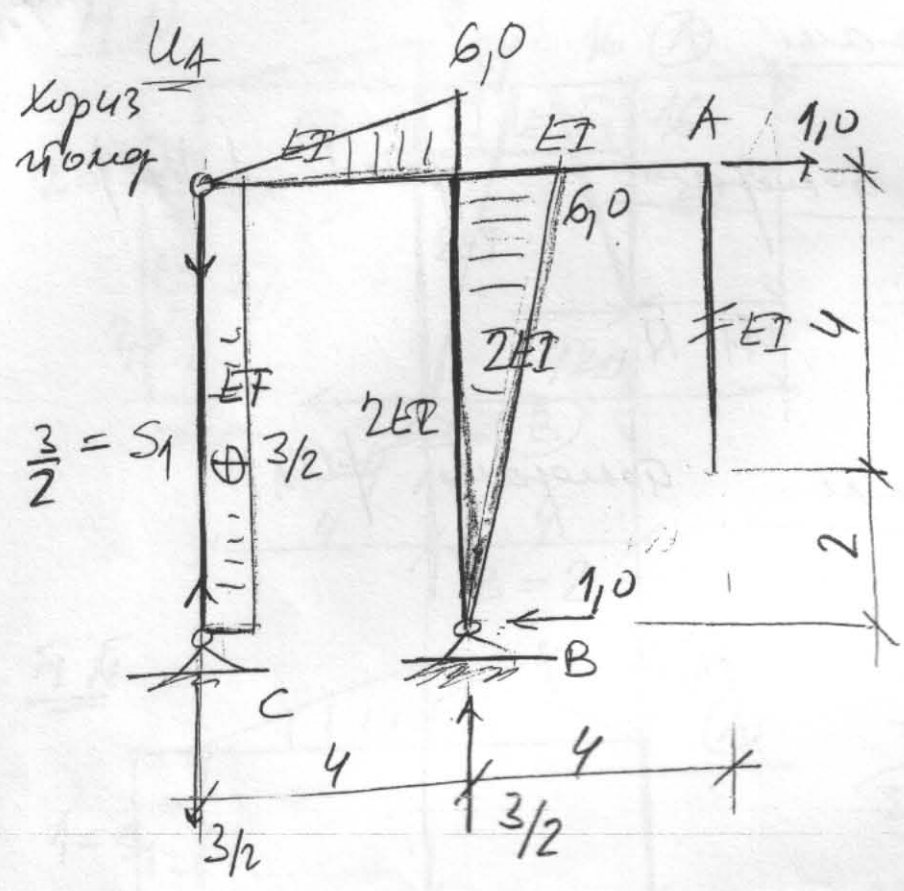
3. томографи



4. одфитане - ротационо - кадис



ММ



$$\sum M_B = 0$$

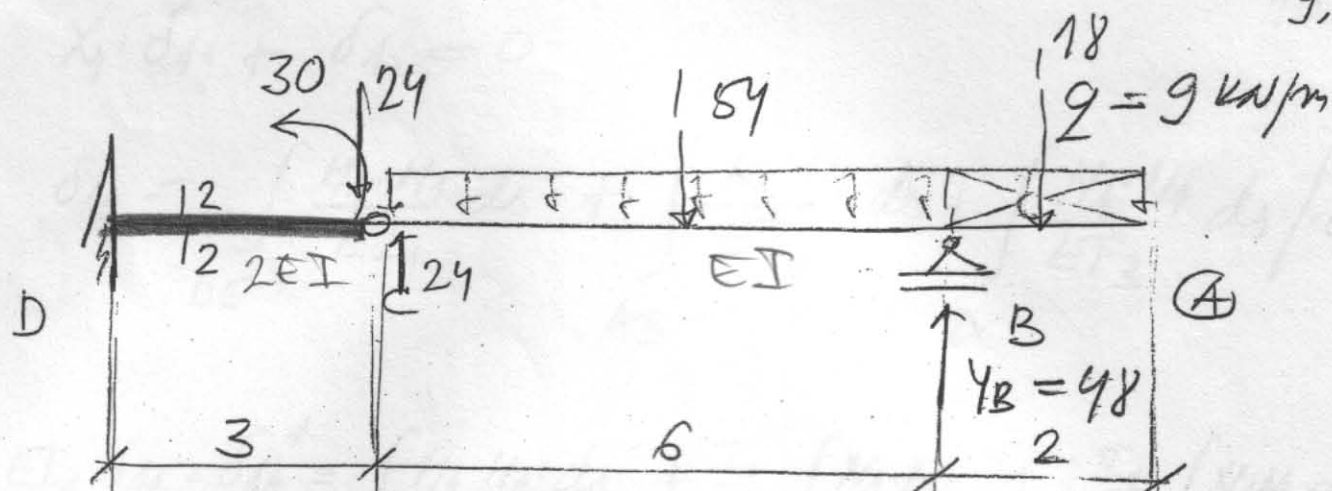
$$1 \cdot 6 - S_1 \cdot 4 = 0$$

$$S_1 = \frac{6}{4} = \frac{3}{2}$$

$$U_A = \frac{1}{EI} \left\{ \frac{1}{2} \cdot \left(\frac{1}{2} \cdot 6 \cdot 6 \right) \cdot \frac{2}{3} \cdot 24 + \left(\frac{1}{2} \cdot 4 \cdot 6 \right) \cdot \frac{2}{3} \cdot 8 + \right.$$

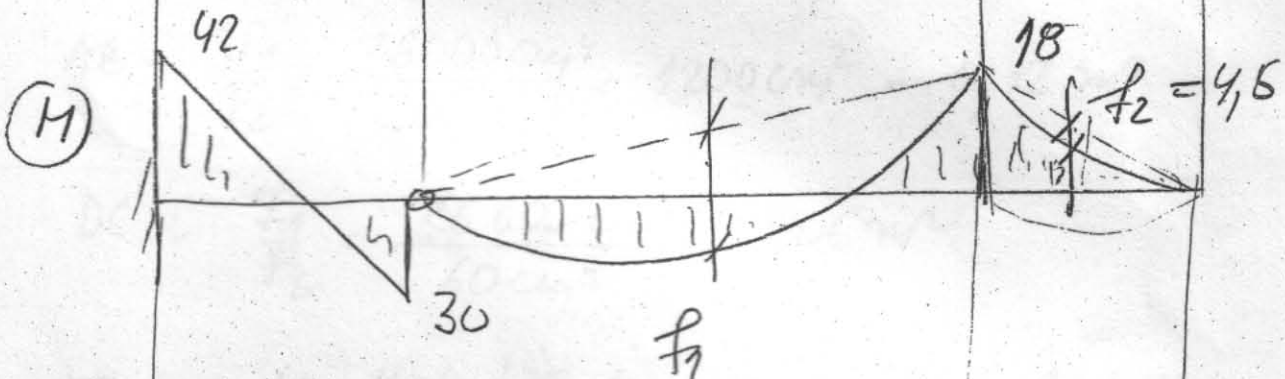
$$\left. + 0,1 \cdot \left(\frac{3}{2} \cdot 6 \right) \cdot 2 \right\}$$

$$\delta_A = \sqrt{U_A^2 + U_A^2}$$



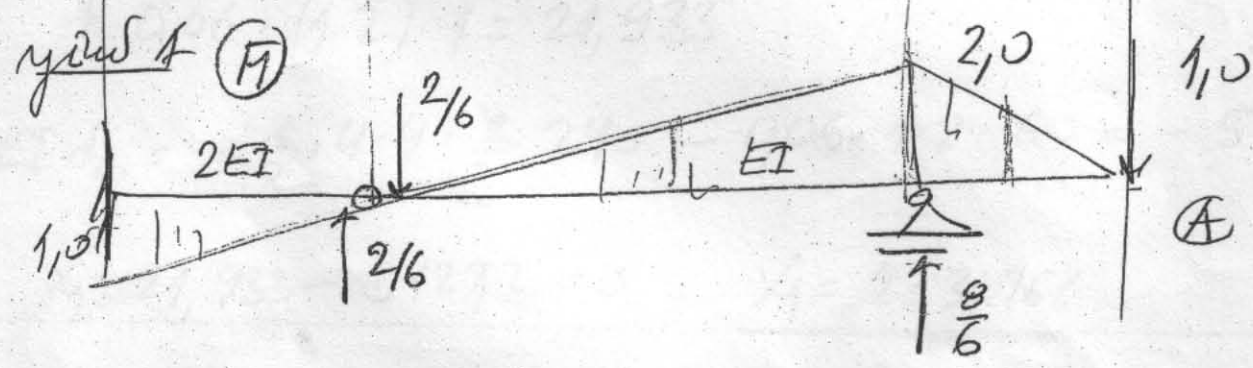
$\sum H_c = 0$

$$54 \cdot 3 + 18 \cdot 7 - Y_B \cdot 6 = 0$$



$$f_1 = \frac{1}{8} \cdot 9 \cdot 6^2 = 40,5$$

$$f_2 = \frac{1}{8} \cdot 9 \cdot 2^2 = 4,5$$



$$EI U_A = \left(\frac{1}{2} \cdot 2 \cdot 2 \right) \cdot \frac{2}{3} \cdot 18 - \frac{2}{3} \cdot 2 \cdot 4,5 \cdot 1,0 +$$

$$+ \left(\frac{1}{2} \cdot 6 \cdot 2 \right) \cdot \frac{2}{3} \cdot 18 - \frac{2}{3} \cdot 6 \cdot 40,5 \cdot 1,0 +$$

$$+ \frac{1}{2} \cdot \frac{3}{6} [11 - 2 \cdot 42 + 30] \text{ kNm}^3$$

$$X_1 \cdot \delta_{11} + \delta_{10} = 0$$

$$\delta_{11} = \int_{DE} \frac{M_1 \cdot M_1}{EI_1} ds + \int_{AB} \frac{N_1 \cdot N_1}{EF_2} ds + \int_{DC} \frac{N_1 \cdot N_1}{EF_3} ds \cdot E$$

$$EI_1 \cdot \delta_{11} = \delta_{11}^* = \int_{DE} M_1 \cdot M_1 ds + \frac{I_1}{F_2} \int_{AB} N_1 \cdot N_1 ds + \frac{I_1}{F_3} \int_{DC} N_1 \cdot N_1 ds$$

$$AB: \frac{I_1}{F_2} = \frac{36000 \text{ cm}^4}{30 \text{ cm}^2} = 1200 \text{ cm}^2 = 0,12 \text{ m}^2$$

$$DC: \frac{I_1}{F_3} = \frac{36000 \text{ cm}^4}{60 \text{ cm}^2} = 0,06 \text{ m}^2$$

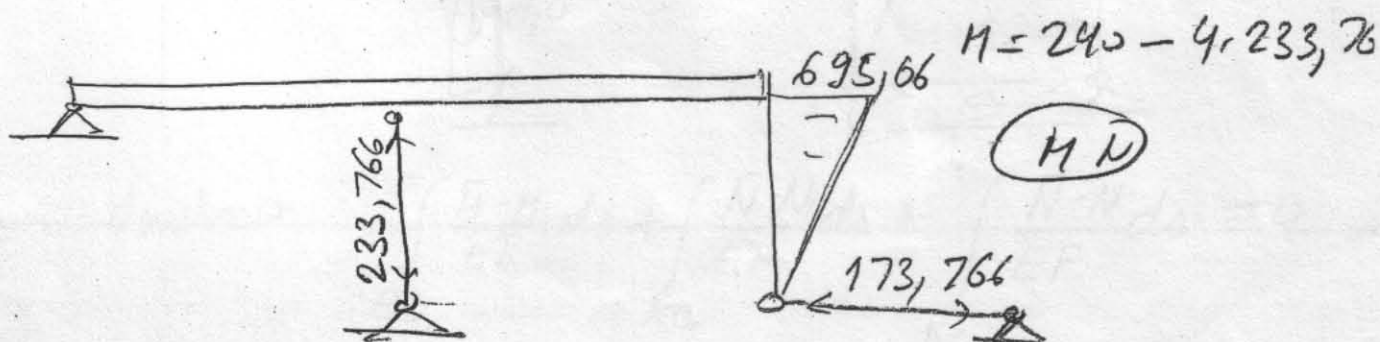
$$EI \delta_{11} = \left(\frac{1}{2} \cdot 4 \cdot 4 \right) \cdot \frac{2}{3} \cdot 4 + 0,12 \cdot (1 \cdot 4) \cdot 1 + 906 \cdot (1 \cdot 2) \cdot 1 = 21,933$$

$$EI \delta_{10} = -\frac{1}{2} \cdot 4 \cdot 4 \cdot \frac{2}{3} \cdot 240 - 906 \cdot 1 \cdot 2 \cdot 60 = -5127,2$$

$$X_1 \cdot 21,933 - 5127,2 = 0 \quad \underline{X_1 = 233,766}$$

$$M = M_0 + X_1 \cdot M_1$$

$$N = N_0 + X_1 \cdot N_1$$



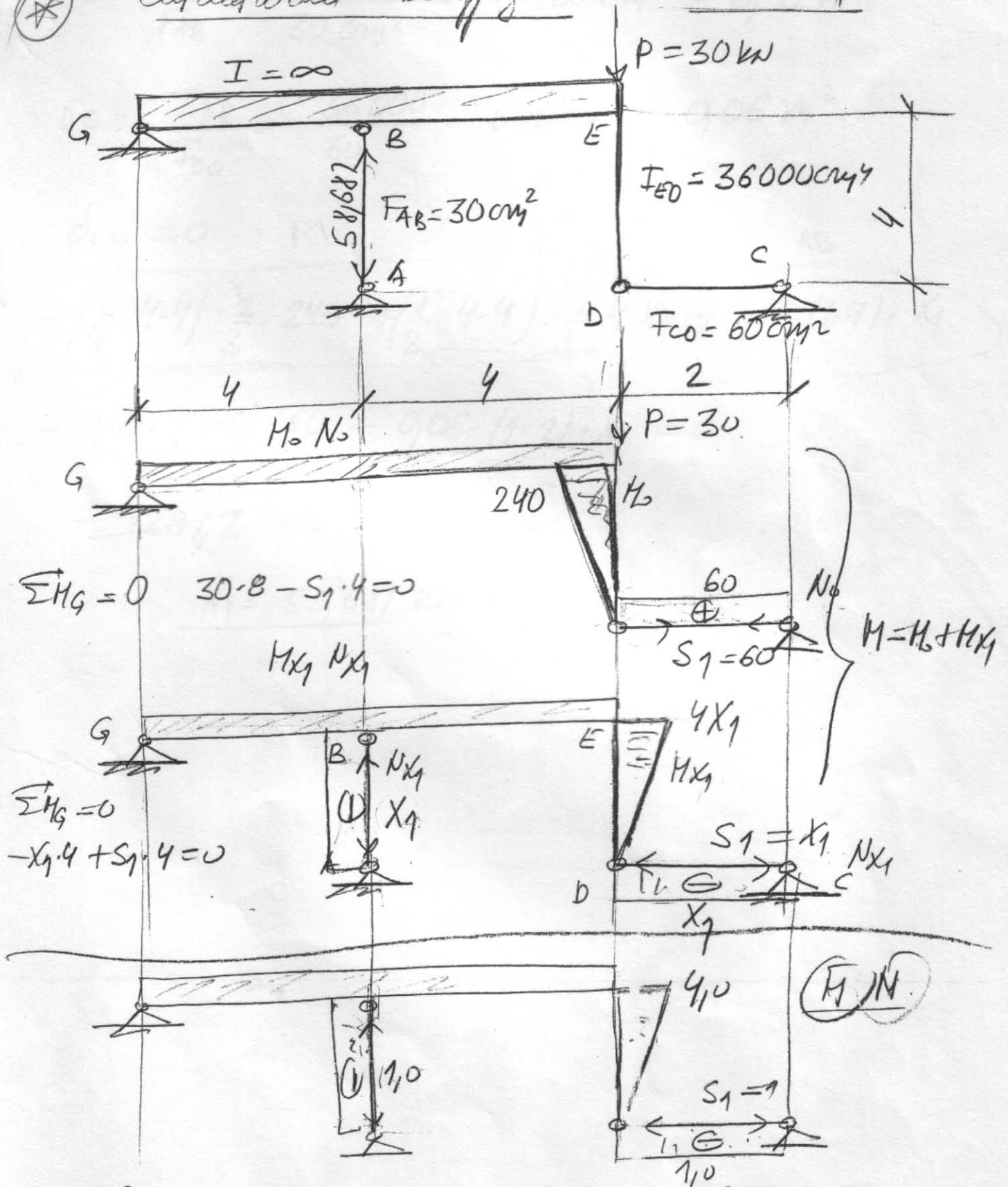
$$S = 60 - 1 \cdot 233,766 = -173,766$$



Ситуациями кривоуголени

$$M = H_0 + M_{X_1}$$

11.



$$\sum M_G = 0 \quad 30 \cdot 8 - S_1 \cdot 4 = 0$$

M_{X_1} N_{X_1}

$$\sum M_G = 0$$

$$-X_1 \cdot 4 + S_1 \cdot 4 = 0$$

$$\delta_{k\omega} = 0$$

$$\int_{EB} \frac{M \cdot M}{EI} ds + \int_{AB} \frac{N \cdot N}{EF} ds + \int_{DC} \frac{N \cdot N}{EF} ds = 0$$

$$M = H_0 + M_{X_1}$$

$$N = N_0 + N_{X_1}$$

$$AB = \frac{I_{DE}}{F_{AB}} = \frac{36000 \text{ cm}^4}{30 \text{ cm}^2} = 1200 \text{ cm}^2 = 0,12 \text{ m}^2 \quad 12.$$

$$DC = \frac{I_{DE}}{F_{DC}} = \frac{36000}{60} = 600 \text{ cm}^2 = 0,06 \text{ m}^2$$

$$\delta_{\text{skid}} = 0 \quad M$$

AB

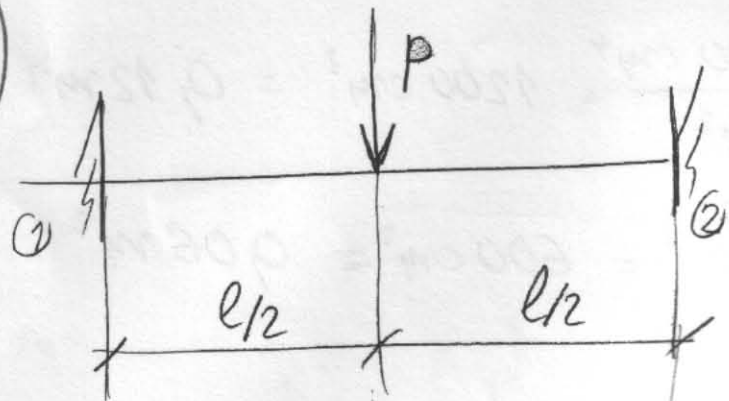
$$-\left(\frac{1}{2} \cdot 4 \cdot 4\right) \cdot \frac{2}{3} \cdot 240 + \left(\frac{1}{2} \cdot 4 \cdot 4\right) \cdot \frac{2}{3} \cdot 4 X_1 + 0,12 \cdot (1 \cdot 4) \cdot X_1$$

$$- 9,06 \cdot (1 \cdot 2) \cdot 60 + 0,06 \cdot (1 \cdot 2) \cdot X_1 = 0$$

$$\begin{array}{r} 1286,72 \\ - 1287,2 \\ \hline \end{array} + 21,933 X_1 = 0$$

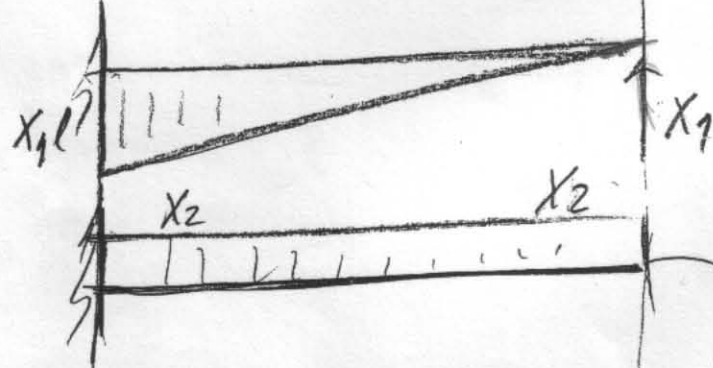
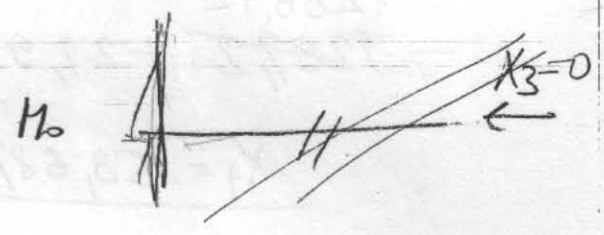
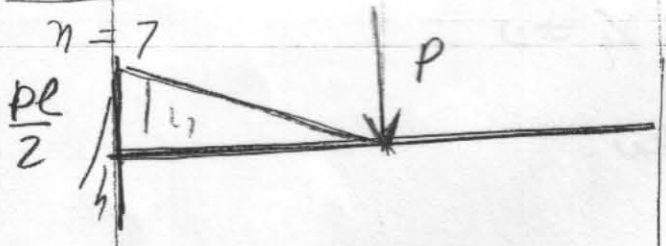
$$\underline{X_1 = 58,687 \text{ kN}}$$

(4)

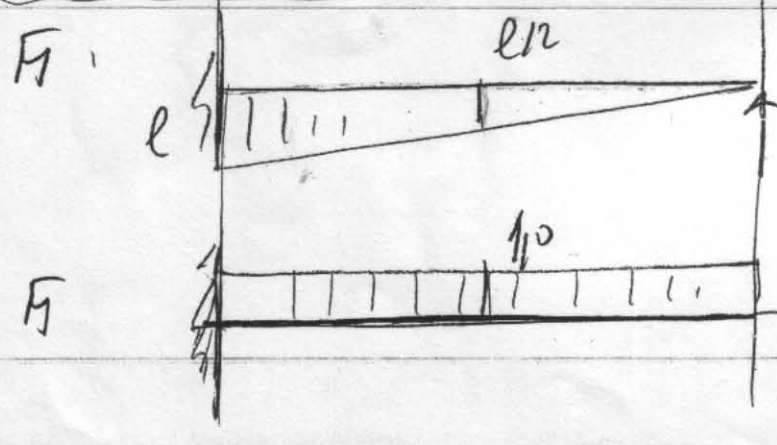


$Z_5 = 1$
 $Z_6 = 4$
 $Z_7 = 2$
 $Z_8 = 0$

Определим жесткость рамы
 $r = 2k = 2 \cdot 2 = 4$



HX_1
 X_1
 HX_2
 X_2



$(B) \quad W_B = 0$
 $\varphi_B = 0$

$$(1) w_B = 0$$

$$M = M_0 + M_{X_1} + M_{X_2}$$

14-

$$\int \frac{\overline{M} \cdot M}{EI} ds = 0$$

$$-\frac{1}{6} \frac{l}{2} \left[\frac{Pl}{2} \left(2l + \frac{l}{2} \right) \right] + \frac{1}{2} \cdot ll \cdot \frac{2}{3} X_1 l - \frac{1}{2} ll \cdot X_2 = 0$$

$$(2) \varphi_B = 0$$

$$\frac{1}{2} \frac{l}{2} \cdot \frac{Pl}{2} \cdot 1 - \frac{1}{2} l \cdot X_1 l \cdot 1 + 1l \cdot X_2 = 0$$

$$-\frac{5}{48} Pl^3 + \frac{1}{3} X_1 l^3 - \frac{1}{2} X_2 l^2 = 0 \quad | : l^2 \quad | \cdot 48$$

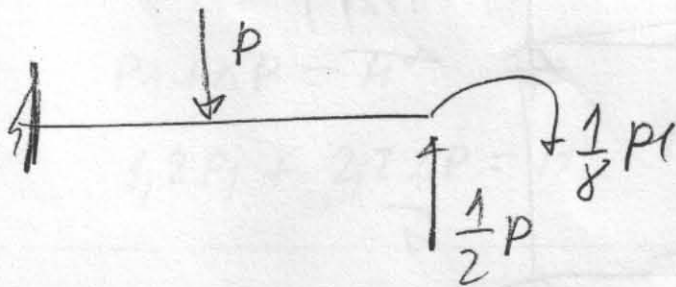
$$\frac{1}{8} Pl^2 - \frac{1}{2} X_1 l^2 + X_2 l = 0 \quad | : l \quad | \cdot 8$$

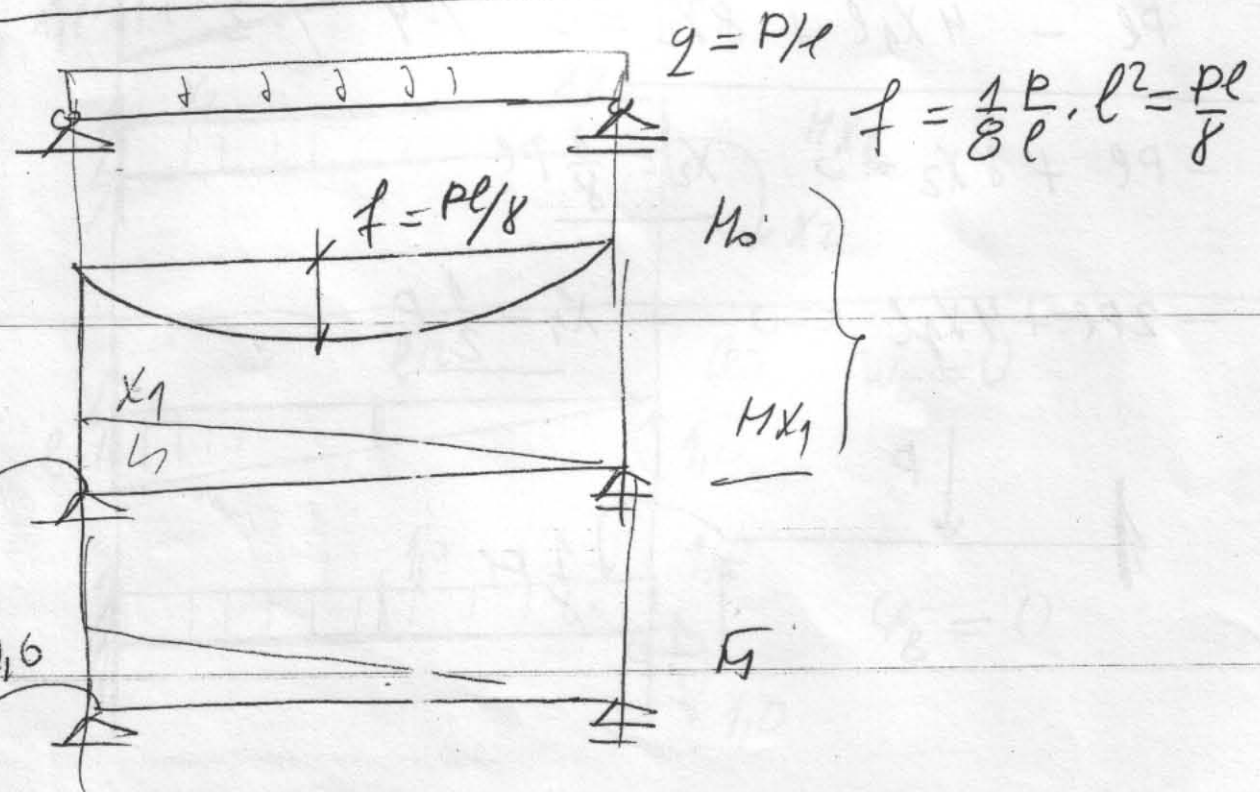
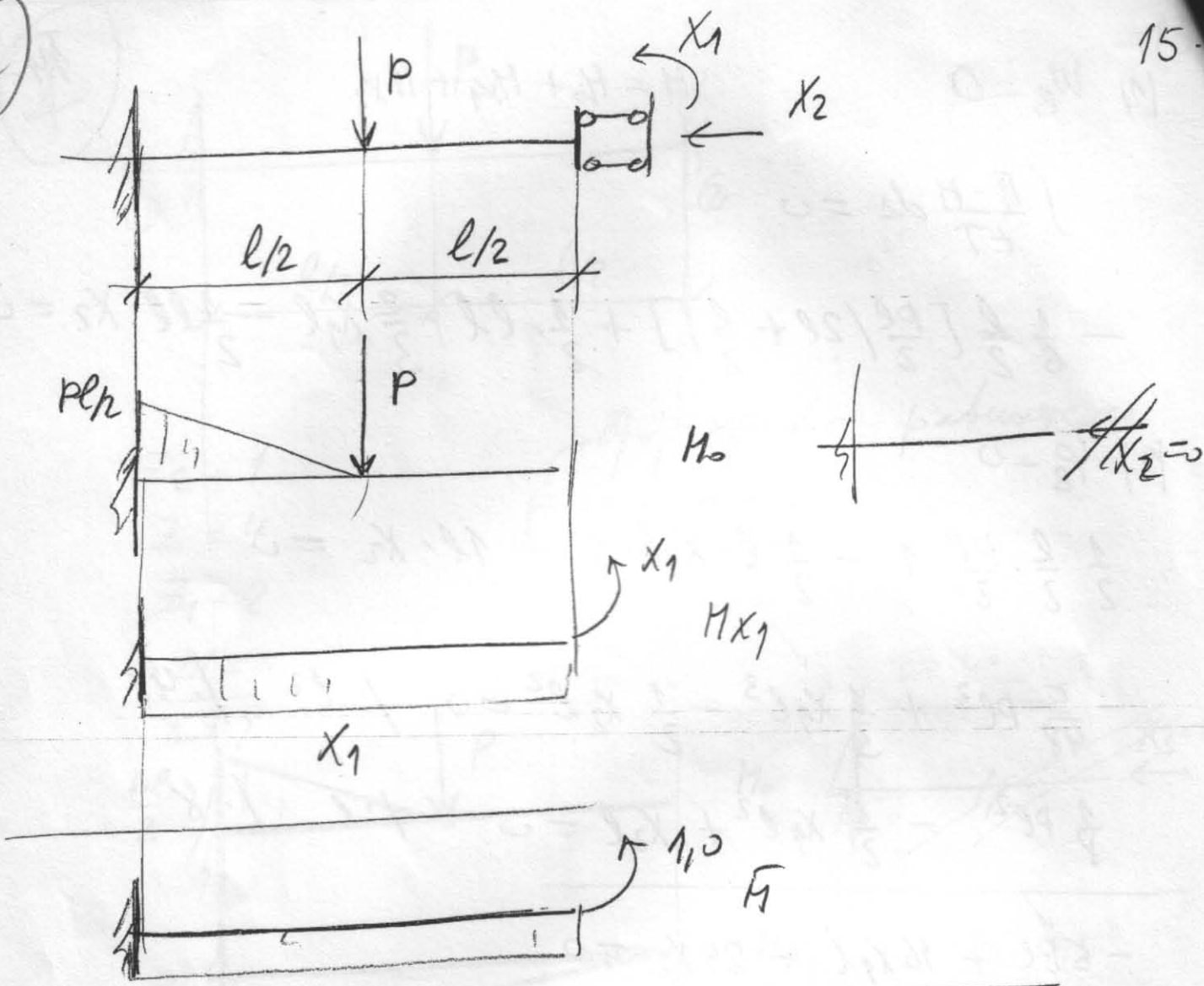
$$-5Pl + 16X_1 l - 24X_2 = 0$$

$$Pl - 4X_1 l + 8X_2 = 0 \quad | \cdot 4 \quad | \cdot 3$$

$$-Pl + 8X_2 = 0 \quad \underline{X_2 = \frac{1}{8} Pl}$$

$$-2Pl + 4X_1 l = 0 \quad \underline{X_1 = \frac{1}{2} P}$$

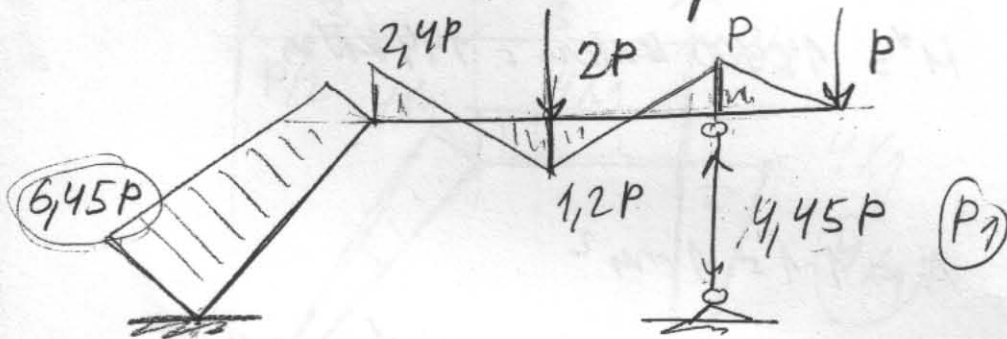




Сила лонс P^* конец конец конец конец 16.

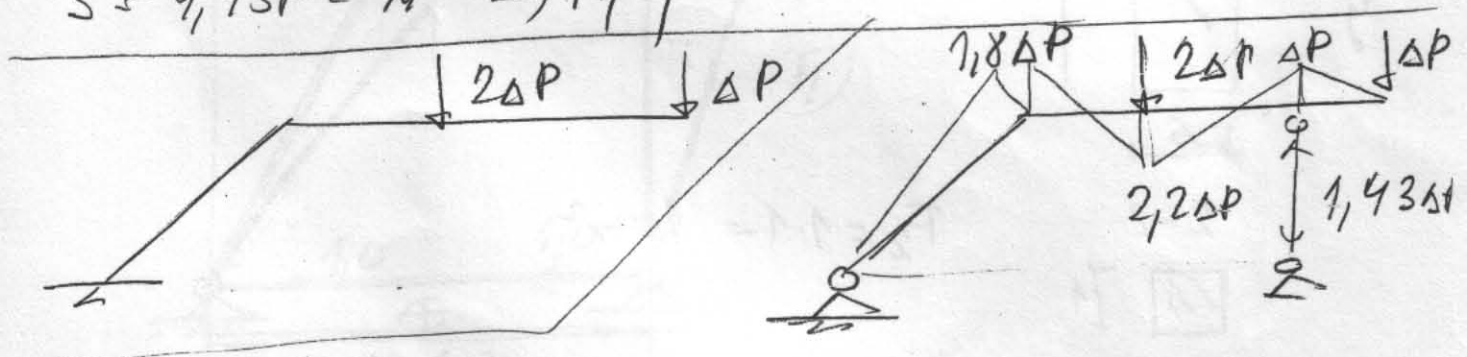
$W^* = \sum A \cdot d_{n-n}$ $M^* = W^* \cdot \sigma_T$ средний исполн

$N^* = A \cdot \sigma_T$ за просека ушиканья



Треть конец

$\max M \ 6,45P = M^* \Rightarrow P_1$
 $S = 4,45P = N^* \Rightarrow P_1$ } $\min P_1 = \underline{\underline{P_1}}$



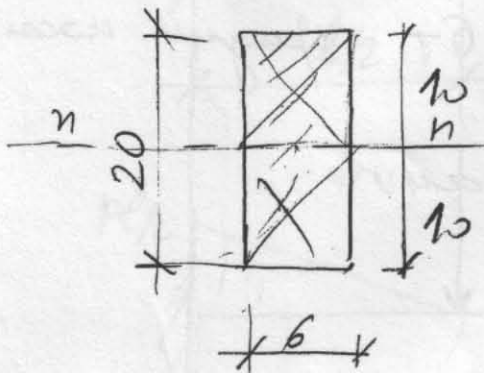
$4,45P_1 + 1,43\Delta P = N^*$
 $P_1 + \Delta P = M^*$
 $1,2P_1 + 2,2\Delta P = M^*$ } $\min \Delta P = \underline{\underline{\Delta P}}$

$P^* = P_1 + \Delta P$

$$\sigma_T = 240 \text{ MPa} = 24 \frac{\text{kJ}}{\text{cm}^2}$$

17-

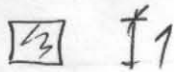
1-1



$$W^* = (6 \cdot 10 \cdot 5) \cdot 2 = 600 \text{ cm}^3$$

$$M^* = W^* \cdot \sigma_T = 600 \text{ cm}^3 \cdot 24 \frac{\text{kJ}}{\text{cm}^2}$$

$$M^* = 14400 \text{ kJ/cm} = 144 \text{ kNm}$$

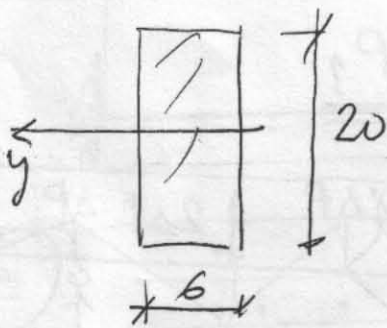


$$A = 1 \cdot 1 = 1 \text{ cm}^2$$



$$N^* = A \sigma_T = 1 \text{ cm}^2 \cdot 24 \frac{\text{kJ}}{\text{cm}^2} = 24 \text{ kN}$$

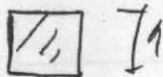
1-1



$$I_y = \frac{6 \cdot 20^3}{12} = 4000 \text{ cm}^4$$

2-2

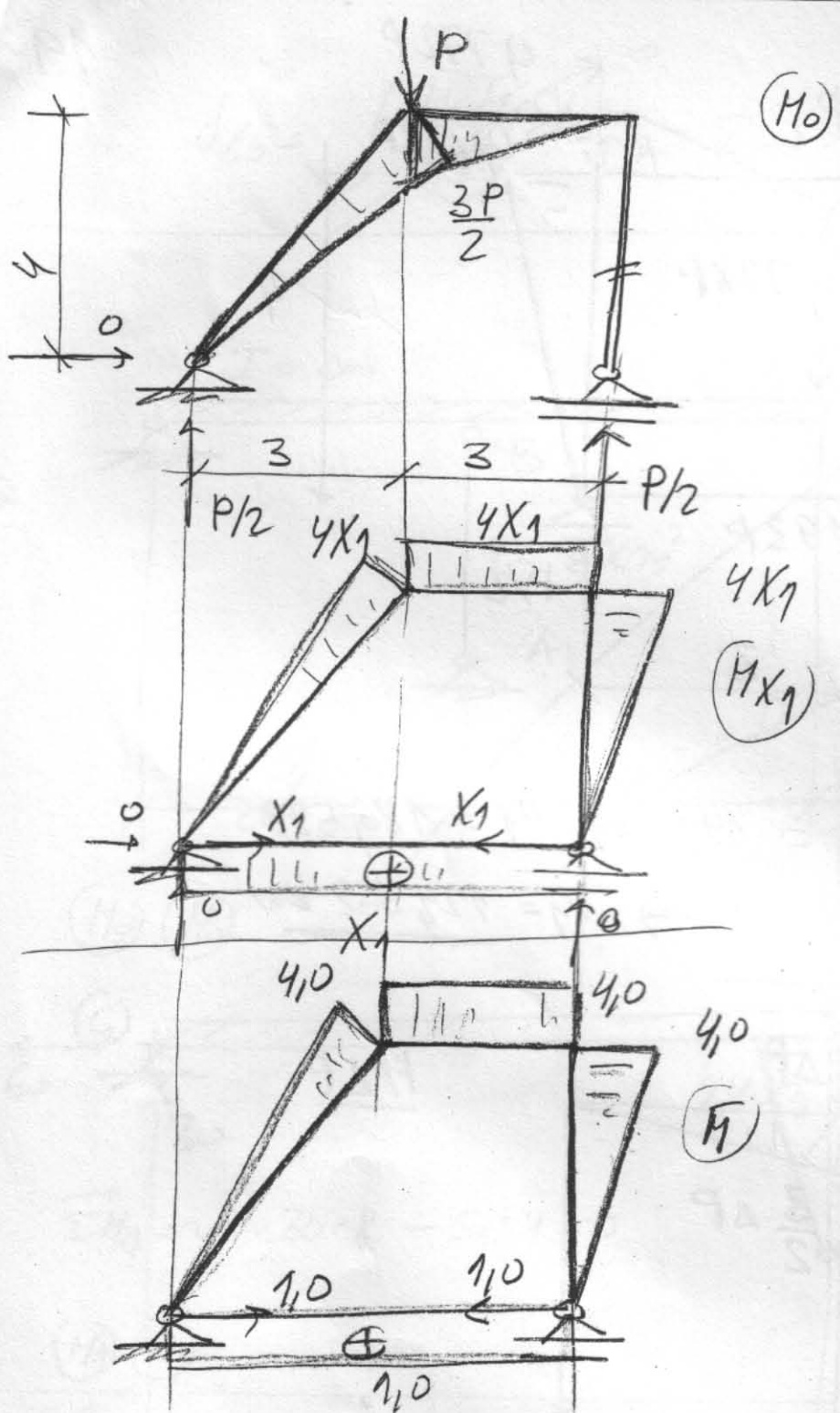
$$F_2 = 1 \cdot 1 = 1 \text{ cm}^2$$



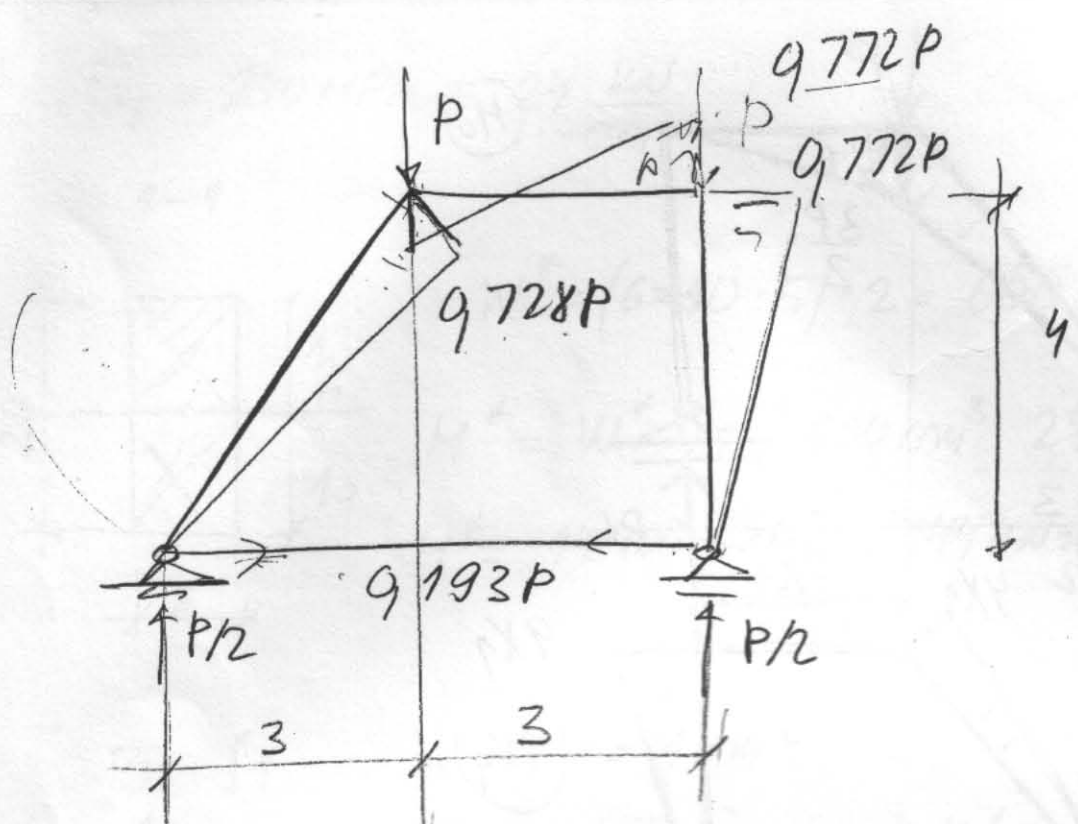
$$\frac{I}{F} = \frac{4000 \text{ cm}^4}{1 \text{ cm}^2} = 4000 \text{ cm}^2 = 0,4 \text{ m}^2$$

wa

$$\begin{aligned} \epsilon_{ij} &= \int_S \frac{N \bar{U}}{E \cdot A} ds + \int_S \frac{M M_y}{E I} ds \quad / \quad \text{Z} \quad \text{I} \\ &= \int_S M M_y ds + \frac{I_y}{A} \int_S N \bar{U} \end{aligned}$$

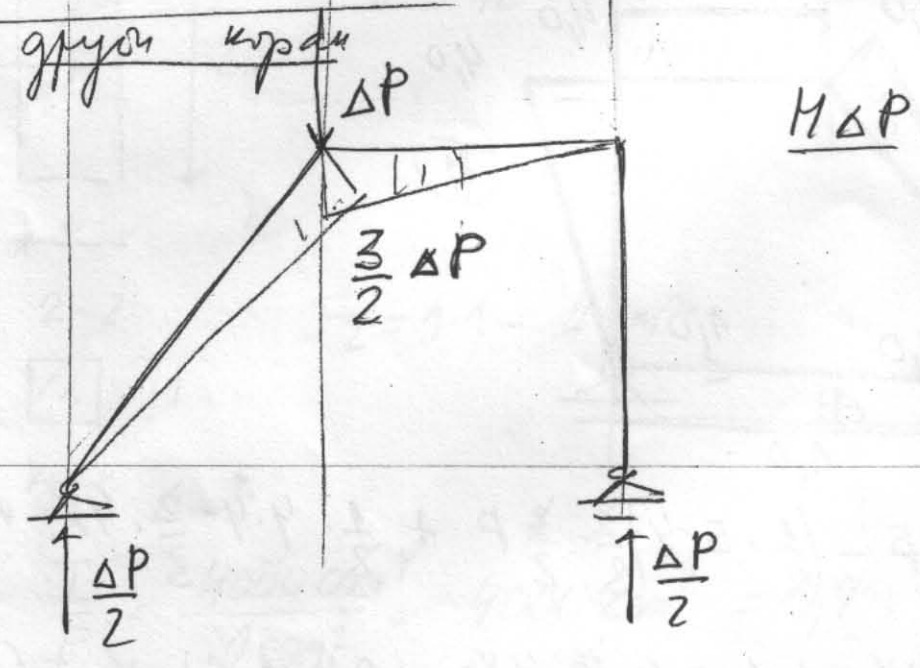


$$\begin{aligned}
 & - (4 \cdot 3) \cdot \frac{3P}{4} - \left(\frac{1}{2} \cdot 5 \cdot 4 \right) \cdot \frac{3}{2} \cdot \frac{3P}{2} + \frac{1}{2} \cdot 4 \cdot 4 \cdot \frac{2}{3} \cdot 4X_1 + \\
 & + (4 \cdot 3) \cdot 4X_1 + \frac{1}{2} \cdot 5 \cdot 4 \cdot \frac{2}{3} \cdot 4X_1 - 9 \cdot 4 \cdot (1 \cdot 6) \cdot X_1 = 0 \\
 & - 19P + 98,4X_1 = 0 \qquad \qquad \qquad X_1 = 0,193P
 \end{aligned}$$



$$\max M = 0,772P = 144 \Rightarrow P_1 = 186,5285$$

$$S = 0,193P = 24 \Rightarrow P_1 = \underline{124,352 \text{ kN}}$$



$$0,728P_1 + \frac{3}{2} \Delta P = 144$$

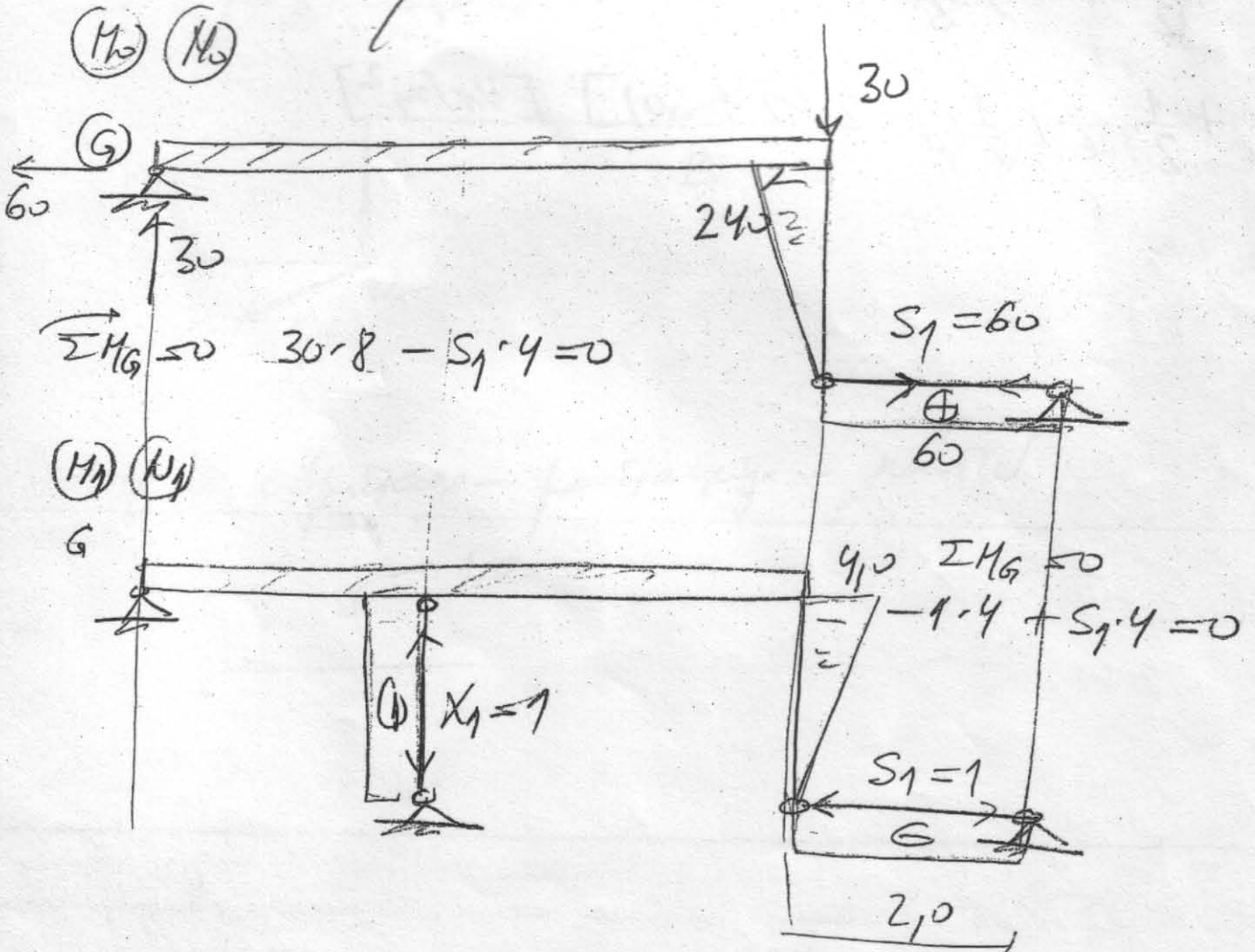
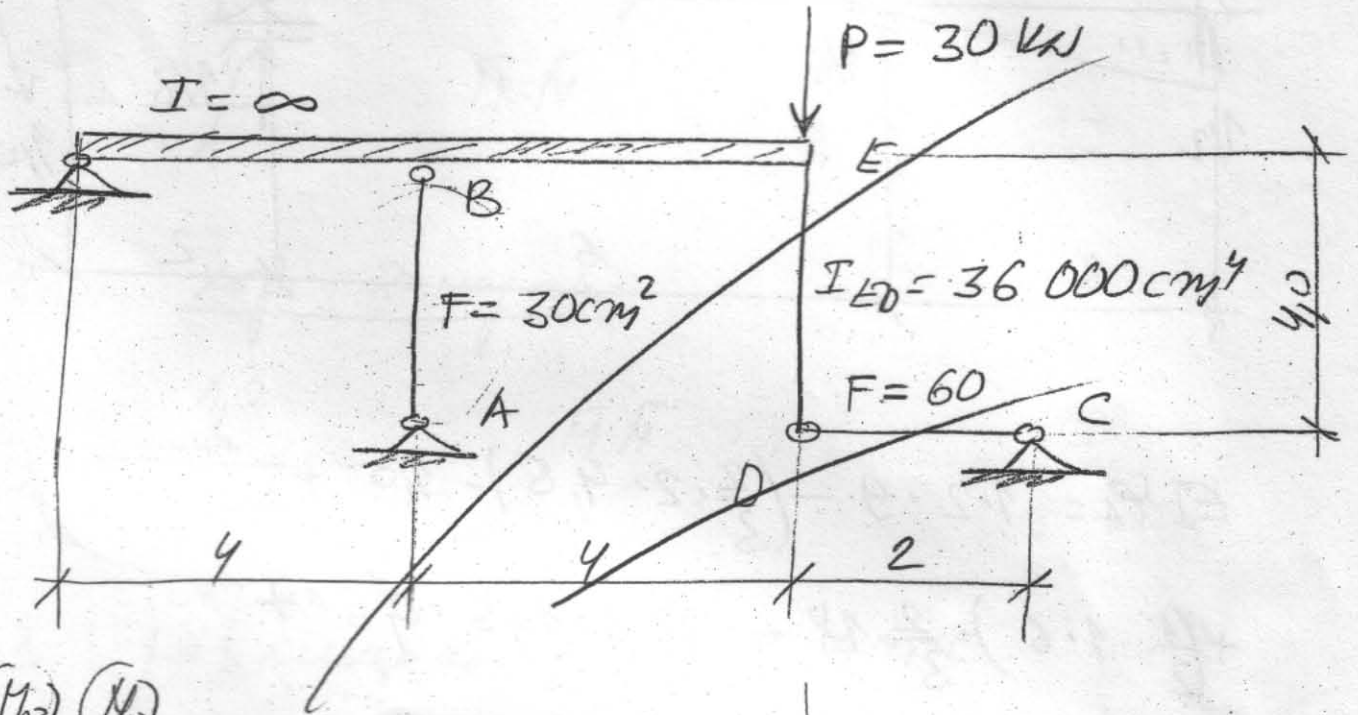
$$0,728 \cdot (124,352) + \frac{3}{2} \Delta P = 144$$

$$\underline{\Delta P = 35,6478}$$

$$P^* = P_1 + \Delta P = \underline{160 \text{ kN}}$$

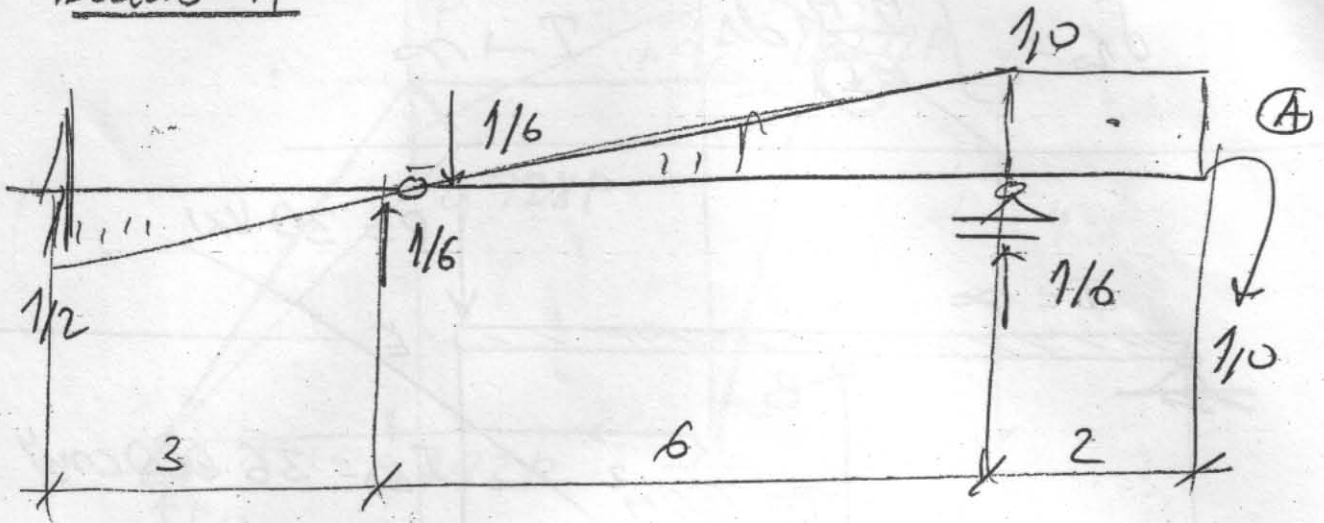
$$\delta_{10} = \int \frac{M \cdot M_0}{EI} ds \quad I \rightarrow \infty$$

11.

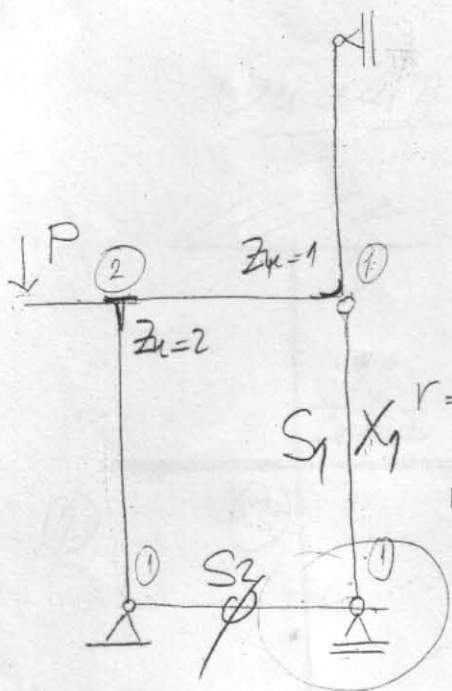


Ward A

12.



$$\begin{aligned}
 EI \varphi_A = & 1 \cdot 2 \cdot 9 - \left(\frac{2}{3} \cdot 2 \cdot 9,5 \right) - 1,0 + \\
 & + \left(\frac{1}{2} \cdot 1 \cdot 6 \right) \cdot \frac{2}{3} \cdot 18 - \frac{2}{3} \cdot 6 \cdot 49,5 - 9,5 + \\
 & + \frac{1}{2} \cdot \frac{3}{6} \left[\frac{1}{2} \cdot (-2 \cdot 42 + 30) \right] \text{ [kNm}^2 \text{]}
 \end{aligned}$$



$$Z_s = 6 \checkmark$$

$$Z_o = 4 \checkmark$$

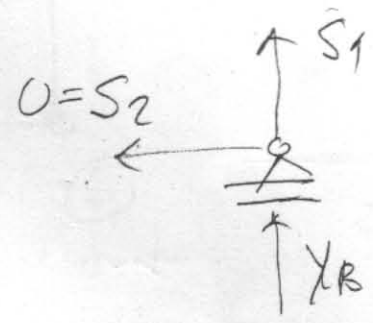
$$Z_u = 0 \checkmark$$

$$Z_k = 3 \checkmark$$

$$n = 13$$

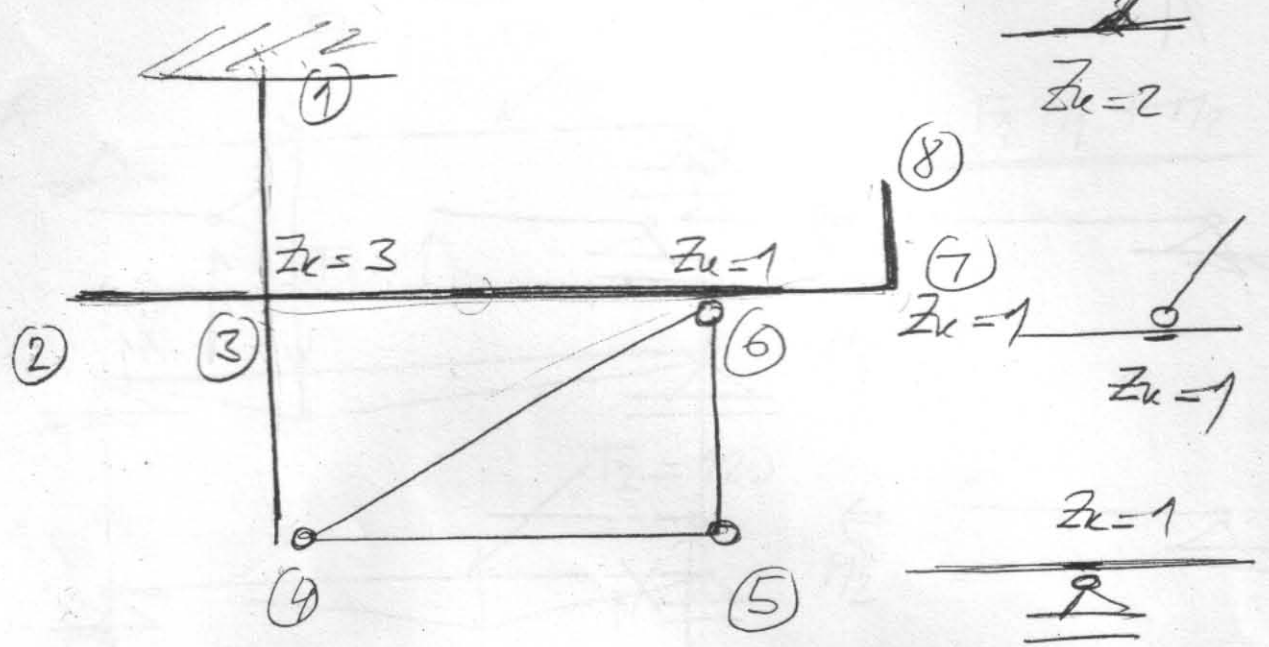
$$r = 2K = 2 \cdot 6 = 12$$

$$n - r = 1 \times \text{CTAT HEQA}$$



topro nuetake

Система ищел неопределенных



неизвестные z_k :

$Z_s = \text{б\text{р}о\text{ж} с\text{л}о\text{ж} н\text{е} \text{з\text{а}д\text{а}ч\text{а}} = 9$

$Z_o = \text{б\text{р}о\text{ж} о\text{с\text{л}о\text{п}н\text{а}р\text{н}н\text{х} о\text{п\text{о}р} = 2$

$Z_u = \text{б\text{р}о\text{ж} м\text{о\text{м\text{е}н\text{т}н\text{а}р\text{н}н\text{х} у\text{з\text{л}о\text{в} = 1$

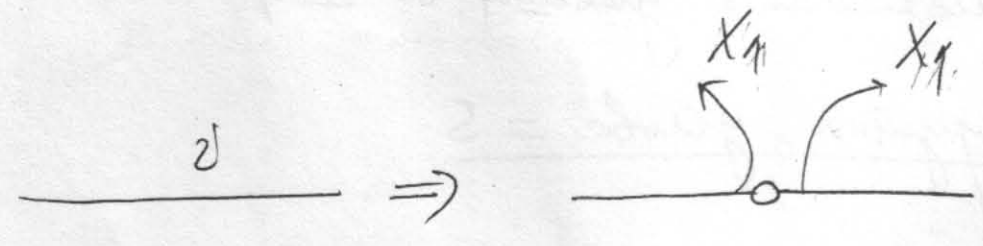
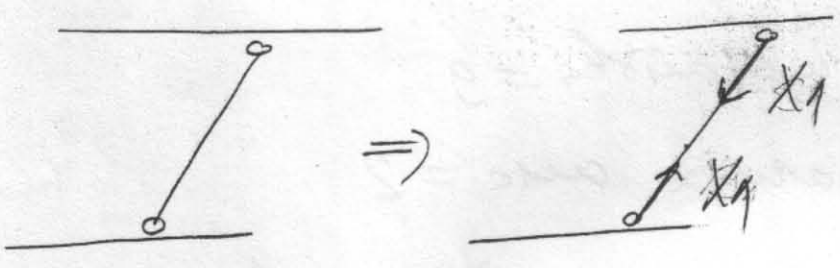
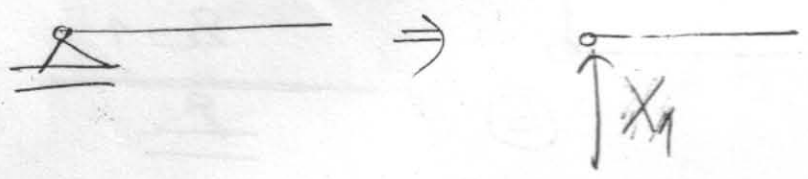
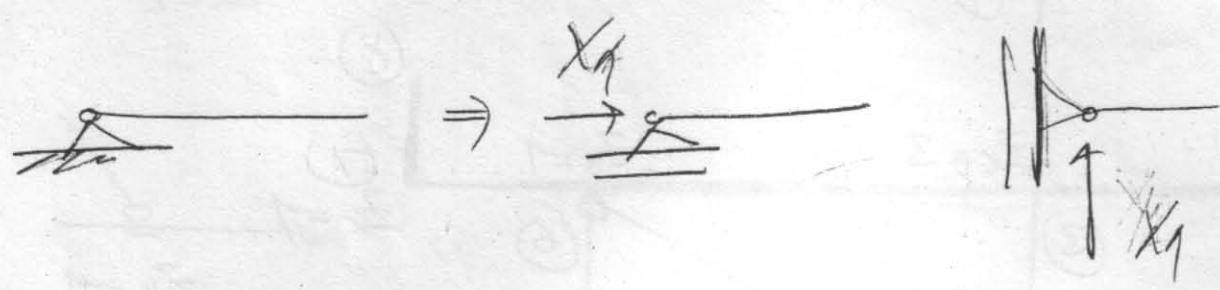
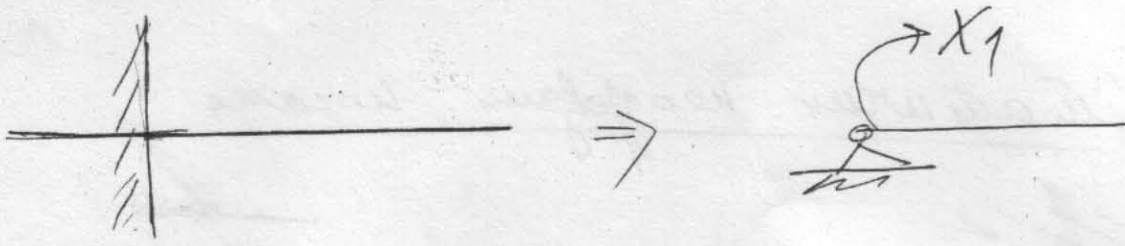
$Z_k = \text{б\text{р}о\text{ж} к\text{р}у\text{ч}н\text{х} у\text{з\text{л}о\text{в} = 5$

$n = 17$

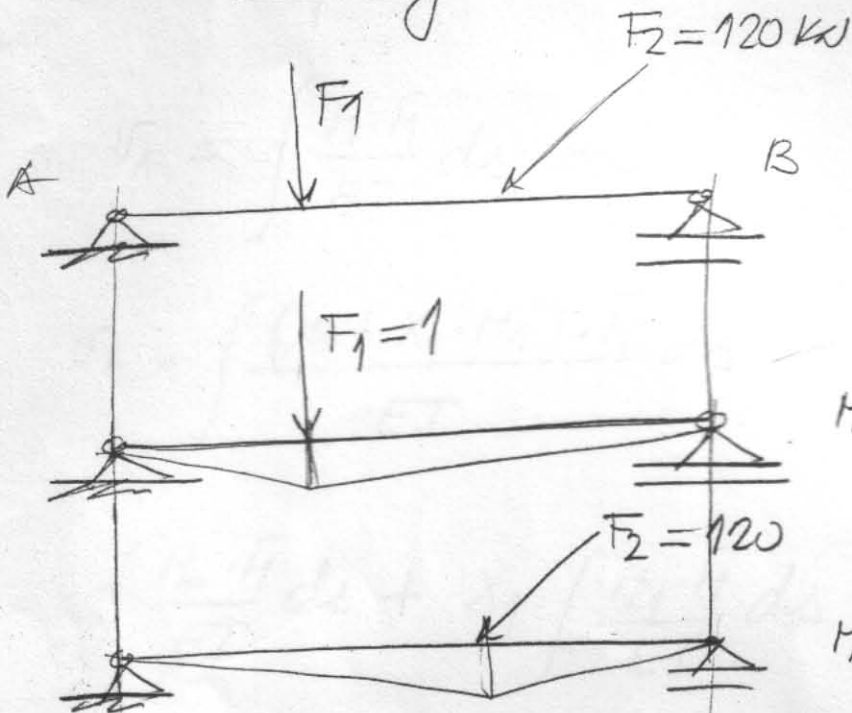
б\text{р}о\text{ж} у\text{с\text{л}о\text{в} р\text{а\text{в}н\text{о}с\text{т}е\text{н}

$r = 2k = 2 \cdot 8 = 16$

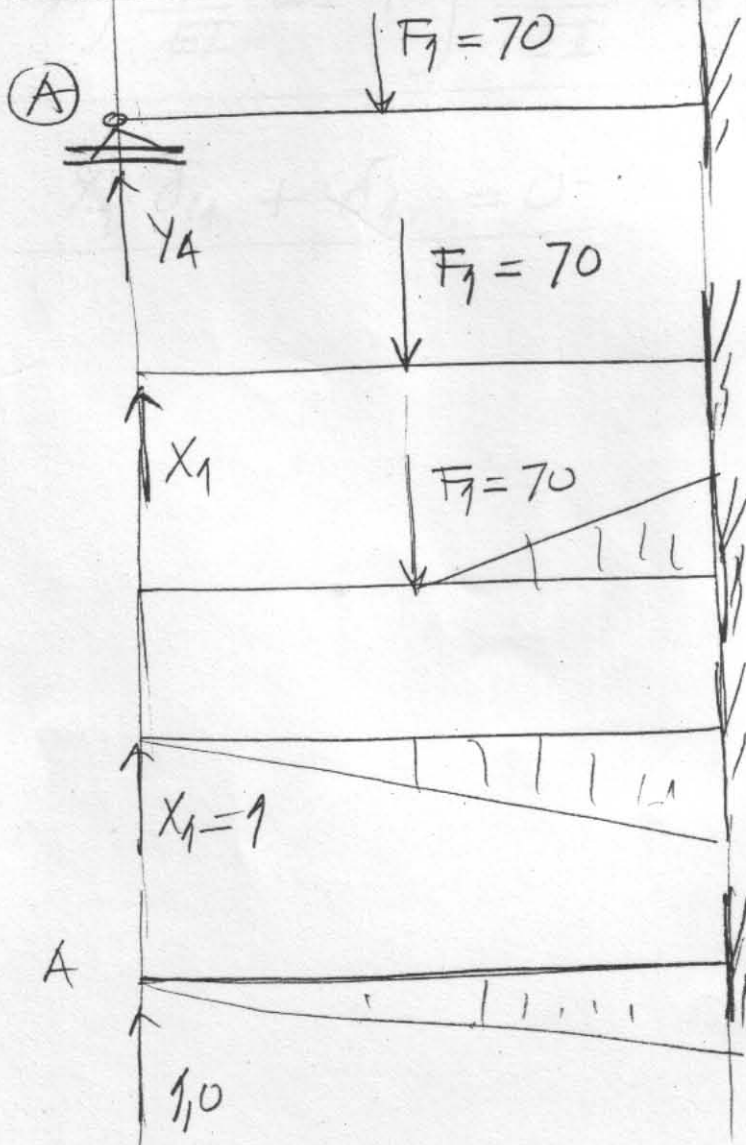
$n - r = 17 - 16 = 1 \times \text{с\text{и}\text{с}\text{т\text{е}\text{м}а} \text{ н\text{е} \text{о\text{п}р\text{е}д\text{е}\text{л}\text{е}\text{н}}$



Membaca cara



$M = F_1 \cdot M_1 + M_2$



$V_A = 0$

$M = M_0 + X_1 \cdot M_1$

(M_0)

(M_1)

(M) = M_1

Поперечное изгибное качение

4.

$$v_A = \int \frac{M \cdot \bar{M}}{EI} ds = 0$$

$$v_A = \int \frac{(M_0 + X_1 \cdot M_1) \cdot \bar{M}}{EI} ds = 0$$

$$\int \frac{M_0 \cdot \bar{M}}{EI} ds + X_1 \int \frac{M_1 \cdot \bar{M}}{EI} ds = 0$$

$$X_1 \int \frac{M_1 \cdot \bar{M}}{EI} ds + \int \frac{M_0 \cdot \bar{M}}{EI} ds = 0$$

$$X_1 \cdot \delta_{11} + \delta_{10} = 0$$

$$X_1 \cdot \delta_{11} + \delta_{10} = 0 \Rightarrow X_1 \quad / \cdot EI \quad 5.$$

$$\left. \begin{aligned} X_1 \cdot \delta_{11} + X_2 \cdot \delta_{12} + \delta_{10} &= 0 \\ X_1 \cdot \delta_{21} + X_2 \cdot \delta_{22} + \delta_{20} &= 0 \end{aligned} \right\} \begin{array}{l} X_1 \\ X_2 \end{array}$$

$$\left. \begin{aligned} X_1 \cdot \delta_{11} + X_2 \cdot \delta_{12} + X_3 \cdot \delta_{13} + \delta_{10} &= 0 \\ X_1 \cdot \delta_{21} + X_2 \cdot \delta_{22} + X_3 \cdot \delta_{23} + \delta_{20} &= 0 \\ X_1 \cdot \delta_{31} + X_2 \cdot \delta_{32} + X_3 \cdot \delta_{33} + \delta_{30} &= 0 \end{aligned} \right\} \begin{array}{l} X_1 \\ X_2 \\ X_3 \end{array}$$

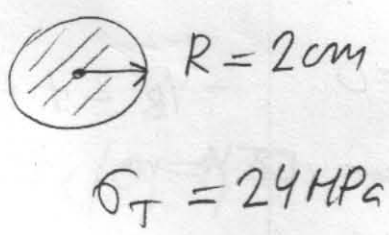
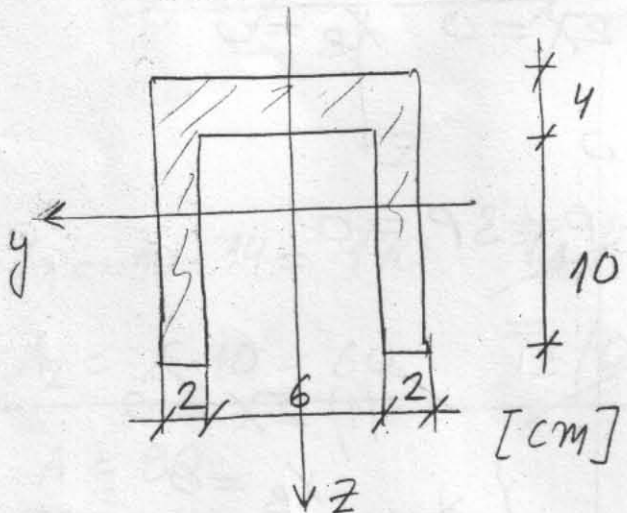
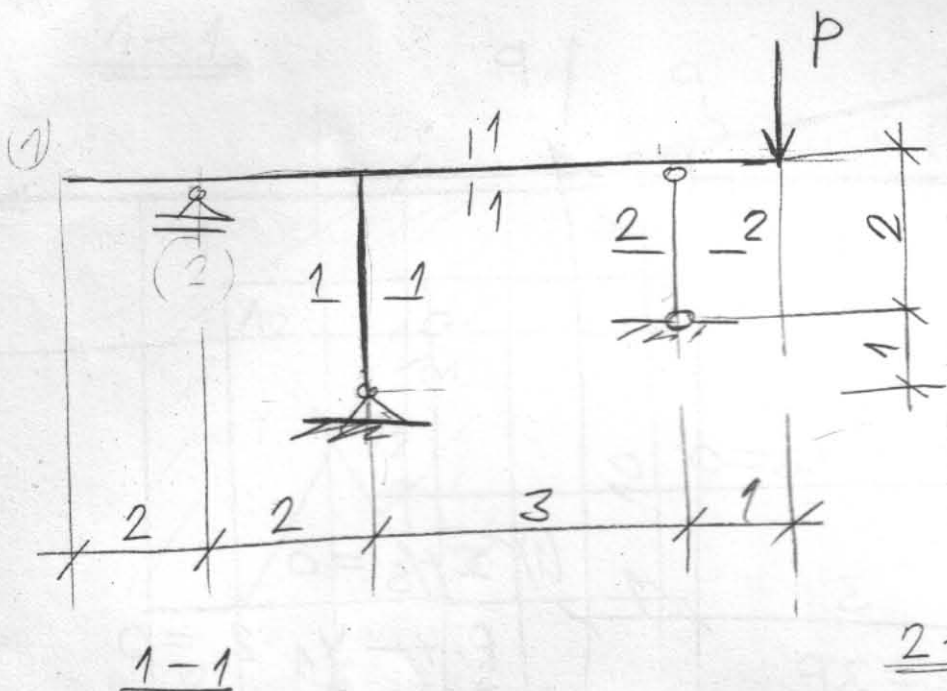
$$\delta_{11} = \int \frac{M_1 \cdot M_1}{EI} ds + \int \frac{N_1 \cdot N_1}{EF} ds \quad / \cdot EI_c$$

$$\delta_{11}' = EI \delta_{11} = \int \frac{I_c}{I_i} M_1 \cdot M_1 ds + \left(\frac{I_c}{F_c} \right) \int N_1 \cdot N_1 ds$$

$$\delta_{12}' = \delta_{21}' =$$

$$I = I_y \quad y \leftarrow \begin{array}{|c|} \hline \diagup \\ \hline \diagdown \\ \hline \end{array}$$

$$FI = b \cdot h \quad \begin{array}{|c|} \hline \diagup \\ \hline \diagdown \\ \hline \end{array} \begin{array}{l} h \\ b \end{array}$$



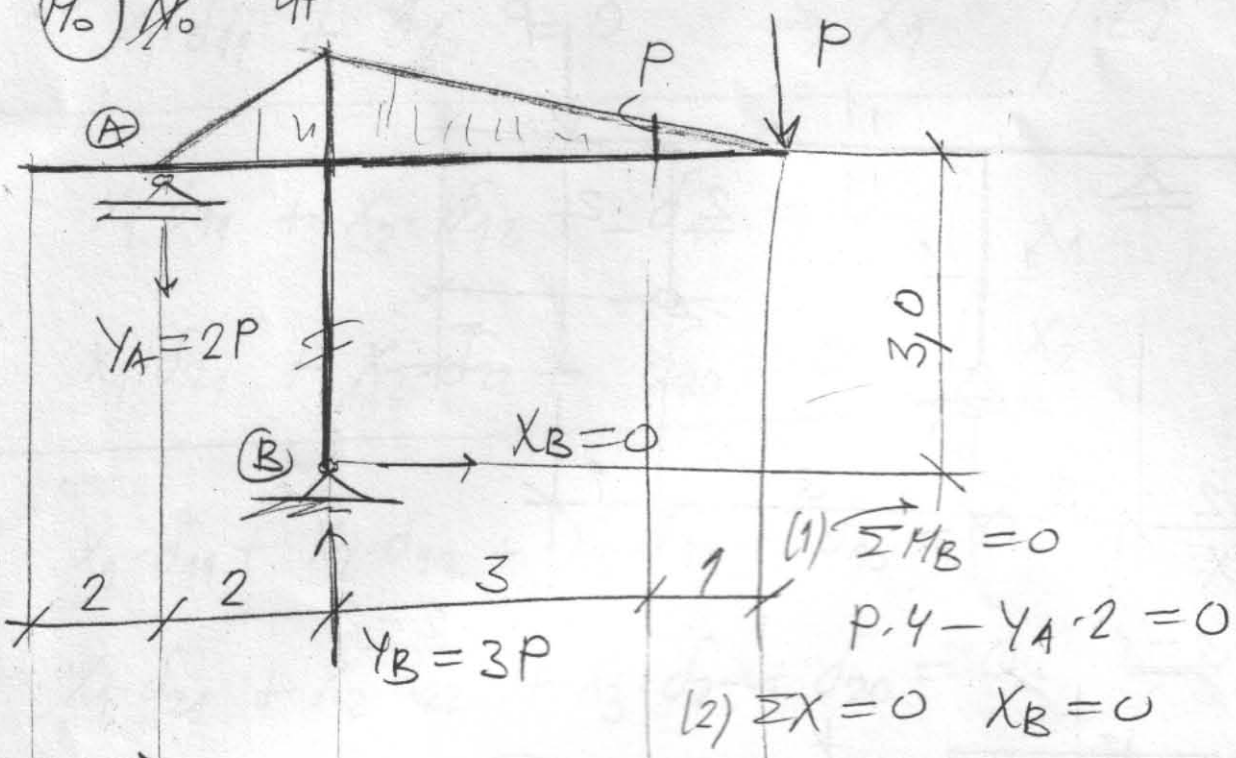
$\sigma_T = 240 \text{ MPa}$ $\sigma_{T \text{ по } z}$ поворота

- $z_5 = 6$
- $z_6 = 5$
- $z_4 = 0$
- $z_k = 4$

- $n = 15$

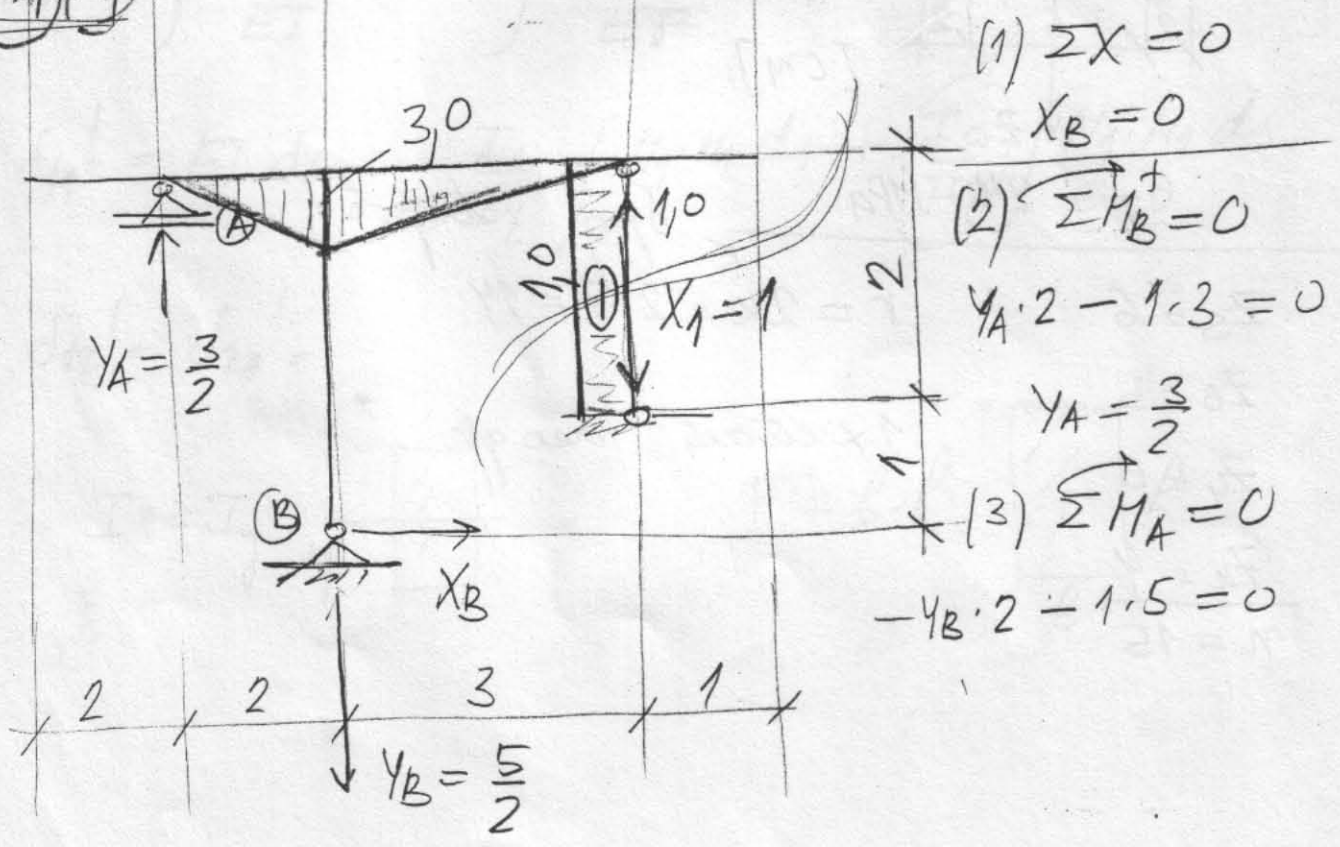
$r = 2k = 2 \cdot 7 = 14$
 1 x сечение не о гр

M_0 No 4P



(3) $\Sigma M_A = 0 \quad -Y_B \cdot 2 + P \cdot 6 = 0$
 Проверка $\Sigma Y = 0 \quad -2P - P + 3P = 0$

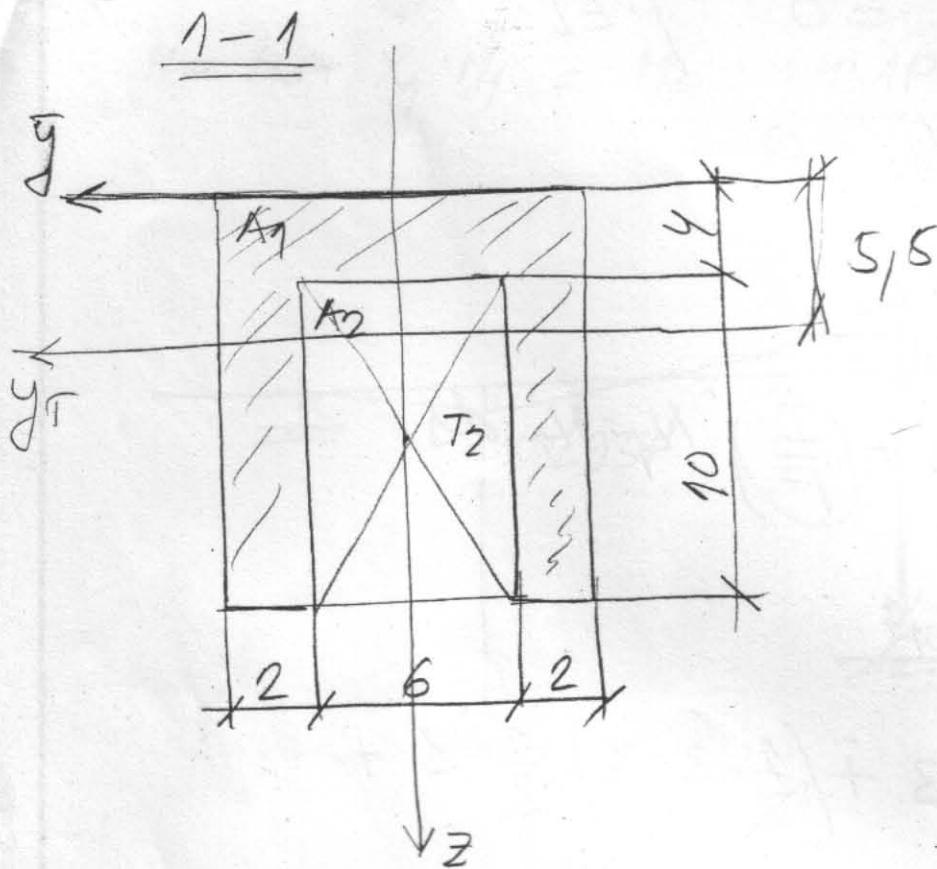
M_1 N_1



(1) $\Sigma X = 0$
 $X_B = 0$

(2) $\Sigma M_B = 0$
 $Y_A \cdot 2 - 1 \cdot 3 = 0$

$Y_A = \frac{3}{2}$
 (3) $\Sigma M_A = 0$
 $-Y_B \cdot 2 - 1 \cdot 5 = 0$



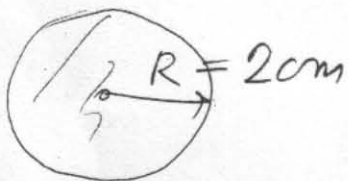
$$A_1 = 10 \cdot 14 = 140 \quad \bar{T}_1 (0; 7) \quad T_1 (0; 1,5)$$

$$A_2 = 6 \cdot 10 = 60 \quad \bar{T}_2 (0; 9) \quad T_2 (0; 3,5)$$

$$A = 80$$

$$\bar{z}_T = \frac{140 \cdot 7 - 60 \cdot 9}{80} = 5,5$$

$$I_y = \frac{10 \cdot 14^3}{12} + 140 \cdot 1,5^2 - \left[\frac{6 \cdot 10^3}{12} + 60 \cdot 3,5^2 \right] = 1366,667 \text{ cm}^4$$



$$A = R^2 \pi = 2^2 \pi = 4\pi \text{ cm}^2$$

$$\frac{I_y}{F} = \frac{1366,667 \text{ cm}^4}{4\pi \text{ cm}^2} = 108,7558778 \text{ cm}^2 = 0,01088 \text{ m}^2$$

$$X_1 \cdot \delta_{11} + \delta_{10} = 0 \quad / \cdot EI$$

9.

$$X_1 \cdot EI \delta_{11} + EI \delta_{10} = 0$$

$$(1) \quad \underline{X_1 \cdot \delta_{11}' + \delta_{10}' = 0}$$

$$\delta_{11}' = \int M_1 \cdot M_1 \, ds + \left(\frac{I}{F} \right) \int N_1 \cdot N_1 \, ds$$

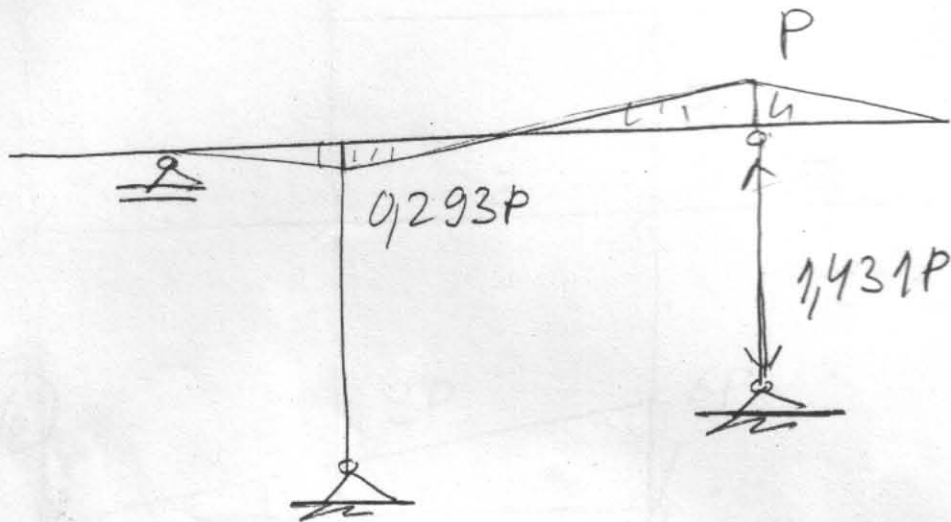
$$\underline{\frac{I}{F} = 0,01088 \, \text{m}^2}$$

$$\delta_{11}' = \left(\frac{1}{2} \cdot 2 \cdot 3 \right) \cdot \frac{2}{3} \cdot 3 + \left(\frac{1}{2} \cdot 3 \cdot 3 \right) \cdot \frac{2}{3} \cdot 3 +$$
$$+ 0,01088 \cdot (2 \cdot 1) \cdot 1 = 15,022$$

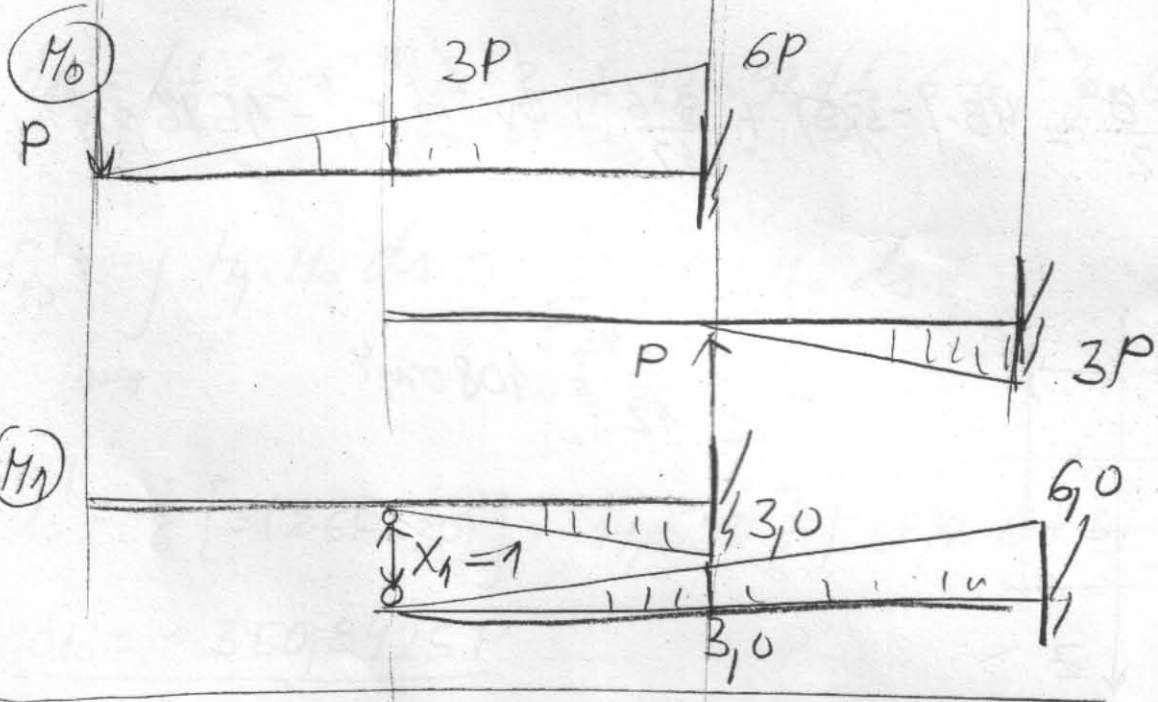
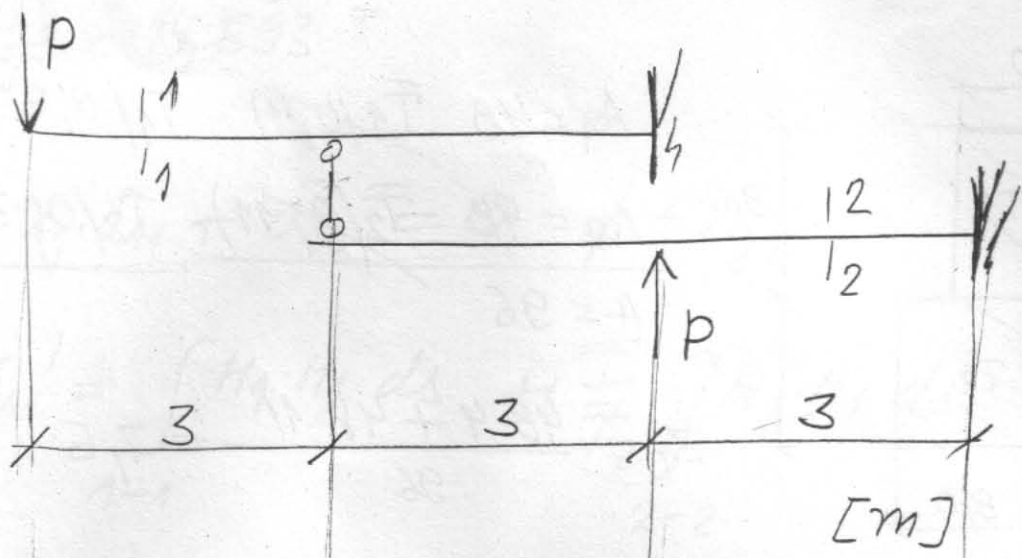
$$\delta_{10}' = \int M_1 \cdot M_0 \, ds = - \left(\frac{1}{2} \cdot 2 \cdot 3 \right) \cdot \frac{2}{3} \cdot 4P -$$
$$- \frac{3}{6} [3(2 \cdot 4P + P)] = -21,5P$$

$$(1) \quad X_1 \cdot 15,022 - 21,5P = 0 \quad \underline{X_1 = 1,431P}$$

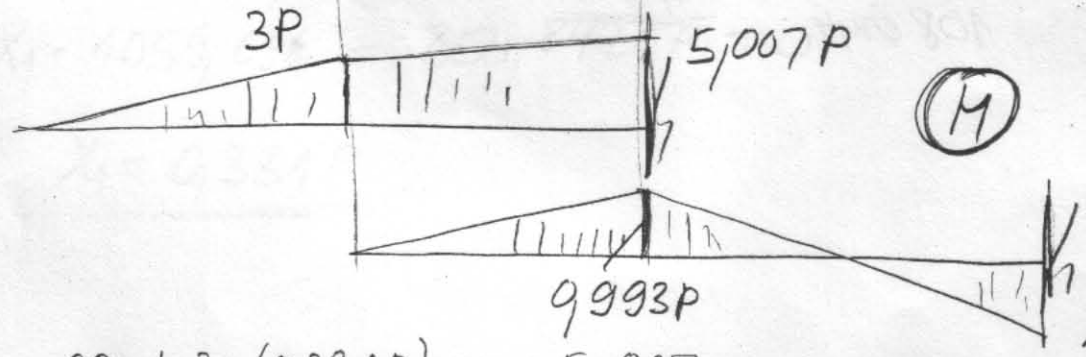
$$M = M_0 + X_1 \cdot M_1 = M_0 + 1,431P \cdot M_1$$



$$M = -4P + 1,431P \cdot (3) = 0,293P$$



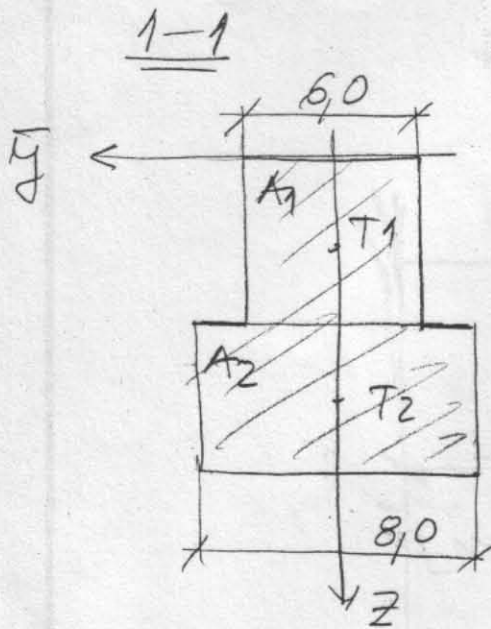
$$M = M_0 + X_1 \cdot M_1 = M_0 + 9.331P \cdot M_1$$



$$M = -6P + 3 \cdot (9.331P) = -5.007$$

$$M = -3 \cdot 9.331P = -9.993P$$

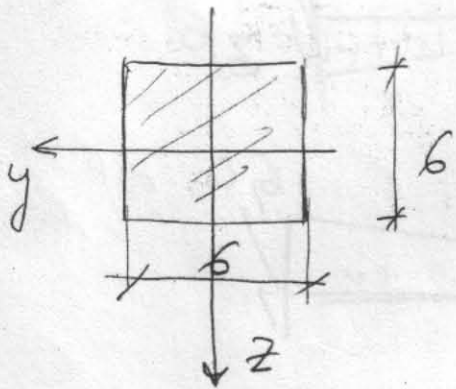
$$M = 3P - 6 \cdot 9.331P = 1.014P$$



$$\begin{aligned}
 A_1 &= 48 & \bar{T}_1 & (0, 4) & T_1 & (0, -3,5) \\
 A_2 &= 48 & \bar{T}_2 & (0, 11) & T_2 & (0, 3,5) \\
 \hline
 A &= 96 \\
 \bar{z}_T &= \frac{48 \cdot 4 + 48 \cdot 11}{96} = 7,5
 \end{aligned}$$

$$I_{yA} = \frac{6 \cdot 8^3}{12} + 48 \cdot (-3,5)^2 + \frac{8 \cdot 6^3}{12} + 48 \cdot (3,5)^2 = 1576 \text{ cm}^4$$

2-2



$$I_{y2} = \frac{6^4}{12} = 108 \text{ cm}^4$$

$$\frac{I_1}{I_2} = \frac{1576 \text{ cm}^4}{108 \text{ cm}^4} = \underline{\underline{14,593}}$$

$$\frac{I_1}{I_2} = 14,593$$

$$X_1 \cdot \delta_{11} + \delta_{10} = 0 \quad / \cdot EI_{y1}$$

$$\delta_{11}' = \int_{1-1} M_1 \cdot M_1 ds + \left(\frac{I_1}{I_2} \right) \int_{2-2} M_1 \cdot M_1 ds$$

$$\delta_{11}' = \left(\frac{1}{2} \cdot 3 \cdot 3 \right) \cdot \frac{2}{3} + 14,593 \cdot \left(\frac{1}{2} \cdot 6 \cdot 6 \right) \cdot \frac{2}{3} = \underline{\underline{1059,696}}$$

$$\delta_{10}' = \int_{1-1} M_1 \cdot M_0 ds + \frac{I_1}{I_2} \int_{2-2} M_1 \cdot M_0 ds$$

$$\delta_{10}' = -\frac{3}{6} [3 \cdot (2 \cdot 6P + 3P)] - 14,593 \cdot \frac{3}{6} [3P/2 \cdot 6 + 3P]$$

$$\delta_{10}' = \underline{\underline{-350,8425P}}$$

$$X_1 \cdot \delta_{11}' + \delta_{10}' = 0$$

$$X_1 \cdot 1059,696 - 350,8425P = 0$$

$$\underline{\underline{X_1 = 0,331P}}$$